# Warren County Light Industrial Site Assessment 

Final Report

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Table of Contents
Executive Summary .....  i
Introduction ..... 1
Site Identification and Zoning Analysis ..... 4
Trip Generation ..... 21
Trip Assignment and Distribution ..... 21
TRAFFIC ANALYSIS ZONES ..... 22
Socioeconomic Variables ..... 24
Employment Estimates ..... 24
Trip Generation ..... 25
Trip Distribution ..... 26
Mode Choice ..... 26
Trip Assignment ..... 26
Modeling Scenarios ..... 27
Roadway Suitability ..... 33
Height and Weight Restrictions ..... 33
Turning Radii Analysis ..... 35
Capacity Analysis ..... 39
Peak Hour Volumes - 2020 Existing Condition ..... 40
Peak Hour Volumes - 2045 No Build Condition (Background Growth) ..... 40
Peak Hour Volumes - 2045 Build (2045 No Build plus Proposed Development) ..... 41
Intersection Capacity Assessment ..... 41
Mid-Block Capacity Assessment ..... 46
Crash analysis ..... 50
Overall Crash Clusters (All Roadways) ..... 51
County Road Crash Clusters ..... 52
Mitigation Measures ..... 56
Midblock Operational Improvements ..... 56
Intersection Mitigations ..... 57
Intersection Safety Improvements ..... 69
Transportation Demand Management (TDM) strategies ..... 70
Implemenation ..... 71
Conclusion ..... 71
Appendix A - Zoning and Trip Generation
Appendix B - Model Volume ChangesAppendix C - Turning Radii AnalysisAppendix D - Capacity AnalysisAppendix E - Crash Tables

## LIST OF FIGURES

Figure 1- Light Industrial Sites .....  3
Figure 2 - Highlands Preservation Area ..... 5
Figure 3 - Site 1 Constraints ..... 6
Figure 4 - Site 2 Constraints ..... 7
Figure 5 - Site 3 Constraints ..... 8
Figure 6 - Site 4 Constraints ..... 9
Figure 7 - Site 5 Constraints ..... 10
Figure 8 - Site 6 Constraints ..... 11
Figure 9 - Site 7 Constraints ..... 12
Figure 10 - Site 8 Constraints ..... 13
Figure 11 - Site 9 Constraints ..... 14
Figure 12 - Site 10 Constraints ..... 15
Figure 13 - Site 11 Constraints ..... 16
Figure 14 - Site 12 Constraints ..... 17
Figure 15 - Site 13 Constraints ..... 18
Figure 16 - Site 14 Constraints ..... 19
Figure 17 - Site 15 Constraints ..... 20
Figure 18 - NJRTME Model Coverage ..... 22
Figure 19 - Warren County TAZ's and Identified Sites ..... 23
Figure 20 - Changes in Daily Traffic Flows (Auto \& Truck) between 2045 No Build and 2045 Build Scenarios ..... 28
Figure 21 - Changes in Daily Truck Traffic Flows between 2045 No Build and 2045 Build Scenarios ..... 29
Figure 22 - Analyzed Intersections ..... 32
Figure 23 - County Facilities with Height and Weight Restrictions ..... 34
Figure 24 - Sample AutoTURN Analysis ..... 35
Figure 25 - Turning Radii Assessment Intersections (Locations A to H) ..... 37
Figure 26 - Turning Radii Assessment Intersections (Locations I to O) ..... 38
Figure 27 - Intersection Level of Service and Delay (seconds) - Existing ..... 43
Figure 28 - Intersection Level of Service - No Build 2045 ..... 44
Figure 29 - Intersection Level of Service - Build 2045 ..... 45
Figure 30 - Mid Block Level of Service and Demand to Capacity Ratio - Existing ..... 47
Figure 31 - Mid Block Level of Service and Demand to Capacity Ratio - No Build 2045 ..... 48
Figure 32 - Mid Block Level of Service and Demand to Capacity Ratio - Build 2045 ..... 49
Figure 33 - Hotspots for All Crashes, Warren County (2016-2018) ..... 50
Figure 34 - US 22/ Phillipsburg Crashes (2016-2018) ..... 51
Figure 35 - US 46, NJ 182, CR 517 \& CR 604 Crashes (2016-2018) ..... 52
Figure 36 - Hotspots for County Route Crashes, Warren County (2016-2018) ..... 53
Figure 37 - US 46 at NJ 182 \& CR 517 Crashes (2016-2018) ..... 54
Figure 38 - Selected Hotspots for County Route Crashes, Warren County (2016-2018) ..... 55
Figure 39 - US 46/CR 519 Mitigation ..... 57
Figure 40 - CR 519/CR 623 Mitigation ..... 58
Figure 41 - CR 519/CR 620 Mitigation ..... 59
Figure 42 - CR 519/Foul Rift Road Mitigation ..... 60
Figure 43 - CR 519/CR 626 Mitigation ..... 61
Figure 44 - CR 519/CR 622 Mitigation ..... 62
Figure 45 - CR 519/CR 621 Mitigation ..... 63
Figure 46 - CR 519/CR 647 Mitigation ..... 64
Figure 47 - CR 519/CR 646 Mitigation ..... 65
Figure 48 - CR 519/NJ 57 Mitigation ..... 66
Figure 49 - CR 519/Strykers Road Mitigation ..... 67
Figure 50 - I-78/CR 632 Mitigation ..... 68
Figure 51 - NJ 31/CR 632 Mitigation ..... 69
LIST OF TABLES
Table 1 - Identified Sites ..... 1
Table 2 - Trip Production Rate by Land Use Code ..... 21
Table 3 - Socioeconomic Variables ..... 24
Table 4-2045 Employment Estimates Based on 2,000 Square Feet by Employee ..... 25
Table 5 - Truck Trip Generation Rates ..... 26
Table 6 - Percentage Truck Split by Facility Type ..... 26
Table 7 - Analyzed Intersections ..... 31
Table 8 - CAGR Computation ..... 40
Table 9 - CAGR Weighting ..... 41
Table 10 - Intersection LOS and Delay (seconds) ..... 42
Table 11 - Mid-Block D/C Ratios and LOS ..... 46
Table 12 - US 46/CR 519 LOS and Delay (seconds) ..... 57
Table 13 - CR 519/CR 623 LOS and Delay (seconds) ..... 58
Table 14 - CR 519/CR 620 LOS and Delay (seconds) ..... 59
Table 15 - CR 519/Foul Rift Road LOS and Delay (seconds) ..... 60
Table 16 - CR 519/CR 626 LOS and Delay (seconds) ..... 61
Table 17 - CR 519/CR 622 LOS and Delay(seconds) ..... 62
Table 18 - CR 519/CR 621 LOS and Delay (seconds) ..... 63
Table 19 - CR 519/CR 646 LOS and Delay (seconds) ..... 65
Table 20 - CR 519/NJ 57 LOS and Delay (seconds) ..... 66
Table 21 - CR 519/Strykers Road LOS and Delay (seconds) ..... 67
Table 22 - I-78/CR 632 LOS and Delay (seconds) ..... 68

## EXECUTIVE SUMMARY

Warren County's location in the Region and proximity to Interstates 78 and 80 position the County as a desirable center for warehouse development and freight/goods movement. The County is currently experiencing increased interest in warehousing and distribution development. This study was undertaken to understand the potential long-term impact of such development in the County.

Locations with large clusters of industrial zoning were identified for analysis. Locations within the Highlands Preservation area were not considered as developable. Fifteen sites with the potential for industrial development were identified for analysis in the study (Figure 1.) These 15 sites include over 4,000 acres and over 45 million square feet of gross floor area which could potentially be developed for industrial uses such as warehousing. If developed, these sites would generate a significant amount of traffic, both from trucks and automobiles, as increased employment and goods movement would be generated to and from these sites.

Figure I - Sites and Highlands Preservation Area


Warren County is comprised of a variety of community types, and County and local officials wish to be prepared for the challenges this potential development may bring throughout its communities. The purpose of the study was to identify areas of the greatest potential impact and the types of measures that would be necessary to mitigate the negative effects associated with traffic.

## CONDITIONS ASSESSMENT

To understand the County's needs and concerns, and to establish a relevant set of existing and possible future conditions in the study area, various data sources were consulted with a focus on freight and heavy vehicles. The data analysis included information about current land use and zoning; demographics; traffic patterns; traffic counts; and crash data. An extensive trip generation, distribution and assignment process was undertaken for each of the 15 sites. All traffic volumes were projected to a "Build Year" of 2045 to understand traffic conditions if all sites under study were developed in the future.

These additional site generated trips were overlaid on typical expected traffic growth from existing year 2020 to build year 2045. A capacity analysis was performed at key intersections and mainline roadway sections near the potential development site. This comparison was done for Existing 2020 conditions, 2045 No Build conditions (background growth only), and 2045 Build conditions (background growth plus potential development site trips). This comparison between future No Build and Build shows the direct impact of the additional development. The resulting analysis found that conditions deteriorate at nearly every location analyzed. The results of this future analysis are depicted in Figure 2 through Figure 5 and discussed in more detail in the body of the report.

Roadway suitability was considered during trip assignment which included existing height and weight restrictions along County roadways. A detailed truck turning radii analysis was completed to identify possible pinch points in the network for the expected increase in truck traffic. These locations are depicted in Figure 6 and 7 and methodology is discussed in more detail in the body of the report.

Figure 2 - Intersection Level of Service - No Build 2045



Figure 4 -Mid Block Level of Service and Demand to Capacity Ratio - No Build 2045


Figure 5 -Mid Block Level of Service and Demand to Capacity Ratio - Build 2045


Figure 6 -Turning Radii Assessment Intersections (Locations A to H)


Figure 7 -Turning Radii Assessment Intersections (Locations I to O)


## MITIGATION MEASURES

Based on the detailed data analysis and County input key mitigations measures for the identified issues will be needed to maintain acceptable traffic operations if the sites are developed. The mitigation measures relate to issues including:

- Intersection and Mainline Congestion
- Safety
- Truck Movements at Intersections
- Transportation Demand Management

This analysis identified the roadway capacity that would be required to accommodate an acceptable level of service to meet potential traffic demand for the full-buildout of the industrial sites evaluated. An evaluation of existing road widths, available right of way, and required additional right of way necessary to construct the potential improvements would require further study. Extensive right-of-way acquisition may be required in many locations to accommodate needed roadway capacity. It is noted that road widening may be prohibited on roadways and intersections that are adjacent to the Highlands Preservation Area boundary and may affect how widening concepts are advanced.

Mitigation measures that would be needed to accommodate expected increases in traffic as a result of site development at key intersections were developed. The potential increase in cars and trucks could be better accommodated at intersections through a variety of potential improvements ranging from low cost solutions such as moving stop bars to higher cost investments such as roadway widening. These necessary improvements are explained in more detail in the body of the report.

At the locations nearest the highest areas of projected development along CR 519, the mainline traffic volume is expected to be in excess of 3,000 vehicles per direction in the peak hour. One lane in each direction will not be sufficient to handle the additional demand. CR 519 would need to be widened to two lanes in each direction from approximately CR 646/Uniontown Road in Harmony to Route 46 in White Township to accommodate the anticipated demand to bring CR 519 to at least a Level of Service (LOS) D. If a LOS C is desired along CR 519, the widening should be further extended south to NJ 57 and north to l-80. The widening from CR 646 to Route 46 is assumed in many of the intersection mitigations measures described in the next section. Additionally, the segment of CR 620 between Belvidere and CR 519 would need to be widened to two lanes in each direction to accommodate the anticipated car traffic expected to be generated due to site developments.

The following intersections and midblock segments were included in this report. Capacity analysis was completed where volume data and signal timings were available.

## Intersections

- I-80 and CR 521 - 2-way stop controlled ramps
- CR 519 and CR 618 - 2-way stop controlled (T intersection)
- US 46 and CR 519 - 4-way signalized
- CR 519 and CR 623 - 4-way stop controlled by a blinker signal
- CR 519 and CR 620-2-way stop controlled (T intersection)
- CR 519 and Foul Rift Road - 2-way stop controlled (T intersection)
- CR 519 and CR 626 - 2-way stop controlled (T intersection)
- CR 519 and CR 622 (Roxburg Station Road) - 2-way stop controlled
- CR 519 and Brainards Road - 2-way stop controlled (T intersection)
- CR 519 and CR 647- 2-way stop controlled (T intersection
- CR 519 and CR 646 - 2-way stop controlled (T intersection)
- CR 519 and NJ 57 - 4-way signalized
- CR 519 and Strykers Road - 2-way stop controlled (T intersection)
- I-78 EB off-ramp and CR 632 - ramp stop controlled left turn to NB CR 632


## Midblock Segments

- CR 519, northeast of CR 610
- CR 519, Stone Hedge to Hope Crossing Road N
- CR 519, CR 623 (Brass Castle Road) to Pequest Drive
- CR 519, CR 620 to Brookfield Drive
- CR 519, Reeder Road to Grist Mill Road
- CR 519, Fairway Road to Hillside Avenue
- CR 632, Shurts Road to Halls Mill Road

Typical improvements that are needed to accommodate the expected increase in traffic include signal installation or optimization, addition of turning lanes at intersections, or other geometric changes to improve safety or truck accessibility. More detail regarding capacity analysis and the necessary improvements are provided in the body of the report.

Transportation Demand Management (TDM) strategies specific to freight and warehousing developments have been utilized within New Jersey and throughout the region, particularly in locations with substantial growth in warehousing and distribution centers. A series of potential TDM strategies specific to freight are included below.

- Identify potential rail connections to reduce the reliance entirely on truck trips.
- Promote non-peak trips where possible.
- Stagger worker shifts to reduce congestion during peak times.
- Promote development adjacent to key regional highways.
- Promote requirements that developers fund their "fair share" of necessary infrastructure improvements
- Create a county-wide freight transportation advisory group
- Encourage facility operators to promote specific trip paths/routing
- Promote use of alternative transportation modes, including worker shuttles or microtransit


## IMPLEMENTATION

Each mitigation measure would require additional study, engineering, funding and acceptance from various stakeholders and agencies. To explore these measures, coordination will be required between Warren County, NJ Highlands Council, the involved municipalities, developers, NJDOT, and the North Jersey Transportation Planning Authority. It is noted that road widening may be prohibited on roadways and intersections that are adjacent to the Highlands Preservation Area boundary and may affect how widening concepts are advanced.

## CONCLUSION

Warren County's proximity to Interstates 78 and 80 position the County as a desirable center for warehouse development and freight/goods movement. As a result of its location in the region and availability of large parcels of land zoned for industrial use, there is an increased interest in warehousing and distribution development.

This study evaluated a build-out scenario of property zoned for industrial use at 15 sites in Warren County. The potential long-term impacts of such development in the County would be substantial. The
increase in automobile and truck traffic volumes that would be anticipated if all 15 light industrial sites studied were developed would have a major impact on the County roadway network. The traffic increase is largely driven by the increase in automobiles that are expected to result from increased employment at these sites. Roadway levels of service would deteriorate to unacceptable conditions at most analyzed intersection locations and mainline segments of CR 519, as well as other key intersections throughout the County. In addition, the existing physical configuration at some intersections is challenging for trucks to complete turns without lane or shoulder encroachments which would be further impacted with an increase in truck traffic in the future.

TDM strategies can be used to reduce the demand on the roadway network; however, TDM strategies alone would not be enough to maintain traffic operations at an acceptable level should all sites studied be developed for industrial use. Necessary improvements to County roadways and intersections to maintain traffic operations at an acceptable level of service would require further detailed study as development projects are proposed. Future studies will need to identify locations where there are roadway right-of-way constraints that will require property acquisition for roadway widening for capacity improvements and/or to alleviate lane encroachments by turning trucks. Acquisition costs and Highland Preservation Area restrictions may be a consideration for the implementation of any required widening improvements in Warren County, particularly along CR 519.

## INTRODUCTION

Warren County's location in the Region and proximity to Interstates 78 and 80 position the County as a desirable center for warehouse development and freight/goods movement. The County is currently experiencing increased interest in warehousing and distribution development. This study was undertaken to understand the potential long-term impact of such development in the County.

Locations with large clusters of industrial zoning were identified for analysis. Locations within the Highlands Preservation area were not considered as developable. Fifteen sites with the potential for industrial development were identified for analysis in the study for evaluation in the study, as shown in Figure. These 15 sites include over 4,000 acres and over 45 million square feet of gross floor area which could potentially be developed for industrial uses such as warehousing. These sites are located in Alpha Borough, Belvidere, Franklin Township, Greenwich Township, Harmony Township, Lopatcong Township, Mansfield Township, Oxford Township, Phillipsburg, Pohatcong Township, and White Township. Table 1 lists the sites, municipality, zoning, and total acreage for each site.

Table 1 - Identified Sites

| Site ID | Municipality | Zoning | Total Area (Acres) |
| :---: | :---: | :---: | :---: |
| 1 | Belvidere | LM - Light Manufacturing | 283.2 |
|  | White | I - Industrial | 1260.7 |
| 2 | Oxford | I - Industrial | 49.0 |
|  | Oxford | I - Industrial, O \& LI - Office and Light Industrial | 66.6 |
|  | Oxford | I - Industrial, LI - Light Industrial | 186.2 |
| 3 | Mansfield | I - Industrial | 356.0 |
| 4 | Franklin | I - Industrial | 141.3 |
| 5 | Franklin | I - Industrial, IP-A - Industrial Park | 89.8 |
| 5 | Franklin | I - Industrial, IP-A - Industrial Park | 444.7 |
| 6 | Greenwich | ROM - Research, Office \& Manufacturing | 246.9 |
| 7 | Greenwich | RO - Research, Office | 199.7 |
| 8 | Alpha | I - Industrial | 71.6 |
| 9 | Pohatcong | I - Industrial | 146.0 |
|  | Alpha | I - Industrial | 239.0 |
| 10 | Phillipsburg | I - Industrial, Phillipsburg Commerce Park Redevelopment Area | 384.6 |
| 11 | Lopatcong | ROM -Research, Office \& Manufacturing | 376.2 |
| 12 | Harmony | I - Industrial | 623.9 |
| 13 | White | LDI -Low Density Industrial | 622.8 |
| 14 | White | I - Industrial | 943.3 |
| 15 | Harmony | I - Industrial | 369.0 |

The sites for analysis include warehouses under construction, known proposed/planned warehouse sites, and potential future sites. The list of potential future sites is based on building potential permitted by use as-of-right per current zoning in each municipality. The amount of potential development on sites was constrained based on site conditions limiting development such as wetlands, floodplains, steep slopes,
drainage/detention basins, internal roadways, and other identified factors. The 15 sites include one warehouse site already approved and under construction, and two warehouse sites currently in the site plan review process.

Figure 1- Light Industrial Sites


## SITE IDENTIFICATION AND ZONING ANALYSIS

To determine the impact of possible development of these 15 sites, corresponding parcels for each site were aggregated, determining total acreage using a geospatial geometrical computation. Sites within multiple municipalities or with different zoning regulation were separated for analysis. Areas of environmental constraint or impervious surfaces were considered not eligible for development.

Environmental constraints for each site that could limit developable area were identified and removed from the calculated developable areas. These included wetlands, waterways, Federal Emergency Management Agency (FEMA) flood zones, preserved open space, and preserved farmland. These are constraints that cannot be or would be difficult to overcome; therefore, they have been excluded from the total developable area. Impervious surfaces such as roads, buildings, and others were also removed from the developable area. The Highlands Preservation Area is depicted in Figure 2. GIS layers/data obtained from New Jersey Department of Environmental Protection (NJDEP), FEMA, and Warren County for the environmental screening include:
i. Impervious Surfaces
ii. Wetlands
iii. Waterways
iv. FEMA Flood Zones
v. County Property
vi. Federal Property
vii. Municipal Property
viii. Non-Profit Property
ix. Preserved Farmland
x. Semi Public Property
xi. State Property

Impervious surfaces for each site include roads, buildings, and other structures. On-site buildings were confirmed by using available Impervious Surfaces of New Jersey Edition September 30h, 2018 to conduct a visual analysis comparing footprints of buildings within the 15 sites with Bing satellite imagery from November 2019. From this exercise, 64 buildings were identified as no longer existing within the sites. The area of these sites was subtracted from the combined environmental and impervious surface area, and therefore considered to be clear for new development.

The end result was the available developable area that omitted environmental constraints, impervious surface, and proposed planned development areas. Those individual constraints and combined constraints are shown for each site in Figure 3 through Figure 17.

To estimate the total number of trips being generated by a site, the total allowable buildable area (Gross Floor Area) needed to be identified. The total allowable buildable area was calculated based on the zoning code of each municipality. The zoning code defines the limits for minimum and maximum lot size as well as setbacks, Floor Area Ratio (FAR), and maximum building coverage. Gross Floor Area (GFA) for each site was calculated by multiplying FAR, where available, by the available developable area. In cases where FAR is not provided, maximum building coverage was used.

Figure 2 - Highlands Preservation Area


Figure 3 - Site 1 Constraints


Figure 4 - Site 2 Constraints


Figure 5 - Site 3 Constraints


Figure 6 - Site 4 Constraints


Figure 7 - Site 5 Constraints


Figure 8 - Site 6 Constraints


Figure 9 - Site 7 Constraints


Figure 10 - Site 8 Constraints


Figure 11 - Site 9 Constraints


Figure 12 - Site 10 Constraints


Figure 13 - Site 11 Constraints


Figure 14 - Site 12 Constraints


Figure 15 - Site 13 Constraints


Figure 16 - Site 14 Constraints


Figure 17 - Site 15 Constraints


## TRIP GENERATION

Using the 15 sites identified and their respective developable area assessment from the zoning analysis, trip generation was completed using the $10^{\text {th }}$ Edition of the Institute of Transportation Engineers (ITE) Trip Generation Handbook. Corresponding land use codes from ITE $10^{\text {th }}$ Edition handbook for each site was identified based on the zoning and permitted land use. It should be noted that for a majority of sites the allowed zoning and permitted land use varies; therefore, the Industrial Land Use codes 110 through 157 from the ITE Handbook were considered for screening. Also, since sites could potentially include multiple developments, each with different trip production rates, three land use codes were identified per site for low $\left(R_{L}\right)$, medium ( $\mathrm{R}_{\mathrm{M}}$ ) and high ( $\mathrm{R}_{H}$ ) trip production rates. For the high trip production rate, land use code 110 (General Light Industrial) was used for all sites because the uses specified in the industrial zone districts generally fall within the light industrial definition. Table 2 illustrates the potential land use codes and the trip production rate for peak hours for each code.

Table 2 - Trip Production Rate by Land Use Code

| ITE Land <br> Use Code | Description <br> Combined <br> AM and PM <br> Peak Hour <br> Trip Rate |  |
| :---: | :--- | :---: |
| 110 | General Light Industrial | 1.33 |
| 130 | Industrial Park | 0.80 |
| 140 | Manufacturing | 1.29 |
| 150 | Warehousing | 0.36 |
| 151 | Mini-Warehouse | 0.27 |
| 154 | High-Cube Transload and Short-term Storage Warehouse | 0.18 |
| 155 | High-Cube Fulfillment Center Warehouse | 0.96 |
| 156 | High-Cube Parcel Hub Warehouse | 1.34 |
| 157 | High-Cube Cold Storage Warehouse | 0.23 |

Source: ITE $10^{\text {th }}$ Edition Handbook
Based on the previously calculated GFA in square feet for each of the 15 identified sites, trips (auto and truck) were generated for the AM / PM peak hours, and Daily. Trip production was estimated as a MixedUse scenario. Mixed Use assumes a weighted trip production approach, where each development will include a mix of multiple developments with different trip production rates. Under this approach each identified trip production rate (low, medium and high) per site are weighted by weighting constant. GFA is multiplied by a user defined percentage for the low ( $R_{L}$ ), medium ( $R_{m}$ ) and high ( $R_{H}$ ) AM and PM trip production rates identified per Land Use per site. To best represent the most likely development scenario, in consultation with the County the weights were set as: low production trip rate ( $R_{L}$ ) at $50 \%$, medium ( $R_{M}$ ) at $30 \%$, and high ( $\mathrm{R}_{\mathrm{H}}$ ) at 20\%. Detailed site data, zoning assignments, and trip generation information is presented in the table in Appendix A.

## TRIP ASSIGNMENT AND DISTRIBUTION

To conduct trip assignment and to identify the roadway segments that will see an increase in traffic flows originated from the proposed sites, the North Jersey Regional Transportation Model Enhanced (NJRTME) was used. This travel demand model was developed by the North Jersey Transportation Planning

Authority (NJTPA). It is a conventional four step transportation model that consists of trip generation, trip distribution, mode choice, and trip assignment. This model includes both highway and transit networks. It covers the NJTPA region, and the five surrounding Metropolitan Planning Organizations (MPO's) areas, as shown in Figure 18.

Figure 18-NJRTME Model Coverage


Source: NJTPA

## TRAFFIC ANALYSIS ZONES

The NJRTME is designed to support the forecasting of regional traffic flows, using socioeconomic information such as population and employment forecasts at five-year intervals. The underlying socioeconomic data is gathered, developed, and processed from the latest MPO-approved socioeconomic projections, as well as the U.S. Census, and other sources. This data is compiled into several categories by Traffic Analysis Zones (TAZs), which are established based on geographic definitions consistent with U.S. Census Tracts, but in some areas are disaggregated into Block Groups where finer levels of detail are required. For Warren County the TAZ zone system is comprised of twentyseven zones, closely aligned to the municipal boundaries, although slightly different. The TAZ zone system within the County was enhanced to include fifteen additional zones replicating the size and location of each proposed site. Figure 19 below displays the added zones (outlined in red) overlaid on top of the twenty-seven TAZs within the County.

Figure 19 - Warren County TAZ's and Identified Sites


Source: WSP, NJTPA

## Socioeconomic Variables

TAZs contain the relevant socioeconomic information needed to develop traffic flow forecasts for the fourstep process. This information is divided into population, number of households, employment, and average household income as shown in Table 3. Employment is further subdivided into ten different sectors corresponding to the North American Industry Classification System (NAICS).

Table 3 - Socioeconomic Variables

| CODE | DESCRIPTION |
| :--- | :--- |
| POP | Number of Persons Living within TAZ |
| HH | Number of Households contained in TAZ |
|  | EMPLOYMENT |
| AGMINE | Agriculture, Forestry, Fishing, and Mining |
| CONST | Construction |
| MFG | Manufacturing |
| TRANS | Transportation, Communications, Electric, Gas, and Sanitary |
| WHLSE | Wholesale Trade |
| RET | Retail Trade |
| FIRE | Finances, Insurance, and Real Estate |
| SER | Services |
| GOV | Government-Public Administration |
| MIL | Military |
|  |  |
| INCOME | Average Household Income |

For this project, the 2045 NJTPA socioeconomic forecasts were used and adjusted to include the information pertaining to each of the 15 sites. It was assumed the 2045 NJTPA socioeconomic projections do not include the proposed growth that would result from the inclusion of these sites. Therefore, employment estimates for each of these sites were added to the corresponding employment sector within each TAZ within the study area.

## Employment Estimates

To estimate the employment generated by each site, an average ratio of 2,000 square feet by employee was used. This metric was obtained from the National Association for Industrial and Office Parks (NAIOP), using the Commercial Buildings and Energy Consumption Survey (CBECS). This survey identifies the inventory, employment and square feet by employee for logistics buildings and their characteristics across a set of variables including region, building size, year built, and building type. This ratio was applied to the estimated GFA for each site. Logistics buildings included in this survey include refrigerated and non-refrigerated warehouses, distribution or shipping center, self-storage, and flex buildings ${ }^{1}$. This ratio varies according to the region, type of industry, and building type. Thus, applying this ratio to the 15 identified sites within the study area, socioeconomic estimates shown in Table 4 were used for the 2045 forecast year.

[^0]Table 4-2045 Employment Estimates Based on 2,000 Square Feet by Employee

| Site ID | Total Area <br> (Acres) | Developable Area <br> (Acres) | Gross Floor Area <br> (1,000 SQFT) | Employment <br> (\# of jobs) |
| :---: | ---: | ---: | ---: | ---: |
| $\mathbf{1}$ | $1,543.9$ | 809.2 | 8,175 | 4,088 |
| $\mathbf{2}$ | 301.7 | 152.9 | 1,332 | 666 |
| $\mathbf{3}$ | 356.0 | 88.3 | 962 | 481 |
| $\mathbf{4}$ | 141.3 | 88.9 | 968 | 484 |
| $\mathbf{5}$ | 534.5 | 313.4 | 3,413 | 1,707 |
| $\mathbf{6}$ | 246.9 | 149.9 | 980 | 490 |
| $\mathbf{7}$ | 199.7 | 53.2 | 658 | 329 |
| $\mathbf{8}$ | 71.6 | 143.8 | 694 | 347 |
| $\mathbf{9}$ | 385.0 | 325.5 | 1,123 | 562 |
| $\mathbf{1 0}$ | 384.6 | 379.2 | 5,672 | 2,836 |
| $\mathbf{1 1}$ | 376.2 | 537.7 | 1,648 | 824 |
| $\mathbf{1 2}$ | 623.9 | 660.0 | 5,066 | 2,533 |
| $\mathbf{1 3}$ | 622.8 | 311.7 | 4,877 | 2,439 |
| $\mathbf{1 4}$ | 943.3 |  | 5,750 | 2,875 |
| $\mathbf{1 5}$ | 369.0 |  | 4,073 | 2,037 |

## TRIP GENERATION

The NJRTM-E contains a Truck Specific procedure/module estimating trip distribution between destinations and/or origins, subdivided into External to External (pass-by-trips from zones outside the NJTPA Region to zones outside the NJTPA region), External to Internal (trips from zones outside the NJTPA Region to zones inside the NJTPA region), and Internal (trips within the NJTPA region) zones. Truck flows can be obtained for medium ( 2 axle, 6 -tire vehicles) and heavy ( $3+$ axle vehicles) size trucks. To perform truck trip generation, the employment data is grouped into five categories: retail, industrial (manufacturing), public (government and military), office (finance, insurance, real state) and other (Agriculture, Forestry, Fishing, Mining, Construction, Transportation, Communications, Electric, Gas, Sanitary, and Wholesale Trade). The trip rates in Table 5 are used for this purpose.

Table 5 - Truck Trip Generation Rates

| Type | Medium <br> Truck | Heavy <br> Truck | Commercial <br> Trips <br> Manhattan | Commercial <br> Trips NY Other <br> Counties | Commercial <br> Trips Other <br> Regions |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| by Population | 0.0240 | 0.0202 | 0.0407 | 0.0234 | 0.0116 |  |
| Households |  |  |  |  |  |  |
| by Employment | 0.1264 | 0.0590 | 0.1241 | 0.0709 | 0.0355 |  |
| Retail Employment | 0.0522 | 0.0800 | 0.1470 | 0.0840 | 0.0420 |  |
| Industrial Employment | 0.0032 | 0.0384 | 0.1470 | 0.0840 | 0.0420 |  |
| Public Employment | 0.0202 | 0.0051 | 0.0630 | 0.0360 | 0.0180 |  |
| Office Employment | 0.0553 | 0.1207 | 0.1470 | 0.0840 | 0.0420 |  |
| Other Employment |  |  |  |  |  |  |

Intermodal facilities are also accounted for in the NJRTM-E. For Warren County, the model shows the municipalities of Phillipsburg, Harmony, Lopatcong, White, and Liberty Townships as having Truck Terminals. To account for the assumption that by 2045 each of the 15 sites will have a warehouse built, this database was augmented to include a warehouse at each of these zones. The model considers the truck size split for each facility type as shown in Table 6.

Table 6 - Percentage Truck Split by Facility Type

| Intermodal <br> Facility | Medium Truck <br> Percentage | Heavy Truck <br> Percentage |  |
| ---: | ---: | ---: | :---: |
| Truck Terminal | $45 \%$ | $55 \%$ |  |
| Warehouse | $36 \%$ | $64 \%$ |  |
| Pipeline Terminals | $20 \%$ | $80 \%$ |  |
| Other Special Generators <br> (such as Ports and Airports) | $100 \%$ | $100 \%$ |  |

## TRIP DISTRIBUTION

This procedure is designed to match (distribute) trips between population areas and employment centers. It considers the cost of travel between different destinations. Trips are classified on whether they are oriented toward home or work. The model includes multiple trip purposes: Home-Based Work Direct (from home to work), Home-Based Work Strategic (e.g. drop off kids, pick up coffee on the way to work), HomeBased Shopping, Home-Based Other (e.g. leisure), Home-Based University, Work-Based Other (e.g. to lunch, shopping), Non-Home Non-Work (all the rest, e.g. from a store to school), and Trucks.

## MODE CHOICE

No specific adjustments were made to mode choice components of the model. This procedure was performed using the base parameters and methodology included in the model.

## TRIP ASSIGNMENT

The model performs the assignment of trips to both highway and transit networks. For the highway assignment the roadway network includes multiple parameters that determine the capacity of each roadway segment, such as number of lanes, facility type, tolls, and speed. Other, physical and
operational roadway characteristics such as terrain type, presence of shoulders, right or left turn lanes, and traffic control devices are also included but these do not play a significant role on the determination of the capacity. Roadway characteristics such as truck weight or height restrictions are roadway attributes not included on the model highway network. Therefore, truck trips could be assigned to roadway segments with any of these restrictions in place. Such trips cannot be reassigned with the model; rather, those volumes were manually rerouted to other roadways from one link to another before the intersection or mainline capacity assessment was performed.

## MODELING SCENARIOS

Two scenarios were modeled for this project: 2045 No Build and 2045 Build (2045 No Build + Proposed Development). For the 2045 No Build scenario, no modifications were made to the socioeconomic variables within the TAZs in Warren County. Relevant Transportation Improvement Projects (TIP) projects were included on the roadway network. However, for the 2045 Build scenario, the employment data described previously was added. Other changes to this scenario include the addition of warehouse facilities and centroid connectors to the roadway network.

Daily traffic flows from each scenario were compared to estimate changes in traffic patterns due to the proposed developments. Changes in traffic volumes can be used as proxy to trace routes (roadway segments) where an increase in future traffic will occur. Figure 20 and Figure 21 show the changes in daily traffic flows (total vehicles and trucks only, respectively) between scenarios.

Figure 20 - Changes in Daily Traffic Flows (Auto \& Truck) between 2045 No Build and 2045 Build Scenarios


Figure 21 - Changes in Daily Truck Traffic Flows between 2045 No Build and 2045 Build Scenarios


The magnitude of the line width highlights those roadway segments where an increase of traffic would occur. The highest impact would occur along roadways connecting proposed sites in the western portion of the county, County Road (CR) 621 (River Road) and CR 519 (Belvidere Road) These roads provide connections to major roadways such as U.S. Routes 22 and 46, on the south and north respectively. U.S. Route 22 would carry north-south traffic flows destined to Interstate 78. U.S. Route 46 would carry traffic flows to Interstate 80. For those sites analyzed in the southern portion of the county, CR 632 (Asbury Bloomsbury Road) would provide the main connection to Interstate 78. Other routes being impacted include CR 626, CR 624, and CR 632.

More specifically in AM and PM peak periods we see increased volumes that indicate commuter patterns. For example, in the AM we see an increase in southbound trips from Route 46 or I-80 towards CR 519 in Belvidere. In the PM the reverse is true, and there is an increase in trips heading north from CR 519 towards Route 46 and I-80. Projected model changes are displayed in more detail in Appendix B.

As explained previously, the NJRTME model is a demand-based model. These types of models are designed to assign trips to roadway segments despite its available capacity or physical constraints. Because of this, the model can result in roadway segments with excessive demand, or in other words, segments with Demand to Capacity Ratios (D/C) above one. For planning purposes, this characteristic is very important since it provides an indication of where the demand would want to go despite physical constraints. For example, the model assigns some of the site generated truck demand to CR 626 to connect CR 519 with CR 623 and NJ 57. However, CR 626 is a narrow, steep and windy roads that goes over a mountain making it a difficult path for trucks use. To account for such roadway characteristics (i.e. steepness, narrowness, weight and height restrictions), the highway assignment final volumes from this study were reviewed by county staff. Using the feedback from the County, truck trips that had been assigned to incompatible roadways by the model, i.e. weight or height restricted, were manually shifted to truck-compatible alternate paths that most closely replicated the trip assigned by the model. Those additional truck volumes were added to mid block and intersection Build volumes along the new path and subtracted from the original path. The adjusted volumes were used in the capacity analysis for both mid block and intersection locations.

Key intersections that would receive additional auto and truck traffic generated by future development of the industrial sites were identified. Those intersections were analyzed for truck turning radii compatibility, and where recent traffic counts were available, operation for the existing, 2045 No Build, and 2045 Build conditions. Mid-block locations between these intersections were also analyzed for traffic operations. The analyzed intersections are listed in Table 7 and shown in Figure 22.

Table 7 - Analyzed Intersections

| Intersection Intersecting Streets | Municipality |  |
| :--- | :--- | :--- |
| A | I-80 at CR 521 | Hope Township |
| B | CR 519 at CR 618 (Sarepta Road) | White Township |
| C | US 46 at CR 519 | White Township |
| D | CR 519 at CR 623 (Brass Castle Road) | White Township |
| E | CR 519 at CR 620 | White Township |
| F | CR 519 at Foul Rift Road | White Township |
| G | CR 519 at CR 626 (Lommason Glen Road) | White Township |
| H | CR 519 at CR 621 (Brainards Road) | White Township |
| I | CR 519 at CR 622 (Roxburg Station Road) | Harmony Township |
| J | CR 519 at CR 647 (Harmony Brass Castle Road) | Harmony Township |
| K | CR 519 at CR 646 (Belvidere Road) | Harmony Township |
| L | CR 519 at NJ 57 | Lopatcong Township |
| M | CR 519 at Strykers Road | Greenwich Township |
| N | I-78 at CR 632 (Asbury Bloomsbury Road) | Franklin Township |
| O | NJ 31 at CR 632 (Asbury Anderson Road) | Washington Township |

Figure 22 - Analyzed Intersections


## ROADWAY SUITABILITY

## HEIGHT AND WEIGHT RESTRICTIONS

Numerous bridges and roadways in Warren County have weight or height restrictions that preclude the use of a roadway by trucks exceeding those limits. The design or condition of these bridges and roadways do not permit usage by certain vehicles. Height is measured from the roadbed to the highest point on the vehicle or load it is carrying. Weight includes the weight of the vehicle plus the weight of the load that is being carried.

While necessary for physical and safety reasons, height and weight restrictions can create secondary impacts. Restrictions can limit transportation accessibility for local businesses, impact local economic viability, increase vehicle miles traveled, and divert traffic through residential neighborhoods. Eleven County routes have height restrictions and five county routes have weight restrictions

County roads with height and weight restrictions tend to be around the border of Warren County, with few restrictions in the County's interior. In Pohatcong, both CR 636 and CR 639 have height restrictions of 11'3', and 13'6', respectively. Additionally, CR 519 in Alpha has a 13'9' height restriction and a 10'6" height restriction in Lopatcong. These restrictions pose a mobility concern for trucks in the County as they restrict entrance into the County from the southeast. In the north, height restrictions are present along CR 658 in Knowlton, and CR 616 and CR 655 in Blairstown. Near the Delaware River, two height restrictions are present on CR 622 in Harmony, west of CR 519. To the north of this, CR 620 Spur A in Belvidere has a 13'9" height restriction.

Five county roads have weight restrictions, mostly in the southern portion of the County. CR 519 in Pohatcong has a four-ton limit and in Greenwich it has an eight-ton limit. CR 637 in Lopatcong and Greenwich has a 10-ton limit. CR 646 in Philipsburg, Lopatcong, and Harmony has a four-ton limit. CR 620 has an eight-ton limit White and Belvidere, and the short extent of CR 519 in Pohatcong has a fourton limit. The location of height and weight restricted County routes are presented in Figure 23.

Figure 23 - County Facilities with Height and Weight Restrictions


## TURNING RADII ANALYSIS

A turning radii analysis was conducted at the selected intersections. This analysis utilized AutoCAD's AutoTURN feature to simulate the ability of a WB-67 truck (defined as 73.5-foot-long total, including 53foot trailer) make each of the turns at the key intersections. Roadway extents were gathered from recent Google Earth satellite images. Turning movements were tested in five mph increments, so if a vehicle was able to turn at five mph, they were also tested at ten mph, etc. until the vehicle was not able to make the turn.

An example of the AutoTURN analysis for a sample intersection (CR 519 \& CR 623) from AutoCAD is presented in Figure 24. The process of testing turning movements at each intersection identified specific issues involving each turn. In the sample AutoTURN analysis below, green lines represent the outline of the vehicle body movement as it makes a turn. The magenta lines represent the path of the truck, defined as the center of the truck axles.

Figure 24 - Sample AutoTURN Analysis


An existing condition turning radii assessment was performed that classified each turning movement into one of three categories, as defined below and presented in Figure 25 and Figure 26:

- Trucks can turn without infringing on opposing traffic (Green)
- Trucks must encroach upon the opposing travel lane (Orange)
- Trucks must mount the curb or otherwise leave the roadway (Red)

Most turns can be presently made but require encroaching into the opposing lane. The ease of safely maneuvering depends on the location, as trucks may be able to easily turn at a low-volume intersection but require more encroachment into opposing traffic at busier locations.

Locations where trucks are currently unable to turn tend to have narrow rights-of-way or slip lanes that make maneuvering difficult while locations where trucks can easily turn tend to have wider right of ways or are off-ramps to interstate highways with higher speeds and truck volumes (such as I-80 or I-78).

More detailed information by movement is available in Appendix C .

Figure 25 - Turning Radii Assessment Intersections (Locations A to H)


Figure 26 - Turning Radii Assessment Intersections (Locations I to O)


## CAPACITY ANALYSIS

The level of service (LOS) measure is an indication of the amount of delay, measured in seconds, experienced by motorists before they can proceed through an intersection during peak travel hours. LOS results for intersections are given a letter grade, ' $A$ ' through ' $F$ ', with ' $A$ ' indicating no delay and ' $F$ ' denoting highly congested conditions. Generally, LOS A through C are considered acceptable. For roadway mainline sections, LOS is based on the ratio of demand versus roadway capacity, or D/C ratio.

Count traffic data was collected from available resources and summarized to derive traffic volumes, peak hour adjustment factors, and the percentage of heavy vehicles for the morning and evening peak hours. Subsequently, intersections and roadway segments were analyzed with traffic simulation software. For this study LOS was calculated for the morning and evening peak hours to evaluate the differences in traffic patterns, and to better quantify the delay along the more congested roadway segments in the study area.

The following intersections and midblock segments were analyzed, where volume data and signal timings were available. The letter assignments provide a location key to the results figures provided later in this section.

## Intersections

- C - US 46 and CR 519 - signalized
- D - CR 519 and CR 623 - 4-way stop controlled by a blinked signal
- E - CR 519 and CR 620-2-way stop controlled (T intersection)
- F CR 519 and Foul Rift Road - 2-way stop controlled (T intersection)
- G - CR 519 and CR 626-2-way stop controlled (T intersection)
- H - CR 519 and CR 622 (Roxburg Station Road) - 2-way stop controlled
- I - CR 519 and Brainards Road - 2-way stop controlled (T intersection)
- K - CR 519 and CR 646 - 2-way stop controlled (T intersection)
- L - CR 519 and NJ 57-Signalized
- M - CR 519 and Strykers Road - 2-way stop controlled (T intersection)
- N - I-78 EB off-ramp and CR 632 - ramp stop controlled left turn to NB CR 632


## Midblock Segments

- AA - CR 519, northeast of CR 610
- BB - CR 519, Stone Hedge to Hope Crossing Road N
- CC - CR 519, CR 623 (Brass Castle Road) to Pequest Drive
- DD - CR 519, CR 620 to Brookfield Drive
- EE - CR 519, Reeder Road to Grist Mill Road
- FF - CR 519, Fairway Road to Hillside Avenue
- GG - CR 632, Shurts Road to Halls Mill Road

Volume data was obtained from the NJDOT Traffic Monitoring website https://www.njtms.org/map/ and from sources provided by Warren County. Trafficware LLC's Signal Timing and Analysis software, Synchro version 10.3.122.0 was used for all stop controlled and signalized intersection analysis.
McTrans' Highway Capacity Software, version 7.8.5, Highways - Two Lane module was used for all midblock analysis segments. Output files are presented in Appendix D.

## PEAK HOUR VOLUMES - 2020 EXISTING CONDITION

Available traffic data was obtained from various years, ranging from 2003 to 2019 and included intersection peak hour turning movement counts and AADT mainline counts. Morning and evening peak hour volumes were pulled directly from counts provided with hourly distribution. For locations where only mainline AADT was available a peak hour factor was applied to produce peak hour volumes. Peak hour volume growth was projected to the year 2020 using a Compound Annual Growth Rate (CAGR) derived by looking at historical data at five locations where multiple years were available. The growth factor obtained fluctuates widely between locations. In order to account for this variability an overall weighted CAGR was obtained using the latest traffic volumes to normalize the data. This resulted in a 1.15\% overall CAGR and shown in Table 8. This factor was applied to each count grown to the Year 2020.

Table 8 - CAGR Computation

|  |  |  | CAGR |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Roadway Segment | Year1 | Year2 | AADT | AM | PM |
| CR 519, Reeder Road to Grist Mill Road | 2015 | 2018 | 4.85\% | -1.64\% | 2.26\% |
| CR 519, CR 623 (Brass Castle Road) to Pequest Road | 2015 | 2018 | 5.95\% | 16.63\% | 12.04\% |
| NJ 57, Lincoln Avenue to N Wandling Avenue | 2015 | 2018 | 0.74\% | 2.16\% | 0.12\% |
| NJ 31, Springtown Road to Clubhouse Drive | 2014 | 2017 | -2.24\% | 0.14\% | -2.96\% |
| CR 519, northeast of CR 610 | 2011 | 2017 | 0.10\% | 3.97\% | 2.88\% |
|  |  |  | 0.93\% | 3.49\% | 1.50\% |
| Weighted Compou | Annual | wth Rate | 1.15\% |  |  |

## PEAK HOUR VOLUMES - 2045 NO BUILD CONDITION (BACKGROUND GROWTH)

To develop traffic volumes for the 2045 No Build condition a background growth rate was derived. This factor was developed using the latest sociodemographic projections from the NJTPA for the 2045 Year and the NJRTME Model. Traffic volumes for the AM, PM Peak, Daily time periods for all roadways within Warren County were used. The CAGR values obtained show little variability between facility type and time periods. However, in order to normalize this small difference a weight was derived using estimated model volumes (Table 9).

|  | CAGR |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Facility Type | AM | PM | DAILY |  |
| Freeways | $0.47 \%$ | $0.60 \%$ | $0.51 \%$ |  |
| Principal Arterials Divided | $0.63 \%$ | $0.66 \%$ | $0.67 \%$ |  |
| Principal Arterials Undivided | $0.58 \%$ | $0.61 \%$ | $0.59 \%$ |  |
| Major Arterials Undivided | $0.57 \%$ | $0.64 \%$ | $0.57 \%$ |  |
| Minor Arterials | $0.90 \%$ | $0.98 \%$ | $0.84 \%$ |  |
| Collector /Locals | $0.44 \%$ | $0.51 \%$ | $0.40 \%$ |  |
| Overall Weighted Average | $\mathbf{0 . 5 9 \%}$ |  |  |  |
|  |  |  |  |  |

## PEAK HOUR VOLUMES - 2045 BUILD (2045 NO BUILD PLUS PROPOSED DEVELOPMENT)

The 2045 Build scenario estimates traffic operations in the future if the potentially developable parcels are built-out. The changes in volumes that were predicted by the NJTRM-E model scenario were overlaid on top of the 2045 No Build volumes. This process consisted of determining the demand along the roadway segments that will carry the site generated traffic using the estimated trip distribution from the 2045 Build condition model run. 2045 Build site generated traffic volumes were derived for the morning and evening peak hours, by applying the percentage trip distribution from the model run to the ITE trip generation estimates described in previous sections.

## INTERSECTION CAPACITY ASSESSMENT

The traffic counts developed above were analyzed as part of the process to determine congestion and how traffic flows through select county roads. The overall result of the traffic volume analysis is that congestion is currently (2020) minimal throughout the study area, though there are some locations that may experience congestion in the future during peak hours.

In 2020 (Figure 27), all intersections operate well, with slight congestion at US 46 and CR 519 during the PM peak hour. By 2045 No Build (Figure 28), that intersection experiences much greater congestion, with a predicted LOS of D and F for AM and PM, respectively. The intersection of CR 519/CR 623 also experiences congestion in 2045 No Build, with LOS of $C$ and $F$ for AM and PM peak hour, respectively. The remaining three intersections are much lower in volume, and therefore operate well both presently and in the 2045 No Build peak periods.

However, if all 15 sites are developed to their full capacity as projected by the trip generation and assignment, the increase in traffic at these locations cause all analyzed intersections to fail in the 2045 Build scenario (Figure 29).

Table 10 summarizes the LOS and delay in seconds of the 2020 Existing, 2045 No Build and 2045 Build Scenarios of each location by peak hour.

Table 10 - Intersection LOS and Delay (seconds)

| Location | $\begin{gathered} \text { EXISTING } \\ \text { AM } \\ \hline \end{gathered}$ |  | $\begin{gathered} \text { EXISTING } \\ \text { PM } \\ \hline \end{gathered}$ |  | 2045 <br> No Build <br> AM |  |  |  | 2045 <br> Build <br> AM |  | $\begin{gathered} 2045 \\ \text { Build } \\ \text { PM } \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | LOS | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS | Delay |
| C-US 46 at CR 519 | C | 21.7 | D | 38.2 | D | 42.4 | F | 82.3 | F | 315.9 | F | 514.4 |
| D-CR 519 at CR 623 <br> (Brass Castle Road) | B | 14.8 | C | 24.1 | C | 21.3 | F | 56.8 | F | 697.4 | F | 722.6 |
| E-CR 519 at CR 620 | A | 4.3 | A | 9.6 | A | 5.4 | C | 24.3 | F | 3541 | F | 1801 |
| F-CR 519 and Foul Rift Road | A | 0.1 | A | 0.1 | A | 0.1 | A | 0.1 | F | ** | F | 4661 |
| G-CR 519 at CR 626 (Lommason Glen Road) | A | 0.4 | A | 0.7 | A | 0.5 | A | 0.9 | F | 1232 | F | 471.2 |
| H-CR 519 at CR 622 (Roxburg Station Road) | A | 1.1 | A | 1.4 | A | 1.3 | A | 1.8 | F | ** | F | ** |
| I-CR 519 at CR 621 <br> (Brainards Road) | A | 1.5 | A | 2.3 | A | 1.6 | A | 2.7 | F | ** | F | 4568 |
| K-CR 519 at CR 646 <br> (Belvidere Road) | A | 5.0 | A | 6.9 | A | 5.5 | A | 8.9 | F | 2836 | F | 1295 |
| L-CR 519 and NJ 57 | B | 17.8 | C | 22.9 | B | 19.4 | C | 25.5 | F | 81.5 | F | 157.5 |
| M-CR 519 and Strykers Road | A | 6.4 | B | 14.8 | A | 7.3 | E | 38.0 | A | 7.9 | F | 64.6 |
| N-I-78 at CR 632 (Asbury Bloomsbury Road) | A | 4 | A | 4.1 | A | 4.1 | A | 4.1 | F | 465.4 | A | 7.2 |

**Delay not calculable - delay is outside the high boundary and cannot be computed.

Figure 27 - Intersection Level of Service and Delay (seconds) - Existing


Figure 28 - Intersection Level of Service - No Build 2045


Figure 29-Intersection Level of Service - Build 2045


## MID-BLOCK CAPACITY ASSESSMENT

In 2020, all midblock sections on County Roads operate well (Figure 30), and continue to operate well in the 2045 No Build (Figure 31) condition. Once the additional trips generated by the 15 industrial sites are added to the roadway network, several segments of CR 519 deteriorating to LOS E or worse, specifically CR 519 between Grist Mill Road and CR 623 (Brass Castle Road) (Figure 32). The remaining segments of CR 519 deteriorate to LOS D in at least one peak hour. Below in Table 11 are the Demand/Capacity Ratios of the 2020 Existing, 2045 No Build and 2045 Build Scenarios of each location by peak hour and direction.

Table 11 - Mid-Block D/C Ratios and LOS

|  | $\begin{gathered} \text { EXISTING - } \\ \text { AM } \end{gathered}$ |  | EXISTING - PM |  | $\begin{gathered} 2045 \text { No Build } \\ \text { - AM } \end{gathered}$ |  | 2045 No Build - PM |  | 2045 Build -AM |  | $\begin{aligned} & 2045 \text { Build - } \\ & \text { PM } \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Location | $\begin{gathered} \mathrm{D} / \mathrm{C} \\ \text { Ratio } \end{gathered}$ | LOS | $\mathrm{D} / \mathrm{C}$ Ratio | LOS | $\begin{gathered} \mathrm{D} / \mathrm{C} \\ \text { Ratio } \end{gathered}$ | LOS | $\mathrm{D} / \mathrm{C}$ Ratio | LOS | $\mathrm{D} / \mathrm{C}$ Ratio | LOS | $\begin{gathered} \mathrm{D} / \mathrm{C} \\ \text { Ratio } \end{gathered}$ | LOS |
| AA-CR 519, northeast of CR 610 - NB | 0.18 | A | 0.15 | A | 0.20 | B | 0.18 | A | 0.20 | OB | 0.36 | C |
| AA-CR 519, northeast of CR 610 - SB | 0.15 | A | 0.20 | B | 0.17 | A | 0.23 | B | 0.52 | D | 0.23 | B |
| BB-CR 519, Stone Hedge to Hope Crossing Road - EB | 0.20 | B | 0.17 | A | 0.23 | B | 0.20 | B | 0.23 | B | 0.20 | B |
| BB-CR 519, Stone Hedge to Hope Crossing Road - WB | 0.20 | B | 0.22 | B | 0.23 | B | 0.25 | B | 0.52 | D | 0.25 | B |
| CC-CR 519, CR 623 Brass Castle Road to Pequest Drive - NB | 0.29 | B | 0.33 | C | 0.33 | C | 0.38 | C | 0.33 | C | 0.57 | D |
| CC-CR 519, CR 623 Brass Castle Road to Pequest Drive - SB | 0.22 | B | 0.22 | B | 0.25 | B | 0.25 | B | 0.65 | E | 0.25 | B |
| DD-CR 519, CR 620 to Brookfield Drive - NB | 0.19 | A | 0.19 | A | 0.22 | B | 0.22 | B | 0.22 | B | 0.84 | E |
| DD-CR 519, CR 620 to Brookfield Drive - SB | 0.14 | A | 0.15 | A | 0.16 | A | 0.17 | A | 1.01 | F | 0.17 | A |
| EE-CR 519, Reeder Rd to Grist Mill Road - NB | 0.24 | B | 0.28 | B | 0.27 | B | 0.32 | C | 1.73 | F | 0.32 | C |
| EE-CR 519, Reeder Rd to Grist Mill Road - SB | 0.22 | B | 0.28 | B | 0.26 | B | 0.33 | C | 0.37 | C | 0.97 | E |
| FF-CR 519, Fairway Rd to Hillside Ave | 0.12 | A | 0.25 | B | 0.14 | A | 0.28 | B | 0.58 | D | 0.28 | B |
| FF-CR 519, Fairway Rd to Hillside Ave | 0.16 | A | 0.15 | A | 0.18 | A | 0.17 | A | 0.18 | A | 0.47 | D |
| GG-CR 632, Shurts Road to Halls Mill Road - EB | 0.14 | A | 0.13 | A | 0.16 | A | 0.15 | A | 0.18 | B | 0.35 | C |
| GG-CR 632, Shurts Road to Halls Mill Road - EB | 0.11 | A | 0.17 | A | 0.13 | A | 0.20 | B | 0.33 | C | 0.31 | C |

Figure 30 - Mid Block Level of Service and Demand to Capacity Ratio - Existing


Figure 31 - Mid Block Level of Service and Demand to Capacity Ratio - No Build 2045


Figure 32 - Mid Block Level of Service and Demand to Capacity Ratio - Build 2045


## CRASH ANALYSIS

Crash records for the years 2016, 2017, \& 2018 were collected and mapped for all roads in Warren County from the New Jersey Department of State's (NJDOT) Safety Voyager system (Figure 33). This

Figure 33 - Hotspots for All Crashes, Warren County (2016-2018)

analysis was performed for two different crash subsets. The first subset included all crashes within the database (10,041 records). This analysis was aimed to identify the overarching crash clusters in the County (Figure 33). The second subset analyzed only crash incidents along County Roadways and within a 50-foot radius. The purpose of this second analysis was to identify crash clusters at the intersection/ corridor level along County Roadways.

Figure 34 - US 22/ Phillipsburg Crashes (2016-2018)


Source: 2016-2018 NJDOT Safety Voyager / Warren County

## OVERALL CRASH CLUSTERS (ALL ROADWAYS)

Two major hotspots identified are shown in detail in the insets (Figure 34 and Figure 35) near Routes 46/182 (599 total crashes, 8\% involving trucks) and US 22/ Phillipsburg (1,208 total crashes, $9 \%$ involving trucks total), while another minor hotspot at the intersection of NJ 31 and NJ 57 ( 217 total crashes) was also identified. The hotspot containing 400 total crashes includes the top two Warren County crash intersections as reported in the 2017 and 2018 Warren County crash summary reports, US 22/CR 638 and US 22/CR 519.

A detailed summary of the crash analyses is presented in crash tables in Appendix E that provide the number of crashes at each identified hotspot location by Type of Crash, Road Surface Condition, Lighting Conditions, Severity, and Vehicle Type. Statewide averages (2016-2018) for each category are also presented in the table and the percentage of crash for any category that is higher than the Statewide average for similar road type is represented in bold font. Morning peak period for the crash analysis was 7 AM to 9 AM, while evening peak period was 4 PM to 6 PM.

For all roads in Warren County, the identified hotspots and their overrepresented crash types are:

- US 22/ Phillipsburg - Crashes occurring at rates significantly higher than the statewide average include right angle ( $17 \%$ hotspot vs $10 \%$ statewide), fixed object ( $12 \%$ vs $9 \%$ ), stuck parked vehicle ( $16 \%$ vs $1 \%$ ), and backing (4\% vs 1\%). Nine percent involved heavy vehicles.

Figure 35 - US 46, NJ 182, CR 517 \& CR 604 Crashes (2016-2018)


Source: 2016-2018 NJDOT Safety Voyager / Warren County

- US 46/NJ 182/CR 517/CR 604 Crashes occurring at rates significantly higher than the statewide average include right angle (24\% hotspot vs 10\% statewide), struck parked vehicle (11\% vs 1\%), and backing (3\% vs 1\%). Eight percent involved heavy vehicles.


## COUNTY ROAD CRASH CLUSTERS

The second hotspot analysis was completed to determine hotspots from crashes that occurred only on County Routes (Figure 36). Figure 37 and Figure 38 provide more detailed inset maps of the two major hotspot locations for crashes occurring on County Routes, accompanied by a brief summary table. The most prominent hotspots included 61 total crashes (7\% involving trucks) near US 46/Route 182/CR 517, and 92 total crashes (3\% involving trucks) at US 22/CR 519. Crashes involving trucks are indicated by grey dots. Three minor hotspot locations are shown in Figure 36 and tabulated in Appendix E.

The analysis determined that existing crash hot spots are in areas that are NOT expecting a significant increase in traffic as a result of the industrial site development; therefore, it is not expected that crashes in these hotspots will be made worse. It is possible that new hot spots emerge as light industrial development occurs

Figure 36 - Hotspots for County Route Crashes, Warren County (2016-2018)


For all County Roads in Warren County, the identified hotspots and their overrepresented crash types are:

- US 22/CR 638/CR 519 - Crashes occurring at rates significantly higher than the statewide average include rear end (55\% hotspot vs 48\% statewide), backing ( $2 \%$ vs 1\%), and other ( $6 \%$ vs 2\%). Ten percent involved heavy vehicles. This intersection appears as a top crash location on

Warren County's annual crash summary.

Figure 37 - US 46 at NJ 182 \& CR 517 Crashes (20162018)


| US 46 @ NJ 182 \& CR 517 |  |  | Statewide |
| :---: | :---: | :---: | :---: |
| [18 | Right Angle | 16\% | 10\% |
| $\pi$ | Pedestrian | 3\% | 0.9\% |
| ๓ | Wet Surface | 22\% | 18\% |
| $\underbrace{-1}$ | Dusk | 5\% | 3\% |
|  | Heavy Vehicles | 7\% | N/A |
|  | ashes | 61 |  |

## Truck Crashes Orash Concentration

Gashes on County Routes
(xx) No. of Gashes
Eighe
Low

Source: 2016-2018 NJDOT Satety Voyager / Warren County

- US 22/CR 519-Crashes occurring at rates significantly higher than the statewide average include right angle (14\% hotspot vs 10\% statewide), sideswipe ( $15 \%$ vs $9 \%$ ), backing ( $3 \%$ vs $1 \%$ ), and other (15\% vs $2 \%$ ). Three percent involved heavy vehicles. \%). Ten percent involved heavy vehicles. This intersection appears as a top crash location on Warren County's annual crash summary.
- US 46/CR 517-Crashes occurring at rates significantly higher than the statewide average include right angle (16\% hotspot vs 10\% statewide), fixed object (23\% vs 19\%), backing (4\% vs 1\%), pedestrian (3\% vs 1\%) and other (8\% vs 2\%). Seven percent involved heavy vehicles.
- I-80/CR 517 - Crashes occurring at rates significantly higher than the statewide average include left turn/Uturn ( $8 \%$ hotspot vs $2 \%$ statewide), head on ( $4 \%$ vs $2 \%$ ), overturned ( $2 \%$ vs 1\%), backing (6\% vs 1\%), animal (6\% vs 4\%), pedestrian (4\% vs 1\%) and other ( $4 \%$ vs $2 \%$ ). Ten percent involved heavy vehicles.
- US 22/Morris Street/CR 646 Crashes occurring at rates significantly higher than the statewide average include rear end (59\% hotspot vs 48\% statewide), fixed object ( $13 \%$ vs $9 \%$ ), parked vehicle (10\% vs 1\%), and backing (3\% vs 1\%). Five percent involved heavy vehicles.
- CR 630/CR 640-Crashes occurring at rates significantly higher

Figure 38 - Selected Hotspots for County Route Crashes, Warren County (2016-2018)


Source: 2016-2018 NJDOT Salety Voyager / Warren County
than the statewide average include rear end (59\% hotspot vs 48\% statewide), fixed object ( $13 \%$ vs $9 \%$ ), head on ( $5 \%$ vs $2 \%$ ), and overturned (3\% vs 1\%). Three percent involved heavy vehicles.

- NJ 94/CR 521/CR 602/CR 616/CR 607 Crashes occurring at rates significantly higher than the statewide average include fixed object ( $11 \%$ hotspot vs $9 \%$ statewide), struck parked vehicle ( $26 \%$ vs $1 \%$ ), left turn/U-turn (4\% vs 2\%), head on (4\% vs 2\%), and backing (19\% vs 1\%). Seven percent involved heavy vehicles.


## MITIGATION MEASURES

To accommodate the expected increase in traffic that would result from the development of the 15 industrial sites and provide an acceptable level of service, a combination of improvements including additional turning lanes or intersection alignments, traffic signal timing adjustments, and Travel Demand Management strategies were explored. The potential increase in cars and trucks could be better accommodated at intersections through a variety of potential improvements ranging from low cost solutions such as optimizing stop bars to higher cost investments such as roadway widening. Other physical improvement to mitigate roadway impacts, such as round-abouts, should be explored in the future as sites are developed.

An evaluation of existing road widths, available right of way, and required additional right of way necessary to construct these potential improvements would require further study. Extensive right-of-way acquisition may be required in many locations to accommodate needed roadway capacity. It is noted that road widening may be prohibited on roadways and intersections that are adjacent to the Preservation Area boundary and may affect how widening concepts are advanced.

## MIDBLOCK OPERATIONAL IMPROVEMENTS

At the locations nearest the highest areas of projected development along CR 519, the mainline traffic volume is expected to be in excess of 3,000 vehicles per direction in the peak hour. One lane in each direction will not be sufficient to handle the additional demand. CR 519 would need to be widened to two lanes in each direction from approximately CR 646/Uniontown Road in Harmony to Route 46 in White Township to accommodate the anticipated demand. This widening is assumed in many of the intersection mitigations measures described in the next section. Additionally, the segment of CR 620 between Belvidere and CR 519 would need to be widened to two lanes in each direction to accommodate the anticipated car traffic expected to be generated due to site developments. This widening should be carried through each intersection along the corridor and may require extensive right-of-way acquisition depending on the County's current right-of-way.

## INTERSECTION MITIGATIONS

US 46/CR 519
In the 2045 Build condition, this intersection is expected to deteriorate to LOS F in the AM and PM peak hours. With a low level of investment, the northbound and southbound approaches can be restriped to create a left turn lane and a through/right lane and the signal can be optimized to improve operations (Table 12). Currently, each approach is two lanes consisting of a though/left turn lane and a right turn lane. These changes would require coordination with NJDOT as this signal is NJDOT's jurisdiction.

Table 12 - US 46/CR 519 LOS and Delay (seconds)

| US 46 and CR 519 | $\begin{gathered} 2045 \text { Build - } \\ \text { AM } \\ \hline \end{gathered}$ |  | $\begin{gathered} 2045 \text { Build - } \\ \text { PM } \\ \hline \end{gathered}$ |  |  | 2045 Build Improved AM |  | 2045 Build Improved PM |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | LOS | Delay | LOS | Delay |  | LOS | Delay | LOS | Delay |
| Current configuration | F | 315.9 | F | 514.4 | Restripe NB and SB as left, through/right | E | 63.0 | D | 46.6 |

At this intersection, the largest trucks need to cross the double yellow center line to make every turning move other than northbound and southbound left turns. Pulling back the stop bars on each approach allows more pavement area to begin the turn and would enable those moves.
Mitigations are shown in Figure 39.
Figure 39 - US 46/CR 519 Mitigation


## CR 519/CR 623

In the 2045 Build condition, this intersection is expected to deteriorate to LOS F in the AM and PM peak hours (Table 13). This intersection is currently stop controlled with a flashing traffic signal. Adding a signal and widening provides significant operational improvement though the addition of lanes in each direction resulting in eastbound left and through/right lanes, westbound left and through/right lane, northbound left/through and through/right lanes, and southbound left/through and through/right lane. The intersection would still operate at LOS F in the PM with geometric and signal optimization improvements, but with much lower delay as shown below. The County has a design prepared that widens the intersection to left and through/right lanes eastbound and southbound, left, through, and right turn lanes northbound, and left, though, and channelized right turn lane westbound. However, this design was prepared prior to this report and may need to be revisited to account for anticipated traffic increases.

Table 13-CR 519/CR 623 LOS and Delay (seconds)

| CR 519 and CR$623$ | $\begin{gathered} 2045 \text { Build - } \\ \text { AM } \end{gathered}$ |  | 2045 Build PM |  |  | 2045 Build Improved AM |  | 2045 Build Improved PM |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | LOS | Delay | LOS | Delay |  | LOS | Delay | LOS | Delay |
| Current configuration | F | 697.4 | F | 722.6 | Signalize and add EB and WB left turn lanes, and add one NB and SB lane | D | 46.8 | C | 30.0 |

Mitigations are shown in Figure 40.
Figure 40 - CR 519/CR 623 Mitigation


## CR 519/CR 620

This intersection would require significant widening to improve operations in the Build condition (Table 14). Signalizing and enlarging the intersection to include two through lanes and a left turn lane southbound (CR 620), two through lanes and a right turn lane northbound (CR 519), and two left lanes and a right turn lane westbound (CR 519) would improve operations to LOS E.

Table 14 - CR 519/CR 620 LOS and Delay (seconds)

| CR 519 and CR <br> 620 | 2045 Build - <br> AM |  | 2045 Build - <br> PM |  |  | 2045 Build <br> Improved AM |  | 2045 Build <br> Improved PM |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |
| LOS | Delay | LOS | Delay |  | LOS | Delay | LOS | Delay |

Mitigations are shown in Figure 41.
Figure 41 - CR 519/CR 620 Mitigation


CR 519 at Foul Rift Road
At this intersection, it was assumed that approximately half of the vehicular traffic generated by site 12 would be routed through Foul Rift Road, causing the intersection to fail in Build condition. If full buildout were realized, this intersection would require signalization and significant investment, and still operate at LOS F with lower delays. The full mitigated configuration of this intersection would be an eastbound left turn lane and left/right turn lane, northbound double left and double through lanes, and southbound double through and double right lanes.

Mitigations are shown in Figure 42.
Table 15-CR 519/Foul Rift Road LOS and Delay (seconds)

| CR 519 at Foul Rift Road | $\begin{gathered} 2045 \text { Build - } \\ \text { AM } \\ \hline \end{gathered}$ |  | $\begin{gathered} 2045 \text { Build - } \\ \text { PM } \\ \hline \end{gathered}$ |  |  | 2045 Build Improved AM |  | 2045 Build Improved PM |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | LOS | Delay | LOS | Delay |  | LOS | Delay | LOS | Delay |
| Current configuration | F | ** | F | 4661.1 | Signalize and add a lane NB and SB | F | 408 | F | 481 |
|  |  |  |  |  | Signalize and add lane EB and three lanes NB and SB to allow double turn lanes | F | 305.3 | F | 127.2 |

**Delay not calculable - delay is outside the high boundary and cannot be computed.
Figure 42 - CR 519/Foul Rift Road Mitigation


CR 519/CR 626
Signalization alone offers a modest improvement in operations at this location in the PM (Table 16). This intersection would require significant widening to meaningfully improve operations in the Build condition. Widening the westbound approach to a left and right lane, northbound to though and through/right lanes, and southbound to a through/left and two additional through lanes would offer significant operational improvement.

Table 16 - CR 519/CR 626 LOS and Delay (seconds)

| CR 519 and CR <br> 626 | 2045 Build - <br> AM |  | 2045 Build - <br> PM |  |  | 2045 Build <br> Improved AM |  | 2045 Build <br> Improved PM |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | LOS | Delay | LOS | Delay |  | FOS | Delay | LOS | Delay |
| Current <br> configuration | F | 1232.1 | F | 471.2 | Signalize | 1279.8 | F | 334.5 |  |
|  |  |  |  |  | Signalize and <br> add a lane WB <br> and NB, add <br> two lanes SB | D | 38.9 | A | 5.9 |

Mitigations are shown in Figure 43.
Figure 43 - CR 519/CR 626 Mitigation


CR 519/CR 622 (Roxburg Station Road)
At this intersection, it was assumed that approximately half of the vehicular traffic generated by site 12 would be routed through Roxburg Station Road, causing the intersection to fail in Build condition. If full buildout were realized, this intersection would require signalization and significant investment, and still operate at LOS F with lower delays. The full mitigated configuration of this intersection would be eastbound left/through and right lane, westbound one lane for all movements, northbound left, through, and through/right lanes, and southbound left, double through, and right lanes. A slight realignment may be needed to remove the offset of Roxburg Station Road.

Mitigations are shown in Figure 44.
Table 17-CR 519/CR 622 LOS and Delay(seconds)

| CR 519 at CR | 2045 Build AM |  | 2045 Build PM |  |  | 2045 Build Improved AM |  | 2045 Build Improved PM |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 622 | LOS | Delay | LOS | Delay |  | LOS | Delay | LOS | Delay |
| Current configuration | F | ** | F | ** | Signalize and add a lane NB and SB, add lane EB | F | 422 | F | 608 |
|  |  |  |  |  | Signalize and add lane EB, two lanes NB three lanes SB | F | 294.7 | F | 565.3 |

**Delay not calculable - delay is outside the high boundary and cannot be computed.
Figure 44 - CR 519/CR 622 Mitigation


CR 519/CR 621 (Brainards Road)
At this intersection the Build condition is LOS F in both peak hours with incalculable delay in the AM peak hour. Signalization and mainline widening offer some improvement in delay although the intersection will still operate at LOS F. Further widening at the intersection improves delay significantly, but still results in LOS F. The full mitigated configuration would be eastbound left and right turn lanes, northbound double left and double through lanes, and southbound through and through/right lanes.

Table 18-CR 519/CR 621 LOS and Delay (seconds)

| CR 519 at CR 621 | $\begin{gathered} 2045 \text { Build - } \\ \text { AM } \end{gathered}$ |  | 2045 Build PM |  |  | $\begin{gathered} 2045 \text { Build } \\ \text { Improved AM } \end{gathered}$ |  | 2045 Build Improved PM |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | LOS | Delay | LOS | Delay |  | LOS | Delay | LOS | Delay |
| Current configuration | F | ** | F | 4558 | Signalize and add two lanes NB and one lane SB | F | 1057 | F | 400 |
|  |  |  |  |  | Signalize and add lane EB, three lanes NB, one lane SB | F | 507 | F | 340 |

**Delay not calculable - delay is outside the high boundary and cannot be computed.

At this intersection, the largest trucks currently cannot complete northbound left turns, southbound right turns, or eastbound left turns without crossing the double yellow centerline. Pulling back the stop bar at the eastbound approach would alleviate those encroachments.

Mitigations are shown in Figure 45.
Figure 45 - CR 519/CR 621 Mitigation


CR 519/CR 647
The proposed CR 519 mainline widening would add an additional northbound and southbound lane to this intersection.

Mitigations are shown in Figure 46.
Figure 46 - CR 519/CR 647 Mitigation


CR 519/CR 646
This intersection represents the southern limit of where mainline widening would be required to accommodate additional volume. Signalizing the intersection and adding one lane southbound to include a left turn lane would significantly improve delay, though still operate at LOS F. The resulting intersection would be one lane eastbound and northbound to accommodate all movements, and southbound left and through lanes.

Table 19 - CR 519/CR 646 LOS and Delay (seconds)

| CR 519 at CR <br> 646 | 2045 Build - <br> AM |  | 2045 Build - <br> PM |  |  | 2045 Build <br> Improved AM |  | 2045 Build <br> Improved PM |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | LOS | Delay | LOS | Delay |  | LOS | Delay | LOS | Delay |
| Current <br> configuration | F | 2835 | F | 1295 | Signalize and <br> add SB left turn <br> lane | F | 315 | F | 91 |

Currently, large trucks cannot complete northbound right turns or southbound left turns without encroachment into opposing lanes or shoulders. Pulling the northbound and southbound stop bars back when designing the intersection widening would alleviate the current turning encroachments into opposing lanes.

Mitigations are shown in Figure 47.
Figure 47 - CR 519/CR 646 Mitigation


CR 519/NJ 57
This intersection is currently signalized and would deteriorate significantly in the Build condition. NJDOT is currently redesigning the intersection to include dedicated left turn lanes and shared through/right lanes in each direction. This mitigation, when complete, would improve LOS significantly in the AM and cut delays in the PM.

Mitigations are shown in Figure 48.
Table 20 - CR 519/NJ 57 LOS and Delay (seconds)

| CR 519 at NJ 57 | 2045 Build AM |  | 2045 Build PM |  |  | 2045 BuildImproved AM |  | 2045 Build Improved PM |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | LOS | Delay | LOS | Delay |  | LOS | Delay | LOS | Delay |
| Current configuration | F | 81.5 | F | 157.5 | NJDOT design: left turn lane and through/right all approaches | C | 28.7 | F | 99.3 |

Figure 48 - CR 519/NJ 57 Mitigation


CR 519/Strykers Road
This intersection deteriorates slightly in the Build Condition. Signalizing the intersection improves operations.
Table 21 - CR 519/Strykers Road LOS and Delay (seconds)

| CR 519 at | $\begin{gathered} 2045 \text { Build - } \\ \text { AM } \end{gathered}$ |  | $\begin{gathered} 2045 \text { Build - } \\ \text { PM } \end{gathered}$ |  |  | 2045 BuildImproved AM |  | $\begin{aligned} & 2045 \text { Build } \\ & \text { Improved PM } \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Strykers Road | LOS | Delay | LOS | Delay |  | LOS | Delay | LOS | Delay |
| Current configuration | A | 7.9 | F | 64.6 | Signalize | A | 9.7 | D | 38.6 |

Mitigations are shown in Figure 49.
Figure 49-CR 519/Strykers Road Mitigation


## I-78/CR 632

The addition of a signal at the end of the ramp from I-78 eastbound to CR 632 improves operations significantly (Table 22). This would require coordination with NJDOT as this intersection is NJDOT jurisdiction.
Table 22 - I-78/CR 632 LOS and Delay (seconds)

| 1-78 ramp at | 2045 Build AM |  | 2045 Build PM |  |  | 2045 Build Improved AM |  | 2045 Build Improved PM |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CR 632 | LOS | Delay | LOS | Delay |  | LOS | Delay | LOS | Delay |
| Current configuration | F | 465.4 | A | 7.2 | Signalize | D | 41.9 | B | 10.5 |

This ramp geometry currently prevents eastbound right turns and northbound left turns for the largest trucks. The signalization design should consider truck turning radii and widen that lane if advanced.

Mitigations are shown in Figure 50.
Figure 50-I-78/CR 632 Mitigation


## NJ 31/CR 632

Northbound left and right turns, southbound right turns, and westbound right turns cannot be completed by large trucks without encroachment into opposing lanes or shoulders. Pushing back stop bars would improve conditions and would require coordination with NJDOT, as this signal is under their jurisdiction.

Mitigations are shown in Figure 51.
Figure 51 - NJ 31/CR 632 Mitigation


## INTERSECTION SAFETY IMPROVEMENTS

In addition to capacity concerns, several intersections were identified as high crash locations that should be further explored to determine if improvements related to safety as outlined below are warranted.

US 22 Phillipsburg
US 22 near this area has three lanes in each direction with frequent driveways which may be causing the overrepresentation of right-angle crashes. Opportunities to consolidate driveways should be explored to improve safety.

## US 46/NJ 182/CR 517/CR 604

This wide, skewed intersection has several movements that behave like through movements even though it is a turn. Overrepresentation of right-angle crashes may be mitigated by realigning the US 46 westbound approach closer to perpendicular and curbing the reclaimed area. This intersection is under NJDOT jurisdiction and would require further study and coordination between County and State officials.

## US 22/CR 638/CR 519

This intersection has been the subject of many studies over the years. It experiences an overrepresentation of same direction sideswipes, and same direction rear-ends. Southbound to westbound slip lane enters the roadway very quickly and may be causing sideswipe crashes. Additional acceleration distance may reduce crashes. Rear ends may be caused by the short roadway distance available for vehicles to queue between the two directions of US 22. Any geometric or signal timings changes aimed at reducing crashes at this intersection would require further study.
US 22/CR 646
This unsignalized intersection is overrepresented in same direction rear ends, striking fixed object, and striking parked vehicle and is an area of transition from high speeds on US 22 into a residential neighborhood. This change to residential area is likely the reason for striking parked vehicles; and the change in speeds may be responsible for rear end crashes. Improving signage from US 22 to signify the change into a residential neighborhood may mitigate crashes. Tightening the curve from US 22 westbound on CR 646 northbound would slow speeds and improve safety.

## TRANSPORTATION DEMAND MANAGEMENT (TDM) STRATEGIES

Transportation Demand Management (TDM) provides solutions that focus on creating a more efficient transportation network through targeted policies and strategies focused on demand. These strategies are optimal in locations where existing constraints limit physical improvements or where funding for capital improvements is not available or feasible.

TDM strategies specific to freight and warehousing developments have been utilized within New Jersey and throughout the region, particularly in locations with substantial growth in warehousing and distribution centers. A series of potential TDM strategies specific to freight are included below.

## - Identify potential rail connections to reduce the reliance entirely on truck trips.

For facilities where rail access exists, goods that are less time-sensitive may be able to be moved via rail. This solution can be utilized on longer distance trips where the cost of moving goods by rail may result in a cost savings.

- Promote non-peak trips where possible.

Shifting deliveries to off-peak periods will reduce the impact of trucks during peak congested period. This can also benefit the trucking industry by allowing drivers to achieve more consistent trip times. Moving operations to non-peak periods can also reduce the impact of traffic generated by facility employees as well.

- Stagger worker shifts to reduce congestion during peak times.

Staggering employee shifts for individual facilities can reduce congestion associated with a specific location and adjacent roadways/intersections.

- Promote development adjacent to key regional highways.

Encouraging large scale developments that generate truck trips to locate near or adjacent to major regional highways will substantially reduce impacts on local and county roadways.

- Promote requirements that developers fund their "fair share" of necessary infrastructure improvements Where traffic impacts can be identified and quantified, developers can be held to a "fair share" standard that requires they fund necessary transportation improvements required due to traffic impacts from a
proposed facility. These requirements should be explicitly detailed within all applicable municipal, county, and state regulations and ordinances.
- Create a county-wide freight transportation advisory group

Freight uses often exist in clusters and given the amount of regionally significant traffic they generate, a county-wide freight advisory group would help support the common needs and concerns of the goods movement industry. This advisory group should, at a minimum, include key industry partners, county or municipal representatives, as well as citizen advocates. Collectively, such a group would report on these issues to county planning staff.

- Encourage facility operators to promote specific trip paths/routing

Facility operators should work with their drivers to identify and promote optimal routes between a facility and major highways. Providing consistent information to drivers will result in more consistent travel times, while also limiting impacts on local communities from trucks on routes whose design may limit circulation for larger vehicles.

- Promote use of alternative transportation modes, including worker shuttles or microtransit

To reduce impacts from employee traffic related to a facility, user shuttles or microtransit options, often working with county transportation authorities, may be a viable alternative. Further, such transportation options may provide improved mobility for employees that may not have access to a personal motor vehicle.

## IMPLEMENTATION

The results of this study provide information with which to mitigate the effects of freight and freight-related traffic. The mitigation measures represent the most appropriate remedies for the area. They consider the safety of all travelers and the needs of people and businesses to ship and receive goods. The application of the mitigation measures is projected to improve congestion and mitigate the negative effects of siterelated traffic. However, it is not the end of the process.

Each mitigation measure would require additional study, engineering, funding and acceptance from various stakeholders and agencies. An evaluation of existing road widths, available right of way, and required additional right of way necessary to construct the potential improvements would require further study. Extensive right-of-way acquisition may be required in many locations to accommodate needed roadway capacity.

It is noted that road widening may be prohibited on roadways and intersections that are adjacent to the Highlands Preservation Area boundary and may affect how widening concepts are advanced. Approval or waivers from the Highlands Council may be necessary to advance many of the improvements needed to maintain acceptable levels of service. To explore these measures, coordination will be required between Warren County, Highlands Council, the involved municipalities, developers, NJDOT, and the North Jersey Transportation Planning Authority.

## CONCLUSION

Warren County's proximity to Interstates 78 and 80 position the County as a desirable center for warehouse development and freight/goods movement. As a result of its location in the region and availability of large parcels of land zoned for industrial use, there is an increased interest in warehousing and distribution development.

This study evaluated a build-out scenario of property zoned for industrial use at 15 sites in Warren County. The potential long-term impacts of such development in the County would be substantial, particularly along the CR 519 corridor. The increase in automobile and truck traffic volumes that would be anticipated if all 15 light industrial sites studied were developed would have a major impact on the County roadway network. The traffic increase is largely driven by the increase in automobiles that are expected to result from increased employment at these sites. Roadway levels of service would deteriorate to unacceptable conditions at most analyzed intersection locations and mainline segments of CR 519, as well as other key intersections throughout the County. In addition, the existing physical configuration at some intersections is challenging for trucks to complete turns without lane or shoulder encroachments which would be further impacted with an increase in truck traffic in the future.

TDM strategies can be used to reduce the demand on the roadway network; however, TDM strategies alone would not be enough to maintain traffic operations at an acceptable level should all sites studied be developed for industrial use. Necessary improvements to County roadways and intersections to maintain traffic operations at an acceptable level of service would require further detailed study as development projects are proposed. Future studies will need to identify locations where there are roadway right-of-way constraints that will require property acquisition for roadway widening for capacity improvements and/or to alleviate lane encroachments by turning trucks. Acquisition costs and Highland Preservation Area restrictions may be a consideration for the implementation of any required widening improvements in Warren County, particularly along CR 519.

## APPENDIX A - ZONING AND TRIP GENERATION





## APPENDIX B - MODEL VOLUME CHANGES

Figure 1 - AM Peak Volume Change


Figure 2 - PM Peak Volume Change


| CR 519 Belvidere Rd \& CR 620 Belvidere Rd-Peak Hour Volumes |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morning Peak |  |  |  |  |  |  |
|  | CR 519 Belvidere Rd |  | CR 620 Belvidere Rd |  | CR 519 |  |
| Scenario | NBT | NBR | SBL | SBT | WBL | WBR |
| 2020 Existing | 213 | 288 | 14 | 224 | 240 | 14 |
| 2045 No Build | 247 | 334 | 16 | 260 | 278 | 16 |
| 2045 Build | 937 | 333 | 16 | 1927 | 1668 | 94 |

## CR 519 Belvidere Rd \& CR 620 Belvidere Rd-Peak Hour Volumes

Evening Peak

|  | $C R 519$ <br> Belvidere <br> $R d$ |  | $C R 620$ Belvidere <br> $R d$ |  | WR 519 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Scenario | NBT |  | NBR | SBL | SBT | WBL |
| 2020 Existing | 322 | 364 | 10 | 269 | 349 | 14 |
| 2045 No Build | 374 | 423 | 12 | 312 | 405 | 16 |
| 2045 Build | 2484 | 1422 | 11 | 840 | 404 | 641 |

CR 519 Belvidere Rd \& CR 621 Brainards Rd-Peak Hour Volumes
Morning Peak

|  | CR 519 Belvidere Rd |  |  |  | CR 621 Brainards Rd |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Scenario | NBL | NBT | SBT | SBR | EBL | EBR |
| Existing | 56 | 401 | 432 | 9 | 9 | 68 |
| No Build | 65 | 465 | 501 | 10 | 10 | 78 |
| Build | 1868 | 1577 | 501 | 269 | 1448 | 141 |

CR 519 Belvidere Rd \& CR 621 Brainards Rd-Peak Hour Volumes

| Evening Peak |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | CR 519 Belvidere Rd |  |  |  | CR 621 Brainards Rd |  |
| Scenario | NBL | NBT | SBT | SBR | EBL | EBR |
| Existing | 121 | 473 | 503 | 10 | 18 | 83 |
| No Build | 141 | 549 | 584 | 12 | 20 | 96 |
| Build | 236 | 549 | 1028 | 511 | 108 | 1846 |


| Morning Peak |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | CR 519 Belvidere Rd |  |  |  |  |  | Roxburg Station Rd |  |  | Roxburg Hill Rd |  |  |
| Scenario | NBL | NBT | NBR | SBL | SBT | SBR | EBL | EBT | EBR | WBL | WBT | WBR |
| Existing | 10 | 498 | 4 | 1 | 466 | 14 | 20 | 1 | 8 | 9 | 1 | 13 |
| No Build | 12 | 577 | 4 | 1 | 540 | 16 | 23 | 1 | 9 | 10 | 1 | 15 |
| Build | 1319 | 1928 | 5 | 1 | 729 | 1856 | 236 | 1 | 21 | 10 | 64 | 15 |
| CR 519 Belvidere Rd \& CR 622 Roxburg Station Rd/CR 622 Roxburg Hill Rd-Peak Hour Volumes |  |  |  |  |  |  |  |  |  |  |  |  |
| Evening Peak |  |  |  |  |  |  |  |  |  |  |  |  |
|  | CR 519 Belvidere Rd |  |  |  |  |  | Roxburg Station Rd |  |  | Roxburg Hill Rd |  |  |
| Scenario | NBL | NBT | NBR | SBL | SBT | SBR | EBL | EBT | EBR | WBL | WBT | WBR |
| Existing | 15 | 562 | 4 | 5 | 432 | 23 | 25 | 1 | 29 | 5 | 1 | 1 |
| No Build | 18 | 651 | 4 | 6 | 501 | 26 | 29 | 1 | 34 | 6 | 1 | 1 |
| Build | 18 | 651 | 5 | 1430 | 500 | 589 | 713 | 538 | 1284 | 6 | 1 | 1 |


| Morning Peak |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | CR 519 UniontownRd |  | CR 646 Belvidere Rd |  | CR 519 Belvidere Rd |  |
| Scenario | NBL | NBR | NET | NER | SWL | SWT |
| Existing | 3 | 168 | 307 | 9 | 289 | 286 |
| No Build | 3 | 195 | 356 | 10 | 335 | 331 |
| Build | 3 | 838 | 1307 | 10 | 336 | 478 |

CR 646 Belvidere Rd/CR 519 Belvidere Rd \& CR 519 Uniontown Rd-Peak Hour Volumes
Evening Peak

|  | CR 519 Uniontown Rd |  | CR 646 Belvidere Rd |  | CR 519 Belvidere Rd |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PM | NBL | NBR | NET | NER | SWL | SWT |
| Existing | 13 | 326 | 317 | 5 | 241 | 320 |
| No Build | 15 | 378 | 367 | 6 | 280 | 371 |
| Build | 15 | 378 | 398 | 6 | 780 | 1482 |

CR 620 Belvidere Rd \& Foul Lift Rd-Peak Hour Volumes
Morning Peak

|  | CR 620 Belvidere $R d$ |  |  |  | Foul Rift Rd |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Scenario | NBL | NBT | SBT | SBR | EBL | EBR |  |
| Existing | 0 | 481 | 540 | 8 | 5 | 0 |  |
| No Build | 0 | 558 | 626 | 9 | 6 | 0 |  |
| Build | 938 | 1253 | 2042 | 2009 | 813 | 63 |  |

CR 620 Belvidere Rd \& Foul Lift Rd-Peak Hour Volumes

| Evening Peak |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
|  | CRelvidere Rd |  |  |  |  |  |  |
| Scenario | NBL | NBT | SBT | SBR | EBL | EBR |  |
| Existing | 3 | 554 | 588 | 9 | 4 | 1 |  |
| No Build | 3 | 643 | 682 | 10 | 4 | 1 |  |
| Build | 3 | 1254 | 1182 | 573 | 1379 | 1251 |  |

CR 519 Uniontown Rd \& NJ 57-Peak Hour Volumes

| Morning Peak |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | NJ 57 |  |  |  | CR 519 Uniontown Rd |  |  |  |
| Scenario | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT |
| Existing | 29 | 307 | 24 | 250 | 31 | 79 | 3 | 101 |
| No Build | 29 | 307 | 24 | 250 | 31 | 79 | 3 | 101 |
| Build | 284 | 356 | 28 | 290 | 36 | 330 | 3 | 125 |

CR 519 Uniontown Rd \& NJ 57-Peak Hour Volumes

| Evening Peak |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
|  | NJ 57 |  |  |  | CR 519 Uniontown Rd |  |  |  |
| Scenario | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT |
| Existing | 27 | 228 | 82 | 277 | 29 | 213 | 3 | 124 |
| No Build | 27 | 228 | 82 | 277 | 29 | 213 | 3 | 124 |
| Build | 31 | 264 | 145 | 571 | 34 | 295 | 3 | 294 |

CR 519 Uniontown Rd \& Strykers Rd-Peak Hour Volumes

| Morning Peak |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
|  | CR 519 Uniontown Rd |  |  |  |  | Strykers Rd |  |
| Scenario | NBL | NBT | SBT | SBR | EBL | EBR |  |
| Existing | 96 | 142 | 247 | 73 | 110 | 266 |  |
| No Build | 112 | 165 | 286 | 84 | 128 | 309 |  |
| Build | 111 | 483 | 362 | 84 | 128 | 282 |  |

CR 519 Uniontown Rd \& Strykers Rd-Peak Hour Volumes

| Evening Peak |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | CR 519 Uniontown Rd |  |  |  | Strykers Rd |  |
| Scenario | NBL | NBT | SBT | SBR | EBL | EBR |
| Existing | 231 | 356 | 337 | 130 | 144 | 179 |
| No Build | 268 | 412 | 391 | 151 | 167 | 207 |
| Build | 239 | 527 | 618 | 151 | 166 | 223 |

## APPENDIX C - TURNING RADII ANALYSIS



## APPENDIX D - CAPACITY ANALYSIS

# 2020 EXISTING CONDITIONS ANALYSIS <br> INTERSECTION ANALYSIS MID-BLOCK ANALYSIS <br> 2045 NO-BUILD ANALYSIS <br> INTERSECTION ANALYSIS MID-BLOCK ANALYSIS <br> <br> 2045 BUILD ANALYSIS <br> <br> 2045 BUILD ANALYSIS <br> INTERSECTION ANALYSIS MID-BLOCK ANALYSIS 

## 2045 BUILD MITIGATION ANALYSIS

INTERSECTION ANALYSIS

## 2020 EXISTING INTERSECTION ANALYSIS

|  | 4 |  |  |  |  |  |  | $\dagger$ | 7 | $\downarrow$ | $\frac{1}{7}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ | 「 |  | $\uparrow$ | F |
| Traffic Volume (vph) | 20 | 241 | 22 | 48 | 161 | 39 | 31 | 206 | 58 | 84 | 158 | 19 |
| Future Volume (vph) | 20 | 241 | 22 | 48 | 161 | 39 | 31 | 206 | 58 | 84 | 158 | 19 |
| Satd. Flow (prot) | 0 | 1835 | 0 | 0 | 1800 | 0 | 0 | 1848 | 1583 | 0 | 1833 | 1583 |
| Flt Permitted |  | 0.958 |  |  | 0.870 |  |  | 0.883 |  |  | 0.654 |  |
| Satd. Flow (perm) | 0 | 1765 | 0 | 0 | 1580 | 0 | 0 | 1645 | 1583 | 0 | 1218 | 1583 |
| Satd. Flow (RTOR) |  | 10 |  |  | 25 |  |  |  | 70 |  |  | 61 |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.71 | 0.76 | 0.69 | 0.80 | 0.77 | 0.65 | 0.78 | 0.94 | 0.85 | 0.91 | 0.84 | 0.53 |
| Growth Factor | 103\% | 103\% | 103\% | 103\% | 103\% | 103\% | 103\% | 103\% | 103\% | 103\% | 103\% | 103\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 389 | 0 | 0 | 339 | 0 | 0 | 267 | 70 | 0 | 289 | 37 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA | Perm | Perm | NA | Perm |
| Protected Phases |  |  |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Total Split (s) | 47.0 | 47.0 |  | 47.0 | 47.0 |  | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 |
| Total Lost Time (s) |  | 7.0 |  |  | 7.0 |  |  | 5.0 | 5.0 |  | 5.0 | 5.0 |
| Act Effct Green (s) |  | 40.0 |  |  | 40.0 |  |  | 20.0 | 20.0 |  | 20.0 | 20.0 |
| Actuated g/C Ratio |  | 0.56 |  |  | 0.56 |  |  | 0.28 | 0.28 |  | 0.28 | 0.28 |
| v/c Ratio |  | 0.39 |  |  | 0.38 |  |  | 0.59 | 0.14 |  | 0.86 | 0.08 |
| Control Delay |  | 10.3 |  |  | 9.8 |  |  | 28.6 | 6.5 |  | 50.8 | 3.2 |
| Queue Delay |  | 0.0 |  |  | 0.0 |  |  | 0.0 | 0.0 |  | 0.0 | 0.0 |
| Total Delay |  | 10.3 |  |  | 9.8 |  |  | 28.6 | 6.5 |  | 50.8 | 3.2 |
| LOS |  | B |  |  | A |  |  | C | A |  | D | A |
| Approach Delay |  | 10.3 |  |  | 9.8 |  |  | 24.0 |  |  | 45.4 |  |
| Approach LOS |  | B |  |  | A |  |  | C |  |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length: 72
Actuated Cycle Length: 72
Control Type: Semi Act-Uncoord
Maximum v/c Ratio: 0.86
Intersection Signal Delay: 21.7
Intersection LOS: C
Intersection Capacity Utilization 73.8\%
ICU Level of Service D
Analysis Period (min) 15
Splits and Phases: 3: RT 519 \& US 46


|  | 4 |  |  |  |  |  |  | $\dagger$ | 7 | $\downarrow$ | $\frac{1}{7}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ | 「 |  | $\uparrow$ | F |
| Traffic Volume (vph) | 23 | 168 | 17 | 32 | 270 | 63 | 35 | 169 | 44 | 99 | 179 | 36 |
| Future Volume (vph) | 23 | 168 | 17 | 32 | 270 | 63 | 35 | 169 | 44 | 99 | 179 | 36 |
| Satd. Flow (prot) | 0 | 1829 | 0 | 0 | 1801 | 0 | 0 | 1846 | 1583 | 0 | 1827 | 1583 |
| Flt Permitted |  | 0.933 |  |  | 0.955 |  |  | 0.701 |  |  | 0.622 |  |
| Satd. Flow (perm) | 0 | 1715 | 0 | 0 | 1727 | 0 | 0 | 1306 | 1583 | 0 | 1159 | 1583 |
| Satd. Flow (RTOR) |  | 12 |  |  | 31 |  |  |  | 61 |  |  | 61 |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.84 | 0.80 | 0.65 | 0.88 | 0.91 | 0.69 | 0.73 | 0.83 | 0.75 | 0.76 | 0.85 | 0.68 |
| Growth Factor | 103\% | 103\% | 103\% | 103\% | 103\% | 103\% | 103\% | 103\% | 103\% | 103\% | 103\% | 103\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 271 | 0 | 0 | 437 | 0 | 0 | 259 | 60 | 0 | 351 | 55 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA | Perm | Perm | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Total Split (s) | 47.0 | 47.0 |  | 47.0 | 47.0 |  | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 |
| Total Lost Time (s) |  | 7.0 |  |  | 7.0 |  |  | 5.0 | 5.0 |  | 5.0 | 5.0 |
| Act Effct Green (s) |  | 40.0 |  |  | 40.0 |  |  | 20.0 | 20.0 |  | 20.0 | 20.0 |
| Actuated g/C Ratio |  | 0.56 |  |  | 0.56 |  |  | 0.28 | 0.28 |  | 0.28 | 0.28 |
| v/c Ratio |  | 0.28 |  |  | 0.45 |  |  | 0.72 | 0.12 |  | 1.09 | 0.11 |
| Control Delay |  | 9.0 |  |  | 10.5 |  |  | 36.7 | 6.6 |  | 106.7 | 6.1 |
| Queue Delay |  | 0.0 |  |  | 0.0 |  |  | 0.0 | 0.0 |  | 0.0 | 0.0 |
| Total Delay |  | 9.0 |  |  | 10.5 |  |  | 36.7 | 6.6 |  | 106.7 | 6.1 |
| LOS |  | A |  |  | B |  |  | D | A |  | F | A |
| Approach Delay |  | 9.0 |  |  | 10.5 |  |  | 31.1 |  |  | 93.1 |  |
| Approach LOS |  | A |  |  | B |  |  | C |  |  | F |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length: 72
Actuated Cycle Length: 72
Control Type: Semi Act-Uncoord
Maximum v/c Ratio: 1.09
Intersection Signal Delay: 38.2
Intersection LOS: D
Intersection Capacity Utilization 74.0\%
ICU Level of Service D
Analysis Period (min) 15
Splits and Phases: 3: RT 519 \& US 46


| Intersection |  |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 14.8 |  |
| Intersection LOS | B |  |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ |  |  | ¢ |  |  | ¢ |  |  | ¢ |  |
| Traffic Vol, veh/h | 48 | 149 | 8 | 36 | 90 | 32 | 5 | 169 | 44 | 30 | 109 | 30 |
| Future Vol, veh/h | 48 | 149 | 8 | 36 | 90 | 32 | 5 | 169 | 44 | 30 | 109 | 30 |
| Peak Hour Factor | 0.92 | 0.80 | 0.92 | 0.92 | 0.80 | 0.92 | 0.92 | 0.80 | 0.92 | 0.92 | 0.80 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 63 | 225 | 11 | 47 | 136 | 42 | 7 | 256 | 58 | 39 | 165 | 39 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 15.7 |  |  | 13.4 |  |  | 15.8 |  |  | 13.7 |  |  |
| HCM LOS | C |  |  | B |  |  | C |  |  | B |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $2 \%$ | $23 \%$ | $23 \%$ | $18 \%$ |
| Vol Thru, \% | $78 \%$ | $73 \%$ | $57 \%$ | $64 \%$ |
| Vol Right, \% | $20 \%$ | $4 \%$ | $20 \%$ | $18 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 218 | 205 | 158 | 169 |
| LT Vol | 5 | 48 | 36 | 30 |
| Through Vol | 169 | 149 | 90 | 109 |
| RT Vol | 44 | 8 | 32 | 30 |
| Lane Flow Rate | 320 | 299 | 226 | 244 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.534 | 0.515 | 0.393 | 0.421 |
| Departure Headway (Hd) | 6.008 | 6.202 | 6.275 | 6.212 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 599 | 580 | 573 | 578 |
| Service Time | 4.055 | 4.251 | 4.328 | 4.262 |
| HCM Lane V/C Ratio | 0.534 | 0.516 | 0.394 | 0.422 |
| HCM Control Delay | 15.8 | 15.7 | 13.4 | 13.7 |
| HCM Lane LOS | C | C | B | B |
| HCM 95th-tile Q | 3.2 | 2.9 | 1.9 | 2.1 |


| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 24.1 |
| Intersection LOS | C |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | * |  |  | * |  |  | * |  |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 31 | 114 | 13 | 41 | 206 | 31 | 22 | 111 | 31 | 43 | 181 | 52 |
| Future Vol, veh/h | 31 | 114 | 13 | 41 | 206 | 31 | 22 | 111 | 31 | 43 | 181 | 52 |
| Peak Hour Factor | 0.92 | 0.80 | 0.92 | 0.92 | 0.80 | 0.92 | 0.92 | 0.80 | 0.92 | 0.92 | 0.80 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 41 | 172 | 17 | 54 | 312 | 41 | 29 | 168 | 41 | 57 | 274 | 68 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 16.8 |  |  | 29.1 |  |  | 16.8 |  |  | 27.7 |  |  |
| HCM LOS | C |  |  | D |  |  | C |  |  | D |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $13 \%$ | $20 \%$ | $15 \%$ | $16 \%$ |
| Vol Thru, \% | $68 \%$ | $72 \%$ | $74 \%$ | $66 \%$ |
| Vol Right, \% | $19 \%$ | $8 \%$ | $11 \%$ | $19 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 164 | 158 | 278 | 276 |
| LT Vol | 22 | 31 | 41 | 43 |
| Through Vol | 111 | 114 | 206 | 181 |
| RT Vol | 31 | 13 | 31 | 52 |
| Lane Flow Rate | 238 | 230 | 406 | 399 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.478 | 0.469 | 0.768 | 0.752 |
| Departure Headway (Hd) | 7.247 | 7.334 | 6.807 | 6.792 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 497 | 491 | 532 | 530 |
| Service Time | 5.313 | 5.403 | 4.863 | 4.848 |
| HCM Lane V/C Ratio | 0.479 | 0.468 | 0.763 | 0.753 |
| HCM Control Delay | 16.8 | 16.8 | 29.1 | 27.7 |
| HCM Lane LOS | C | C | D | $D$ |
| HCM 95th-tile Q | 2.5 | 2.5 | 6.8 | 6.5 |





HCM Unsignalized Intersection Capacity Analysis
3: CR 519 Belvidere Rd \& Foul Lift Rd


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.4 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | $\uparrow$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 8 | 10 | 427 | 1 | 11 | 366 |
| Future Vol, veh/h | 8 | 10 | 427 | 1 | 11 | 366 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, $\#$ | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 80 | 80 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 10 | 13 | 469 | 1 | 12 | 402 |


| Major/Minor M | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 896 | 470 | 0 | 0 | 470 | 0 |
| Stage 1 | 470 | - | - | - | - | - |
| Stage 2 | 426 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 | - |
| Pot Cap-1 Maneuver | 311 | 594 | - | - | 1092 | - |
| Stage 1 | 629 | - | - | - | - | - |
| Stage 2 | 659 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 307 | 594 | - | - | 1092 | - |
| Mov Cap-2 Maneuver | 307 | - | - | - | - | - |
| Stage 1 | 629 | - | - | - | - | - |
| Stage 2 | 650 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 14.1 |  | 0 |  | 0.2 |  |
| HCM LOS | B |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 420 | 1092 | - |
| HCM Lane V/C Ratio |  | - | - | 0.054 | 0.011 | - |
| HCM Control Delay (s) |  | - | - | 14.1 | 8.3 | 0 |
| HCM Lane LOS |  | - | - | B | A | A |
| HCM 95th \%tile Q(veh) |  | - | - | 0.2 | 0 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.7 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | $\uparrow$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 16 | 12 | 474 | 0 | 18 | 511 |
| Future Vol, veh/h | 16 | 12 | 474 | 0 | 18 | 511 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, $\#$ | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 80 | 80 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 20 | 15 | 520 | 0 | 20 | 561 |


| Major/Minor | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1121 | 520 | 0 | 0 | 520 | 0 |
| Stage 1 | 520 |  | - | - | - | - |
| Stage 2 | 601 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 |  | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 | - |
| Pot Cap-1 Maneuver | 228 | 556 | - | - | 1046 | - |
| Stage 1 | 597 | - | - | - | - | - |
| Stage 2 | 547 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 222 | 556 | - | - | 1046 | - |
| Mov Cap-2 Maneuver | 222 | - | - | - | - | - |
| Stage 1 | 597 | - | - | - | - | - |
| Stage 2 | 532 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 18.6 |  | 0 |  | 0.3 |  |
| HCM LOS | C |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 299 | 1046 | - |
| HCM Lane V/C Ratio |  | - | - | 0.118 | 0.019 | - |
| HCM Control Delay (s) |  | - | - | 18.6 | 8.5 | 0 |
| HCM Lane LOS |  | - | - | C | A | A |
| HCM 95th \%tile Q(veh) |  | - | - | 0.4 | 0.1 | - |

[^1] WSP

HCM Unsignalized Intersection Capacity Analysis
3: CR 519 Belvidere Rd \& CR 622 Roxbury Station Rd/CR 622 Roxbury Hill Rd


HCM Unsignalized Intersection Capacity Analysis
3: CR 519 Belvidere Rd \& CR 622 Roxbury Station Rd/CR 622 Roxbury Hill Rd

|  | $\rangle$ |  | $\rangle$ | 7 | 4 | 4 | 4 | $\uparrow$ | 7 | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | ¢ |  |  | ¢ |  |  | ¢ |  |
| Traffic Volume (veh/h) | 20 | 1 | 23 |  | 1 | 1 | 12 | 501 | 3 | 4 | 385 | 18 |
| Future Volume (Veh/h) | 20 | 1 | 23 | 4 | 1 | 1 | 12 | 501 | 3 | 4 | 385 | 18 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.90 | 0.80 | 0.80 | 0.90 | 0.80 |
| Hourly flow rate (vph) | 25 | 1 | 29 | 5 | 1 | 1 | 15 | 562 | 4 | 5 | 432 | 23 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |

Lane Width ( ft )
Walking Speed (tt/s)
Percent Blockage

| Right turn flare $($ veh $)$ | None | None |
| :--- | :--- | :--- |
| Median type |  |  |
| Median storage veh) |  |  |

Upstream signal (ft)

| pX, platoon unblocked |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| vC , conflicting volume | 1049 | 1050 | 444 | 1077 | 1059 | 564 | 455 | 566 |
| vC1, stage 1 conf vol |  |  |  |  |  |  |  |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  |  |  |
| vCu, unblocked vol | 1049 | 1050 | 444 | 1077 | 1059 | 564 | 455 | 566 |


|  | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.6 | 4.1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| CC, single (s) |  |  |  |  |  |  |  |  |
| TC, 2 stage (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.7 | 2.2 |
| tF (s) | 87 | 100 | 95 | 97 | 100 | 100 | 98 | 100 |
| p0 queue free \% | 198 | 224 | 610 | 185 | 221 | 529 | 894 | 1016 |


| Direction, Lane \# | EB 1 | WB 1 | NB 1 | SB 1 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | :--- |
| Volume Total | 55 | 7 | 581 | 460 |  |  |
| Volume Left | 25 | 5 | 15 | 5 |  |  |
| Volume Right | 29 | 1 | 4 | 23 |  |  |
| cSH | 309 | 210 | 894 | 1016 |  |  |
| Volume to Capacity | 0.18 | 0.03 | 0.02 | 0.00 |  |  |
| Queue Length 95th (tt) | 16 | 3 | 1 | 0 |  |  |
| Control Delay (s) | 19.2 | 22.8 | 0.5 | 0.1 |  |  |
| Lane LOS | C | C | A | A |  |  |
| Approach Delay (s) | 19.2 | 22.8 | 0.5 | 0.1 |  |  |
| Approach LOS | C | C |  |  | A |  |

HCM Unsignalized Intersection Capacity Analysis
3: CR 519 Belvidere Rd \& CR 621 Brainards Rd


HCM Unsignalized Intersection Capacity Analysis
3: CR 519 Belvidere Rd \& CR 621 Brainards Rd


HCM Unsignalized Intersection Capacity Analysis
2: CR 646 Belvidere Rd/CR 519 Belvidere Rd \& CR 519 Uniontown Rd


HCM Unsignalized Intersection Capacity Analysis
2: CR 646 Belvidere Rd/CR 519 Belvidere Rd \& CR 519 Uniontown Rd


Timings
3: CR 519 Uniontown Rd \& NJ 57


Cycle Length: 90
Actuated Cycle Length: 90
Offset: 10.9 (12\%), Referenced to phase 4:EBTL and 8:WBTL, Start of Yellow
Natural Cycle: 80
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 0.61
Intersection Signal Delay: $17.8 \quad$ Intersection LOS: B
Intersection Capacity Utilization 79.1\% ICU Level of Service D
Analysis Period (min) 15
Splits and Phases: 3: CR 519 Uniontown Rd \& NJ 57


Timings
3: CR 519 Uniontown Rd \& NJ 57


Cycle Length: 90
Actuated Cycle Length: 90
Offset: 10.9 (12\%), Referenced to phase 4:EBTL and 8:WBTL, Start of Yellow
Natural Cycle: 80
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 0.79
Intersection Signal Delay: $22.9 \quad$ Intersection LOS: C
Intersection Capacity Utilization 83.8\% ICU Level of Service E
Analysis Period (min) 15

Splits and Phases: 3: CR 519 Uniontown Rd \& NJ 57




HCM Unsignalized Intersection Capacity Analysis
4: CO 632 \& I-78 WB ramp


HCM Unsignalized Intersection Capacity Analysis
4: CO 632 \& I-78 WB ramp


2020 EXISTING MID-BLOCK ANALYSIS

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, northeast of CO <br> 610 | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 3 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 9.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 253 |
| Directional Demand Flow Rate, veh/h | 298 | Total Trucks, \% | 2.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.18 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 52.6 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.17369 | Speed Power Coefficient | 0.52554 |
| PF Slope Coefficient | -1.25142 | PF Power Coefficient | 0.78453 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 2.2 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 51.2 |

## Vehicle Results

| Average Speed, mi/h | 51.2 | Percent Followers, \% | 38.4 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.17 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 2.2 |
| Vehicle LOS | A |  |  |

[^2]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, northeast of CO <br> 610 | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 3 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 9.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 298 |
| Directional Demand Flow Rate, veh/h | 253 | Total Trucks, \% | 2.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.15 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 52.6 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.18761 | Speed Power Coefficient | 0.51566 |
| PF Slope Coefficient | -1.26085 | PF Power Coefficient | 0.78175 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 1.7 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 51.4 |
|  |  |  |  |  |  |
| Vehicle Results |  |  |  |  |  |
| Average Speed, mi/h | 51.4 | Percent Followers, \% | 35.0 |  |  |
| Segment Travel Time, minutes | 1.17 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 1.7 |  |  |
| Vehicle LOS | A |  |  |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, northeast of CO <br> 610 | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |  |
| :--- | :--- | :--- | :--- | :---: |
| Lane Width, ft | 12 | Shoulder Width, ft | 3 |  |
| Speed Limit, mi/h | 50 | Access Point Density, pts/mi | 9.0 |  |
| Demand and Capacity |  |  |  |  |
| Directional Demand Flow Rate, veh/h | 263 | Opposing Demand Flow Rate, veh/h | 347 |  |
| Peak Hour Factor | Total Trucks, \% | 2.00 |  |  |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.15 |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 52.6 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.20174 | Speed Power Coefficient | 0.50607 |
| PF Slope Coefficient | -1.27002 | PF Power Coefficient | 0.77898 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 1.9 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 51.3 |
|  |  |  |  |  |  |
| Vehicle Results | 51.3 | Percent Followers, $\%$ | 36.2 |  |  |
| Average Speed, mi/h | 1.17 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 1.9 |  |  |
| Segment Travel Time, minutes | A |  |  |  |  |
| Vehicle LOS |  |  |  |  |  |

[^3]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, northeast of CO <br> 610 | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 3 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 9.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 263 |
| Directional Demand Flow Rate, veh/h | 347 | Total Trucks, \% | 2.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.20 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 52.6 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.17684 | Speed Power Coefficient | 0.52326 |
| PF Slope Coefficient | -1.25359 | PF Power Coefficient | 0.78389 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 2.9 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 51.1 |
|  |  |  |  |  |  |
| Vehicle Results | 51.1 | Percent Followers, $\%$ | 42.1 |  |  |
| Average Speed, mi/h | 1.18 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 2.9 |  |  |
| Segment Travel Time, minutes | B |  |  |  |  |
| Vehicle LOS |  |  |  |  |  |

[^4]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 17 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, Stone Hedge Rd <br> to Hope Crossing Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Constrained | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 0.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | - |
| Directional Demand Flow Rate, veh/h | 335 | Total Trucks, \% | 3.00 |
| Peak Hour Factor | 0.80 | Demand/Capacity (D/C) | 0.20 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 56.9 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.64416 | Speed Power Coefficient | 0.41674 |
| PF Slope Coefficient | -1.32222 | PF Power Coefficient | 0.75266 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 2.7 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 54.9 |
|  |  |  |  |  |  |
| Vehicle Results | 54.9 | Percent Followers, $\%$ | 44.0 |  |  |
| Average Speed, mi/h | 1.09 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 2.7 |  |  |
| Segment Travel Time, minutes | B |  |  |  |  |
| Vehicle LOS |  |  |  |  |  |

[^5]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 17 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, Stone Hedge Rd <br> to Hope Crossing Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Constrained | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 0.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | - |
| Directional Demand Flow Rate, veh/h | 336 | Total Trucks, \% | 3.00 |
| Peak Hour Factor | 0.84 | Demand/Capacity (D/C) | 0.20 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 56.9 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.64416 | Speed Power Coefficient | 0.41674 |
| PF Slope Coefficient | -1.32222 | PF Power Coefficient | 0.75266 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 2.7 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 54.9 |
|  |  |  |  |  |  |
| Vehicle Results | 54.9 | Percent Followers, \% | 44.1 |  |  |
| Average Speed, mi/h | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 2.7 |  |  |  |
| Segment Travel Time, minutes | 1.09 | B |  |  |  |
| Vehicle LOS |  |  |  |  |  |

[^6]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 17 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, Stone Hedge Rd <br> to Hope Crossing Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Constrained | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 0.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | - |
| Directional Demand Flow Rate, veh/h | 290 | Total Trucks, \% | 3.00 |
| Peak Hour Factor | 0.90 | Demand/Capacity (D/C) | 0.17 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 56.9 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.64416 | Speed Power Coefficient | 0.41674 |
| PF Slope Coefficient | -1.32222 | PF Power Coefficient | 0.75266 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 2.1 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 55.1 |
|  |  |  |  |  |  |
| Vehicle Results | 55.1 | Percent Followers, \% | 40.6 |  |  |
| Average Speed, mi/h | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 2.1 |  |  |  |
| Segment Travel Time, minutes | 1.09 | A |  |  |  |
| Vehicle LOS |  |  |  |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 17 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, Stone Hedge Rd <br> to Hope Crossing Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Constrained | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 0.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | - |
| Directional Demand Flow Rate, veh/h | 371 | Total Trucks, \% | 3.00 |
| Peak Hour Factor | 0.82 | Demand/Capacity (D/C) | 0.22 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 56.9 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.64416 | Speed Power Coefficient | 0.41674 |
| PF Slope Coefficient | -1.32222 | PF Power Coefficient | 0.75266 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 3.2 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 54.8 |
|  |  |  |  |  |  |
| Vehicle Results | 54.8 | Percent Followers, \% | 46.6 |  |  |
| Average Speed, mi/h | Followers Density, followers/mi/ln | 3.2 |  |  |  |
| Segment Travel Time, minutes | 1.10 |  |  |  |  |
| Vehicle LOS | B |  |  |  |  |

[^7]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, CO 623 Brass <br> Castle Rd to Pequest Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 4.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 388 |
| Directional Demand Flow Rate, veh/h | 493 | Total Trucks, \% | 0.00 |
| Peak Hour Factor | 0.88 | Demand/Capacity (D/C) | 0.29 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.7 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.38169 | Speed Power Coefficient | 0.49890 |
| PF Slope Coefficient | -1.26598 | PF Power Coefficient | 0.78592 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 4.8 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.6 |
|  |  |  |  |  |  |
| Vehicle Results |  |  |  |  |  |
| Average Speed, mi/h | 53.6 | Percent Followers, \% | 51.6 |  |  |
| Segment Travel Time, minutes | 1.12 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 4.8 |  |  |
| Vehicle LOS | B |  |  |  |  |

[^8]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, CO 623 Brass <br> Castle Rd to Pequest Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |  |
| :--- | :--- | :--- | :--- | :---: |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |  |
| Speed Limit, mi/h | 50 | Access Point Density, pts/mi | 4.0 |  |
| Demand and Capacity |  |  |  |  |
| Directional Demand Flow Rate, veh/h | 371 | Opposing Demand Flow Rate, veh/h | 472 |  |
| Peak Hour Factor | 0.92 | Total Trucks, \% | 0.00 |  |
| Segment Capacity, veh/h | Demand/Capacity (D/C) | 0.22 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.7 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.40278 | Speed Power Coefficient | 0.48595 |
| PF Slope Coefficient | -1.27764 | PF Power Coefficient | 0.78186 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 3.1 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.9 |
|  |  |  |  |  |  |
| Vehicle Results | 53.9 | Percent Followers, \% | 44.5 |  |  |
| Average Speed, mi/h | 1.11 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 3.1 |  |  |
| Segment Travel Time, minutes | B |  |  |  |  |
| Vehicle LOS |  |  |  |  |  |

[^9]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, CO 623 Brass <br> Castle Rd to Pequest Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 4.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 418 |
| Directional Demand Flow Rate, veh/h | 562 | Total Trucks, \% | 7.00 |
| Peak Hour Factor | 0.85 | Demand/Capacity (D/C) | 0.33 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.5 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.37685 | Speed Power Coefficient | 0.49400 |
| PF Slope Coefficient | -1.27056 | PF Power Coefficient | 0.78476 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 5.9 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.2 |
|  |  |  |  |  |  |
| Vehicle Results | 53.2 | Percent Followers, \% | 55.5 |  |  |
| Average Speed, mi/h | Followers Density, followers/mi/ln | 5.9 |  |  |  |
| Segment Travel Time, minutes | 1.13 | C |  |  |  |
| Vehicle LOS |  |  |  |  |  |

[^10]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, CO 623 Brass <br> Castle Rd to Pequest Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 4.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 503 |
| Directional Demand Flow Rate, veh/h | 374 | Total Trucks, \% | 7.00 |
| Peak Hour Factor | 0.95 | Demand/Capacity (D/C) | 0.22 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.5 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.39753 | Speed Power Coefficient | 0.48165 |
| PF Slope Coefficient | -1.28168 | PF Power Coefficient | 0.78080 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 3.1 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.6 |
|  |  |  |  |  |  |
| Vehicle Results | 53.6 | Percent Followers, \% | 44.8 |  |  |
| Average Speed, mi/h | Followers Density, followers/mi/ln | 3.1 |  |  |  |
| Segment Travel Time, minutes | 1.12 |  |  |  |  |
| Vehicle LOS | B |  |  |  |  |

[^11]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, CO 620 to <br> Brookfield Dr | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 11 | Shoulder Width, ft | 5 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 2.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 245 |
| Directional Demand Flow Rate, veh/h | 321 | Total Trucks, \% | 2.00 |
| Peak Hour Factor | 0.85 | Demand/Capacity (D/C) | 0.19 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.1 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.30909 | Speed Power Coefficient | 0.52759 |
| PF Slope Coefficient | -1.24167 | PF Power Coefficient | 0.79289 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 2.4 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.6 |
| Vehicle Results |  |  |  |  | 53.6 |
| Average Speed, mi/h | Percent Followers, \% |  |  |  |  |
| Segment Travel Time, minutes | 1.12 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 2.4 |  |  |
| Vehicle LOS | A |  |  |  |  |

[^12]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, CO 620 to <br> Brookfield Dr | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 11 | Shoulder Width, ft | 5 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 2.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 314 |
| Directional Demand Flow Rate, veh/h | 239 | Total Trucks, \% | 2.00 |
| Peak Hour Factor | 0.87 | Demand/Capacity (D/C) | 0.14 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.1 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.33055 | Speed Power Coefficient | 0.51240 |
| PF Slope Coefficient | -1.25564 | PF Power Coefficient | 0.78856 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 1.5 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.9 |
|  |  |  |  |  |  |
| Vehicle Results | 53.9 | Percent Followers, $\%$ | 33.4 |  |  |
| Average Speed, mi/h | 1.11 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 1.5 |  |  |
| Segment Travel Time, minutes | A |  |  |  |  |
| Vehicle LOS |  |  |  |  |  |

[^13]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, CO 620 to <br> Brookfield Dr | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 11 | Shoulder Width, ft | 5 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 2.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 254 |
| Directional Demand Flow Rate, veh/h | 325 | Total Trucks, \% | 2.00 |
| Peak Hour Factor | 0.91 | Demand/Capacity (D/C) | 0.19 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.1 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.31209 | Speed Power Coefficient | 0.52540 |
| PF Slope Coefficient | -1.24368 | PF Power Coefficient | 0.79228 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 2.4 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.6 |
|  |  |  |  |  |  |
| Vehicle Results | 53.6 | Percent Followers, $\%$ | 40.0 |  |  |
| Average Speed, mi/h | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 2.4 |  |  |  |
| Segment Travel Time, minutes | A |  |  |  |  |
| Vehicle LOS |  |  |  |  |  |

[^14]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, CO 620 to <br> Brookfield Dr | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |  |
| :--- | :--- | :--- | :--- | :---: |
| Lane Width, ft | 11 | Shoulder Width, ft | 5 |  |
| Speed Limit, mi/h | 50 | Access Point Density, pts/mi | 2.0 |  |
| Demand and Capacity |  |  |  |  |
| Directional Demand Flow Rate, veh/h | 257 | Opposing Demand Flow Rate, veh/h | 329 |  |
| Peak Hour Factor | 0.90 | Total Trucks, \% | 2.00 |  |
| Segment Capacity, veh/h | Demand/Capacity (D/C) | 0.15 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.1 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.33492 | Speed Power Coefficient | 0.50943 |
| PF Slope Coefficient | -1.25836 | PF Power Coefficient | 0.78770 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 1.7 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.8 |
| Vehicle Results |  |  |  |  | 53.8 |
| Average Speed, mi/h | Percent Followers, $\%$ |  |  |  |  |
| Segment Travel Time, minutes | 1.11 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 1.7 |  |  |
| Vehicle LOS | A |  | 35.0 |  |  |

[^15]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, Reeder Rd to Grist <br> Mill Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 5.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 380 |
| Directional Demand Flow Rate, veh/h | 405 | Total Trucks, \% | 7.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.24 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.2 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.35364 | Speed Power Coefficient | 0.50009 |
| PF Slope Coefficient | -1.26602 | PF Power Coefficient | 0.78590 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 3.5 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.4 |
|  |  |  |  |  |  |
| Vehicle Results | 53.4 | Percent Followers, \% | 46.4 |  |  |
| Average Speed, mi/h | Followers Density, followers/mi/ln | 3.5 |  |  |  |
| Segment Travel Time, minutes | 1.12 | B |  |  |  |
| Vehicle LOS |  |  |  |  |  |

[^16]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, Reeder Rd to Grist <br> Mill Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 5.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 405 |
| Directional Demand Flow Rate, veh/h | 380 | Total Trucks, \% | 7.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.22 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.2 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.36018 | Speed Power Coefficient | 0.49595 |
| PF Slope Coefficient | -1.26981 | PF Power Coefficient | 0.78463 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 3.2 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.4 |
|  |  |  |  |  |  |
| Vehicle Results | 53.4 | Percent Followers, \% | 44.8 |  |  |
| Average Speed, mi/h | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 3.2 |  |  |  |
| Segment Travel Time, minutes | B |  |  |  |  |
| Vehicle LOS |  |  |  |  |  |

[^17]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, Reeder Rd to Grist <br> Mill Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 5.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 484 |
| Directional Demand Flow Rate, veh/h | 475 | Total Trucks, \% | 3.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.28 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.4 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.38665 | Speed Power Coefficient | 0.48428 |
| PF Slope Coefficient | -1.28029 | PF Power Coefficient | 0.78074 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 4.6 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.2 |
|  |  |  |  |  |  |
| Vehicle Results |  |  |  |  |  |
| Average Speed, mi/h | 53.2 | Percent Followers, \% | 51.1 |  |  |
| Segment Travel Time, minutes | 1.13 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 4.6 |  |  |
| Vehicle LOS | B |  |  |  |  |

[^18]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, Reeder Rd to Grist <br> Mill Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 5.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 475 |
| Directional Demand Flow Rate, veh/h | 484 | Total Trucks, \% | 3.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.28 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.4 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.38460 | Speed Power Coefficient | 0.48549 |
| PF Slope Coefficient | -1.27920 | PF Power Coefficient | 0.78113 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 4.7 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.2 |
|  |  |  |  |  |  |
| Vehicle Results | 53.2 | Percent Followers, $\%$ | 51.6 |  |  |
| Average Speed, mi/h | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 4.7 |  |  |  |
| Segment Travel Time, minutes | B |  |  |  |  |
| Vehicle LOS |  |  |  |  |  |

[^19]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 17 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, Fairway Rd to <br> Hillside Ave | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 5 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 4.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 323 |
| Directional Demand Flow Rate, veh/h | 210 | Total Trucks, \% | 3.00 |
| Peak Hour Factor | 0.78 | Demand/Capacity (D/C) | 0.12 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 54.9 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.32061 | Speed Power Coefficient | 0.51056 |
| PF Slope Coefficient | -1.25807 | PF Power Coefficient | 0.78748 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 1.2 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.8 |
|  |  |  |  |  |  |
| Vehicle Results | 53.8 | Percent Followers, $\%$ |  |  |  |
| Average Speed, mi/h | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 1.2 |  |  |  |
| Segment Travel Time, minutes | A |  | 30.8 |  |  |
| Vehicle LOS |  |  |  |  |  |

[^20]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 17 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, Fairway Rd to <br> Hillside Ave | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 5 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 4.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 176 |
| Directional Demand Flow Rate, veh/h | 271 | Total Trucks, \% | 3.00 |
| Peak Hour Factor | 0.93 | Demand/Capacity (D/C) | 0.16 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 54.9 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.27194 | Speed Power Coefficient | 0.54619 |
| PF Slope Coefficient | -1.22523 | PF Power Coefficient | 0.79744 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 1.8 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| \# | Segment Type | Length, ft | Radius, ft |  | Superelevation, \% | Average Speed, mi/h |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Tangent | 5280 | - |  | - | 53.7 |
| Vehicle Results |  |  |  |  |  |  |
| Average Speed, mi/h |  | 53.7 |  | Perce |  | 35.1 |
| Segment Travel Time, minutes |  | 1.12 |  | Follo | followers/mi/ln | 1.8 |
| Vehicle LOS |  | A |  |  |  |  |

[^21]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/17/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, Fairway Rd to <br> Hillside Ave | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |  |
| :--- | :--- | :--- | :--- | :---: |
| Lane Width, ft | 12 | Shoulder Width, ft | 5 |  |
| Speed Limit, mi/h | 50 | Access Point Density, pts/mi | 4.0 |  |
| Demand and Capacity |  |  |  |  |
| Directional Demand Flow Rate, veh/h | 418 | Opposing Demand Flow Rate, veh/h | 277 |  |
| Peak Hour Factor | 0.78 | Total Trucks, \% | 3.00 |  |
| Segment Capacity, veh/h | Demand/Capacity (D/C) | 0.25 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 54.9 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.30679 | Speed Power Coefficient | 0.52014 |
| PF Slope Coefficient | -1.24924 | PF Power Coefficient | 0.79024 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 3.7 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.1 |
|  |  |  |  |  |  |
| Vehicle Results | 53.1 | Percent Followers, \% | 46.6 |  |  |
| Average Speed, mi/h | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 3.7 |  |  |  |
| Segment Travel Time, minutes | 1.13 | B |  |  |  |
| Vehicle LOS |  |  |  |  |  |

[^22]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 17 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, Fairway Rd to <br> Hillside Ave | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |  |
| :--- | :--- | :--- | :--- | :---: |
| Lane Width, ft | 12 | Shoulder Width, ft | 5 |  |
| Speed Limit, mi/h | 50 | Access Point Density, pts/mi | 4.0 |  |
| Demand and Capacity |  |  |  |  |
| Directional Demand Flow Rate, veh/h | 248 | Opposing Demand Flow Rate, veh/h | 375 |  |
| Peak Hour Factor | 0.87 | Total Trucks, \% | 3.00 |  |
| Segment Capacity, veh/h | Demand/Capacity (D/C) | 0.15 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 54.9 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.33494 | Speed Power Coefficient | 0.50108 |
| PF Slope Coefficient | -1.26680 | PF Power Coefficient | 0.78467 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 1.6 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.6 |

## Vehicle Results

| Average Speed, mi/h | 53.6 | Percent Followers, \% | 34.6 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.12 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 1.6 |
| Vehicle LOS | A |  |  |

[^23]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/16/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 632, Shurts Rd to Halls <br> Mill Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 3 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 8.0 |  |
| Demand and Capacity | 45 | Opposing Demand Flow Rate, veh/h | 188 |
| Directional Demand Flow Rate, veh/h | 238 | Total Trucks, \% | 6.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.14 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 46.7 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 2.83200 | Speed Power Coefficient | 0.54268 |
| PF Slope Coefficient | -1.24283 | PF Power Coefficient | 0.77043 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 1.8 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 45.7 |
|  |  |  |  |  |  |
| Vehicle Results |  |  |  |  |  |
| Average Speed, mi/h | 45.7 | Percent Followers, \% | 33.7 |  |  |
| Segment Travel Time, minutes | 1.31 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 1.8 |  |  |
| Vehicle LOS | A |  |  |  |  |

[^24]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 632, Shurts Rd to Halls <br> Mill Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 3 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 8.0 |  |
| Demand and Capacity | 45 | Opposing Demand Flow Rate, veh/h | 238 |
| Directional Demand Flow Rate, veh/h | 188 | Total Trucks, \% | 6.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.11 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 46.7 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 2.84978 | Speed Power Coefficient | 0.52922 |
| PF Slope Coefficient | -1.25634 | PF Power Coefficient | 0.76680 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 1.2 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| \# Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :---: | :---: | :---: | :---: | :---: |
| 1 Tangent | 5280 | - | - | 45.9 |
| Vehicle Results |  |  |  |  |
| Average Speed, mi/h | 45.9 | Perce |  | 29.4 |
| Segment Travel Time, minutes | 1.31 | Follo | followers/mi/ln | 1.2 |
| Vehicle LOS | A |  |  |  |

[^25]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/16/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 632, Shurts Rd to Halls <br> Mill Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 3 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 8.0 |  |
| Demand and Capacity | 45 | Opposing Demand Flow Rate, veh/h | 290 |
| Directional Demand Flow Rate, veh/h | 228 | Total Trucks, \% | 4.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.13 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 46.8 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 2.87005 | Speed Power Coefficient | 0.51726 |
| PF Slope Coefficient | -1.26875 | PF Power Coefficient | 0.76342 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 1.7 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 45.8 |
| Vehicle Results |  |  |  |  |  |
| Average Speed, mi/h | 45.8 | Percent Followers, $\%$ |  |  |  |
| Segment Travel Time, minutes | 1.31 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 1.7 |  |  |
| Vehicle LOS | A |  | 33.7 |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 632, Shurts Rd to Halls <br> Mill Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 3 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 8.0 |  |
| Demand and Capacity | 45 | Opposing Demand Flow Rate, veh/h | 228 |
| Directional Demand Flow Rate, veh/h | 290 | Total Trucks, \% | 4.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.17 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 46.8 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 2.85007 | Speed Power Coefficient | 0.53168 |
| PF Slope Coefficient | -1.25407 | PF Power Coefficient | 0.76740 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 2.4 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 45.6 |

## Vehicle Results

| Average Speed, mi/h | 45.6 | Percent Followers, \% | 38.4 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.32 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 2.4 |
| Vehicle LOS | A |  |  |

[^26]2045 NO-BUILD INTERSECTION ANALYSIS

|  | 4 |  |  | $\checkmark$ |  |  | 4 | 4 | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | ¢ |  |  | $\uparrow$ | 「 |  | $\uparrow$ | F |
| Traffic Volume (vph) | 20 | 241 | 22 | 48 | 161 | 39 | 31 | 206 | 58 | 84 | 158 | 19 |
| Future Volume (vph) | 20 | 241 | 22 | 48 | 161 | 39 | 31 | 206 | 58 | 84 | 158 | 19 |
| Satd. Flow (prot) | 0 | 1835 | 0 | 0 | 1800 | 0 | 0 | 1848 | 1583 | 0 | 1833 | 1583 |
| Flt Permitted |  | 0.950 |  |  | 0.852 |  |  | 0.762 |  |  | 0.551 |  |
| Satd. Flow (perm) | 0 | 1750 | 0 | 0 | 1547 | 0 | 0 | 1419 | 1583 | 0 | 1026 | 1583 |
| Satd. Flow (RTOR) |  | 10 |  |  | 25 |  |  |  | 81 |  |  | 61 |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.71 | 0.76 | 0.69 | 0.80 | 0.77 | 0.65 | 0.78 | 0.94 | 0.85 | 0.91 | 0.84 | 0.53 |
| Growth Factor | 119\% | 119\% | 119\% | 119\% | 119\% | 119\% | 119\% | 119\% | 119\% | 119\% | 119\% | 119\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 449 | 0 | 0 | 391 | 0 | 0 | 308 | 81 | 0 | 334 | 43 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA | Perm | Perm | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Total Split (s) | 47.0 | 47.0 |  | 47.0 | 47.0 |  | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 |
| Total Lost Time (s) |  | 7.0 |  |  | 7.0 |  |  | 5.0 | 5.0 |  | 5.0 | 5.0 |
| Act Efft Green (s) |  | 40.0 |  |  | 40.0 |  |  | 20.0 | 20.0 |  | 20.0 | 20.0 |
| Actuated g/C Ratio |  | 0.56 |  |  | 0.56 |  |  | 0.28 | 0.28 |  | 0.28 | 0.28 |
| v/c Ratio |  | 0.46 |  |  | 0.45 |  |  | 0.78 | 0.16 |  | 1.17 | 0.09 |
| Control Delay |  | 11.2 |  |  | 10.8 |  |  | 40.3 | 6.3 |  | 136.6 | 4.3 |
| Queue Delay |  | 0.0 |  |  | 0.0 |  |  | 0.0 | 0.0 |  | 0.0 | 0.0 |
| Total Delay |  | 11.2 |  |  | 10.8 |  |  | 40.3 | 6.3 |  | 136.6 | 4.3 |
| LOS |  | B |  |  | B |  |  | D | A |  | F | A |
| Approach Delay |  | 11.2 |  |  | 10.8 |  |  | 33.2 |  |  | 121.5 |  |
| Approach LOS |  | B |  |  | B |  |  | C |  |  | F |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length: 72
Actuated Cycle Length: 72
Control Type: Semi Act-Uncoord
Maximum v/c Ratio: 1.17
Intersection Signal Delay: 42.4
Intersection LOS: D
Intersection Capacity Utilization 77.9\%
ICU Level of Service D
Analysis Period (min) 15
Splits and Phases: 3: RT 519 \& US 46


|  | 4 |  |  |  |  |  |  | $\dagger$ | 7 | $\downarrow$ | $\frac{1}{7}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ | 「 |  | $\uparrow$ | F |
| Traffic Volume (vph) | 23 | 168 | 17 | 32 | 270 | 63 | 35 | 169 | 44 | 99 | 179 | 36 |
| Future Volume (vph) | 23 | 168 | 17 | 32 | 270 | 63 | 35 | 169 | 44 | 99 | 179 | 36 |
| Satd. Flow (prot) | 0 | 1829 | 0 | 0 | 1801 | 0 | 0 | 1846 | 1583 | 0 | 1827 | 1583 |
| Flt Permitted |  | 0.920 |  |  | 0.948 |  |  | 0.551 |  |  | 0.548 |  |
| Satd. Flow (perm) | 0 | 1691 | 0 | 0 | 1715 | 0 | 0 | 1026 | 1583 | 0 | 1021 | 1583 |
| Satd. Flow (RTOR) |  | 12 |  |  | 31 |  |  |  | 70 |  |  | 63 |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.84 | 0.80 | 0.65 | 0.88 | 0.91 | 0.69 | 0.73 | 0.83 | 0.75 | 0.76 | 0.85 | 0.68 |
| Growth Factor | 119\% | 119\% | 119\% | 119\% | 119\% | 119\% | 119\% | 119\% | 119\% | 119\% | 119\% | 119\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 314 | 0 | 0 | 505 | 0 | 0 | 299 | 70 | 0 | 406 | 63 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA | Perm | Perm | NA | Perm |
| Protected Phases |  |  |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Total Split (s) | 47.0 | 47.0 |  | 47.0 | 47.0 |  | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 |
| Total Lost Time (s) |  | 7.0 |  |  | 7.0 |  |  | 5.0 | 5.0 |  | 5.0 | 5.0 |
| Act Effct Green (s) |  | 40.0 |  |  | 40.0 |  |  | 20.0 | 20.0 |  | 20.0 | 20.0 |
| Actuated g/C Ratio |  | 0.56 |  |  | 0.56 |  |  | 0.28 | 0.28 |  | 0.28 | 0.28 |
| v/c Ratio |  | 0.33 |  |  | 0.52 |  |  | 1.05 | 0.14 |  | 1.43 | 0.13 |
| Control Delay |  | 9.6 |  |  | 11.8 |  |  | 96.6 | 6.5 |  | 240.5 | 6.7 |
| Queue Delay |  | 0.0 |  |  | 0.0 |  |  | 0.0 | 0.0 |  | 0.0 | 0.0 |
| Total Delay |  | 9.6 |  |  | 11.8 |  |  | 96.6 | 6.5 |  | 240.5 | 6.7 |
| LOS |  | A |  |  | B |  |  | F | A |  | F | A |
| Approach Delay |  | 9.6 |  |  | 11.8 |  |  | 79.5 |  |  | 209.1 |  |
| Approach LOS |  | A |  |  | B |  |  | E |  |  | F |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length: 72
Actuated Cycle Length: 72
Control Type: Semi Act-Uncoord
Maximum v/c Ratio: 1.43
Intersection Signal Delay: 82.3
Intersection LOS: F
Intersection Capacity Utilization 78.1\%
ICU Level of Service D
Analysis Period (min) 15
Splits and Phases: 3: RT 519 \& US 46


| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 21.3 |
| Intersection LOS | C |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | * |  |  | $\uparrow$ |  |  | * |  |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 48 | 149 | 8 | 36 | 90 | 32 | 5 | 169 | 44 | 30 | 109 | 30 |
| Future Vol, veh/h | 48 | 149 | 8 | 36 | 90 | 32 | 5 | 169 | 44 | 30 | 109 | 30 |
| Peak Hour Factor | 0.92 | 0.80 | 0.92 | 0.92 | 0.80 | 0.92 | 0.92 | 0.80 | 0.92 | 0.92 | 0.80 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 73 | 261 | 12 | 55 | 158 | 49 | 8 | 296 | 67 | 46 | 191 | 46 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 23.3 |  |  | 17.7 |  |  | 24.1 |  |  | 18.6 |  |  |
| HCM LOS | C |  |  | C |  |  | C |  |  | C |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $2 \%$ | $23 \%$ | $23 \%$ | $18 \%$ |
| Vol Thru, \% | $78 \%$ | $73 \%$ | $57 \%$ | $64 \%$ |
| Vol Right, \% | $20 \%$ | $4 \%$ | $20 \%$ | $18 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 218 | 205 | 158 | 169 |
| LT Vol | 5 | 48 | 36 | 30 |
| Through Vol | 169 | 149 | 90 | 109 |
| RT Vol | 44 | 8 | 32 | 30 |
| Lane Flow Rate | 370 | 346 | 261 | 282 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.698 | 0.672 | 0.518 | 0.554 |
| Departure Headway (Hd) | 6.782 | 6.991 | 7.151 | 7.065 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 533 | 515 | 504 | 511 |
| Service Time | 4.841 | 5.052 | 5.219 | 5.13 |
| HCM Lane V/C Ratio | 0.694 | 0.672 | 0.518 | 0.552 |
| HCM Control Delay | 24.1 | 23.3 | 17.7 | 18.6 |
| HCM Lane LOS | C | C | C | C |
| HCM 95th-tile Q | 5.4 | 5 | 2.9 | 3.3 |


| Intersection |  |
| :--- | :---: |
| Intersection Delay, s/veh | 58.8 |
| Intersection LOS | F |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ |  |  | ¢ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 31 | 114 | 13 | 41 | 206 | 31 | 22 | 111 | 31 | 43 | 181 | 52 |
| Future Vol, veh/h | 31 | 114 | 13 | 41 | 206 | 31 | 22 | 111 | 31 | 43 | 181 | 52 |
| Peak Hour Factor | 0.92 | 0.80 | 0.92 | 0.92 | 0.80 | 0.92 | 0.92 | 0.80 | 0.92 | 0.92 | 0.80 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 47 | 200 | 20 | 62 | 361 | 47 | 33 | 194 | 47 | 65 | 317 | 79 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 26.6 |  |  | 82.5 |  |  | 27.1 |  |  | 72.1 |  |  |
| HCM LOS | D |  |  | F |  |  | D |  |  | F |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $13 \%$ | $20 \%$ | $15 \%$ | $16 \%$ |
| Vol Thu, \% | $68 \%$ | $72 \%$ | $74 \%$ | $66 \%$ |
| Vol Right, \% | $19 \%$ | $8 \%$ | $11 \%$ | $19 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 164 | 158 | 278 | 276 |
| LT Vol | 22 | 31 | 41 | 43 |
| Through Vol | 111 | 114 | 206 | 181 |
| RT Vol | 31 | 13 | 31 | 52 |
| Lane Flow Rate | 275 | 266 | 470 | 461 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.652 | 0.64 | 1.041 | 1.002 |
| Departure Headway (Hd) | 8.888 | 8.985 | 8.082 | 8.122 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 410 | 405 | 451 | 452 |
| Service Time | 6.888 | 6.985 | 6.082 | 6.122 |
| HCM Lane V/C Ratio | 0.671 | 0.657 | 1.042 | 1.02 |
| HCM Control Delay | 27.1 | 26.6 | 82.5 | 72.1 |
| HCM Lane LOS | D | D | F | F |
| HCM 95th-tile Q | 4.5 | 4.3 | 14.4 | 13 |




HCM Unsignalized Intersection Capacity Analysis
3: CR 519 Belvidere Rd \& Foul Lift Rd


HCM Unsignalized Intersection Capacity Analysis
3: CR 519 Belvidere Rd \& Foul Lift Rd


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.5 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | $\uparrow$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 8 | 10 | 427 | 1 | 11 | 366 |
| Future Vol, veh/h | 8 | 10 | 427 | 1 | 11 | 366 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, $\#$ | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 80 | 80 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 12 | 15 | 538 | 1 | 14 | 461 |


| Major/Minor M | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1028 | 539 | 0 | 0 | 539 | 0 |
| Stage 1 | 539 | - | - | - | - | - |
| Stage 2 | 489 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 | - |
| Pot Cap-1 Maneuver | 259 | 542 | - | - | 1029 | - |
| Stage 1 | 585 | - | - | - | - | - |
| Stage 2 | 616 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 254 | 542 | - | - | 1029 | - |
| Mov Cap-2 Maneuver | 254 | - | - | - | - | - |
| Stage 1 | 585 | - | - | - | - | - |
| Stage 2 | 605 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 15.8 |  | 0 |  | 0.2 |  |
| HCM LOS | C |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRW | BLn1 | SBL |  |
| Capacity (veh/h) |  | - | - | 360 | 1029 | - |
| HCM Lane V/C Ratio |  | - | - | 0.073 | 0.013 | - |
| HCM Control Delay (s) |  | - | - | 15.8 | 8.5 | 0 |
| HCM Lane LOS |  | - | - | C | A | A |
| HCM 95th \%tile Q(veh) |  | - | - | 0.2 | 0 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.9 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | $\uparrow$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 16 | 12 | 474 | 0 | 18 | 511 |
| Future Vol, veh/h | 16 | 12 | 474 | 0 | 18 | 511 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, $\#$ | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 80 | 80 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 23 | 17 | 598 | 0 | 23 | 644 |


| Major/Minor | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1288 | 598 | 0 | 0 | 598 | 0 |
| Stage 1 | 598 | - | - | - | - | - |
| Stage 2 | 690 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 | - |
| Pot Cap-1 Maneuver | 181 | 502 | - | - | 979 | - |
| Stage 1 | 549 | - | - | - | - | - |
| Stage 2 | 498 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 174 | 502 | - | - | 979 | - |
| Mov Cap-2 Maneuver | 174 | - | - | - | - | - |
| Stage 1 | 549 | - | - | - | - | - |
| Stage 2 | 480 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 22.9 |  | 0 |  | 0.3 |  |
| HCM LOS | C |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 242 | 979 | - |
| HCM Lane V/C Ratio |  | - | - | 0.168 | 0.023 | - |
| HCM Control Delay (s) |  | - | - | 22.9 | 8.8 | 0 |
| HCM Lane LOS |  | - | - | C | A | A |
| HCM 95th \%tile Q(veh) |  | - | - | 0.6 | 0.1 | - |

HCM Unsignalized Intersection Capacity Analysis
3: CR 519 Belvidere Rd \& CR 622 Roxbury Station Rd/CR 622 Roxbury Hill Rd


HCM Unsignalized Intersection Capacity Analysis
3: CR 519 Belvidere Rd \& CR 622 Roxbury Station Rd/CR 622 Roxbury Hill Rd

|  | 4 | $\rightarrow$ | $\rangle$ | 7 | 4 | 4 | 4 | $\uparrow$ | $>$ | $\downarrow$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \$ |  |  | \$ |  |  | \$ |  |  | 4 |  |  |
| Traffic Volume (veh/h) | 20 | 1 | 23 | 4 | 1 | 1 | 12 | 501 | 3 | 4 | 385 | 18 |
| Future Volume (Veh/h) | 20 | 1 | 23 | 4 | 1 | 1 | 12 | 501 | 3 | 4 | 385 | 18 |
| Sign Control | Stop |  |  | Stop |  |  | Free |  |  | Free |  |  |
| Grade | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |  |
| Peak Hour Factor | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.90 | 0.80 | 0.80 | 0.90 | 0.80 |
| Hourly flow rate (vph) | 29 | 1 | 34 | 6 | 1 | 1 | 18 | 651 | 4 | 6 | 501 | 26 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |

Lane Width ( ft )
Walking Speed (tt/s)
Percent Blockage

| Right turn flare $($ veh $)$ | None | None |
| :--- | :--- | :--- |
| Median type |  |  |
| Median storage veh) |  |  |

Upstream signal (ft)

| PX , platoon unblocked |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| VC, conflicting volume | 1216 | 1217 | 514 | 1250 | 1228 | 653 | 527 | 655 |

$\mathrm{vC2}$, stage 2 conf vol

| vCu, unblocked vol | 1216 | 1217 | 514 | 1250 | 1228 | 653 | 527 | 655 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| tC , single (s) | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.6 | 4.1 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

tC, 2 stage (s)

| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.7 | 2.2 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| p0 queue free $\%$ | 81 | 99 | 94 | 96 | 99 | 100 | 98 | 99 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| cM capacity (veh/h) | 151 | 177 | 557 | 138 | 175 | 471 | 836 | 942 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Direction, Lane \# | EB 1 | WB 1 | NB 1 | SB1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume Total | 64 | 8 | 673 | 533 |  |
| Volume Left | 29 | 6 | 18 | 6 |  |
| Volume Right | 34 | 1 | 4 | 26 |  |
| cSH | 248 | 156 | 836 | 942 |  |
| Volume to Capacity | 0.26 | 0.05 | 0.02 | 0.01 |  |
| Queue Length 95th (tt) | 25 | 4 | 2 | 0 |  |
| Control Delay (s) | 24.5 | 29.3 | 0.6 | 0.2 |  |
| Lane LOS | C | D | A | A |  |
| Approach Delay (s) | 24.5 | 29.3 | 0.6 | 0.2 |  |
| Approach LOS | C | D |  |  |  |
| Intersection Summary |  |  |  |  |  |
| Average Delay |  |  | 1.8 |  |  |
| Intersection Capacity Utilization |  |  | 49.8\% | ICU Level of Service | A |
| Analysis Period (min) |  |  | 15 |  |  |

HCM Unsignalized Intersection Capacity Analysis
3: CR 519 Belvidere Rd \& CR 621 Brainards Rd


HCM Unsignalized Intersection Capacity Analysis
3: CR 519 Belvidere Rd \& CR 621 Brainards Rd


HCM Unsignalized Intersection Capacity Analysis
2: CR 646 Belvidere Rd/CR 519 Belvidere Rd \& CR 519 Uniontown Rd


HCM Unsignalized Intersection Capacity Analysis
2: CR 646 Belvidere Rd/CR 519 Belvidere Rd \& CR 519 Uniontown Rd


Timings
3: CR 519 Uniontown Rd \& NJ 57


Cycle Length: 90
Actuated Cycle Length: 90
Offset: 10.9 (12\%), Referenced to phase 4:EBTL and 8:WBTL, Start of Yellow
Natural Cycle: 80
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 0.69
Intersection Signal Delay: $19.4 \quad$ Intersection LOS: B
Intersection Capacity Utilization 83.1\% ICU Level of Service E
Analysis Period (min) 15
Splits and Phases: 3: CR 519 Uniontown Rd \& NJ 57


Timings
3: CR 519 Uniontown Rd \& NJ 57


Cycle Length: 90
Actuated Cycle Length: 90
Offset: 10.9 (12\%), Referenced to phase 4:EBTL and 8:WBTL, Start of Yellow
Natural Cycle: 80
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 0.85
Intersection Signal Delay: 25.5 Intersection LOS: C
Intersection Capacity Utilization 89.6\% ICU Level of Service E
Analysis Period (min) 15
Splits and Phases: 3: CR 519 Uniontown Rd \& NJ 57





HCM Unsignalized Intersection Capacity Analysis
4: CO 632 \& I-78 WB ramp


[^27]
## 2045 NO-BUILD MID-BLOCK ANALYSIS

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/16/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, northeast of CO <br> 610 | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 3 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 9.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 291 |
| Directional Demand Flow Rate, veh/h | 343 | Total Trucks, \% | 2.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.20 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 52.6 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.18564 | Speed Power Coefficient | 0.51703 |
| PF Slope Coefficient | -1.25954 | PF Power Coefficient | 0.78214 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 2.8 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 51.0 |

## Vehicle Results

| Average Speed, mi/h | 51.0 | Percent Followers, \% | 42.1 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.18 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 2.8 |
| Vehicle LOS | B |  |  |

[^28]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, northeast of CO <br> 610 | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 3 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 9.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 343 |
| Directional Demand Flow Rate, veh/h | 291 | Total Trucks, \% | 2.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.17 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 52.6 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.20083 | Speed Power Coefficient | 0.50667 |
| PF Slope Coefficient | -1.26944 | PF Power Coefficient | 0.77916 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 2.2 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 51.2 |

## Vehicle Results

| Average Speed, mi/h | 51.2 | Percent Followers, \% | 38.5 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.17 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 2.2 |
| Vehicle LOS | A |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, northeast of CO <br> 610 | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 3 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 9.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 399 |
| Directional Demand Flow Rate, veh/h | 303 | Total Trucks, \% | 2.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.18 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 52.6 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.21576 | Speed Power Coefficient | 0.49701 |
| PF Slope Coefficient | -1.27872 | PF Power Coefficient | 0.77628 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 2.4 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 51.1 |
| Vehicle Results |  |  |  |  | 51.1 |
| Average Speed, mi/h | Percent Followers, $\%$ |  |  |  |  |
| Segment Travel Time, minutes | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 2.4 |  |  |  |
| Vehicle LOS | A |  |  |  |  |

[^29]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, northeast of CO <br> 610 | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 3 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 9.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 303 |
| Directional Demand Flow Rate, veh/h | 399 | Total Trucks, \% | 2.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.23 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 52.6 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.18924 | Speed Power Coefficient | 0.51453 |
| PF Slope Coefficient | -1.26192 | PF Power Coefficient | 0.78143 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 3.6 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 50.9 |

## Vehicle Results

| Average Speed, mi/h | 50.9 | Percent Followers, \% | 46.0 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.18 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 3.6 |
| Vehicle LOS | B |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 17 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, Stone Hedge Rd <br> to Hope Crossing Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Constrained | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 0.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | - |
| Directional Demand Flow Rate, veh/h | 385 | Total Trucks, \% | 3.00 |
| Peak Hour Factor | 0.80 | Demand/Capacity (D/C) | 0.23 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 56.9 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.64416 | Speed Power Coefficient | 0.41674 |
| PF Slope Coefficient | -1.32222 | PF Power Coefficient | 0.75266 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 3.3 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 54.7 |
|  |  |  |  |  |  |
| Vehicle Results | 54.7 | Percent Followers, \% | 47.5 |  |  |
| Average Speed, mi/h | 1.10 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 3.3 |  |  |
| Segment Travel Time, minutes | B |  |  |  |  |
| Vehicle LOS |  |  |  |  |  |

[^30]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 17 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, Stone Hedge Rd <br> to Hope Crossing Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Constrained | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 0.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | - |
| Directional Demand Flow Rate, veh/h | 386 | Total Trucks, \% | 3.00 |
| Peak Hour Factor | 0.84 | Demand/Capacity (D/C) | 0.23 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 56.9 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.64416 | Speed Power Coefficient | 0.41674 |
| PF Slope Coefficient | -1.32222 | PF Power Coefficient | 0.75266 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 3.4 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 54.7 |

## Vehicle Results

| Average Speed, mi/h | 54.7 | Percent Followers, \% | 47.6 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.10 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 3.4 |
| Vehicle LOS | B |  |  |

[^31]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 17 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, Stone Hedge Rd <br> to Hope Crossing Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Constrained | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 0.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | - |
| Directional Demand Flow Rate, veh/h | 334 | Total Trucks, \% | 3.00 |
| Peak Hour Factor | 0.90 | Demand/Capacity (D/C) | 0.20 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 56.9 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.64416 | Speed Power Coefficient | 0.41674 |
| PF Slope Coefficient | -1.32222 | PF Power Coefficient | 0.75266 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 2.7 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 54.9 |
|  |  |  |  |  |  |
| Vehicle Results | 54.9 | Percent Followers, $\%$ | 44.0 |  |  |
| Average Speed, mi/h | 1.09 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 2.7 |  |  |
| Segment Travel Time, minutes | B |  |  |  |  |
| Vehicle LOS |  |  |  |  |  |

[^32]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 17 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, Stone Hedge Rd <br> to Hope Crossing Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Constrained | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 0.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | - |
| Directional Demand Flow Rate, veh/h | 427 | Total Trucks, \% | 3.00 |
| Peak Hour Factor | 0.82 | Demand/Capacity (D/C) | 0.25 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 56.9 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.64416 | Speed Power Coefficient | 0.41674 |
| PF Slope Coefficient | -1.32222 | PF Power Coefficient | 0.75266 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 3.9 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 54.6 |

## Vehicle Results

| Average Speed, mi/h | 54.6 | Percent Followers, \% | 50.2 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.10 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 3.9 |
| Vehicle LOS | B |  |  |

[^33]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, CO 623 Brass <br> Castle Rd to Pequest Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 4.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 445 |
| Directional Demand Flow Rate, veh/h | 567 | Total Trucks, \% | 0.00 |
| Peak Hour Factor | 0.88 | Demand/Capacity (D/C) | 0.33 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.7 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.39642 | Speed Power Coefficient | 0.48975 |
| PF Slope Coefficient | -1.27423 | PF Power Coefficient | 0.78308 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 5.9 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.4 |
|  |  |  |  |  |  |
| Vehicle Results | 53.4 | Percent Followers, $\%$ | 55.8 |  |  |
| Average Speed, mi/h | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 5.9 |  |  |  |
| Segment Travel Time, minutes | C |  |  |  |  |
| Vehicle LOS |  |  |  |  |  |

[^34]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, CO 623 Brass <br> Castle Rd to Pequest Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 4.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 542 |
| Directional Demand Flow Rate, veh/h | 426 | Total Trucks, \% | 0.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.25 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.7 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.41906 | Speed Power Coefficient | 0.47664 |
| PF Slope Coefficient | -1.28592 | PF Power Coefficient | 0.77876 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 3.8 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.7 |
|  |  |  |  |  |  |
| Vehicle Results | 53.7 | Percent Followers, \% | 48.4 |  |  |
| Average Speed, mi/h | 1.12 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 3.8 |  |  |
| Segment Travel Time, minutes | B |  |  |  |  |
| Vehicle LOS |  |  |  |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, CO 623 Brass <br> Castle Rd to Pequest Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 4.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 481 |
| Directional Demand Flow Rate, veh/h | 647 | Total Trucks, \% | 7.00 |
| Peak Hour Factor | 0.85 | Demand/Capacity (D/C) | 0.38 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.5 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.39239 | Speed Power Coefficient | 0.48463 |
| PF Slope Coefficient | -1.27901 | PF Power Coefficient | 0.78178 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 7.3 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 52.9 |
|  |  |  |  |  |  |
| Vehicle Results | 52.9 | Percent Followers, \% | 59.8 |  |  |
| Average Speed, mi/h | 1.13 | Followers Density, followers/mi/ln | 7.3 |  |  |
| Segment Travel Time, minutes | C |  |  |  |  |
| Vehicle LOS |  |  |  |  |  |

[^35]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, CO 623 Brass <br> Castle Rd to Pequest Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |  |
| :--- | :--- | :--- | :--- | :---: |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |  |
| Speed Limit, mi/h | 50 | Access Point Density, pts/mi | 4.0 |  |
| Demand and Capacity |  |  |  |  |
| Directional Demand Flow Rate, veh/h | 431 | Opposing Demand Flow Rate, veh/h | 579 |  |
| Peak Hour Factor | 0.95 | Total Trucks, \% | 7.00 |  |
| Segment Capacity, veh/h | Demand/Capacity (D/C) | 0.25 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.5 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.41442 | Speed Power Coefficient | 0.47228 |
| PF Slope Coefficient | -1.29002 | PF Power Coefficient | 0.77761 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 3.9 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.4 |
|  |  |  |  |  |  |
| Vehicle Results | 53.4 | Percent Followers, \% | 48.8 |  |  |
| Average Speed, mi/h | 1.12 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 3.9 |  |  |
| Segment Travel Time, minutes | B |  |  |  |  |
| Vehicle LOS |  |  |  |  |  |

[^36]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, CO 620 to <br> Brookfield Dr | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |  |
| :--- | :--- | :--- | :--- | :---: |
| Lane Width, ft | 11 | Shoulder Width, ft | 5 |  |
| Speed Limit, mi/h | 50 | Access Point Density, pts/mi | 2.0 |  |
| Demand and Capacity |  |  |  |  |
| Directional Demand Flow Rate, veh/h | 369 | Opposing Demand Flow Rate, veh/h | 281 |  |
| Peak Hour Factor | 0.85 | Total Trucks, \% | 2.00 |  |
| Segment Capacity, veh/h | Demand/Capacity (D/C) | 0.22 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.1 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.32075 | Speed Power Coefficient | 0.51921 |
| PF Slope Coefficient | -1.24938 | PF Power Coefficient | 0.79052 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 3.0 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.5 |
|  |  |  |  |  |  |
| Vehicle Results |  |  |  |  |  |
| Average Speed, mi/h | 53.5 | Percent Followers, \% | 43.4 |  |  |
| Segment Travel Time, minutes | 1.12 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 3.0 |  |  |
| Vehicle LOS | B |  |  |  |  |

[^37]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, CO 620 to <br> Brookfield Dr | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 11 | Shoulder Width, ft | 5 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 2.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 361 |
| Directional Demand Flow Rate, veh/h | 275 | Total Trucks, \% | 2.00 |
| Peak Hour Factor | 0.87 | Demand/Capacity (D/C) | 0.16 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.1 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.34386 | Speed Power Coefficient | 0.50350 |
| PF Slope Coefficient | -1.26381 | PF Power Coefficient | 0.78594 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 1.9 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.7 |
| Vehicle Results |  |  |  |  | 53.7 |
| Average Speed, mi/h | Percent Followers, \% |  |  |  |  |
| Segment Travel Time, minutes | 1.12 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 1.9 |  |  |
| Vehicle LOS | A |  | 36.7 |  |  |

[^38]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, CO 620 to <br> Brookfield Dr | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |  |
| :--- | :--- | :--- | :--- | :---: |
| Lane Width, ft | 11 | Shoulder Width, ft | 5 |  |
| Speed Limit, mi/h | 50 | Access Point Density, pts/mi | 2.0 |  |
| Demand and Capacity |  |  |  |  |
| Directional Demand Flow Rate, veh/h | 374 | Opposing Demand Flow Rate, veh/h | 292 |  |
| Peak Hour Factor | 0.91 | Total Trucks, \% | 2.00 |  |
| Segment Capacity, veh/h | Demand/Capacity (D/C) | 0.22 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.1 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.32416 | Speed Power Coefficient | 0.51681 |
| PF Slope Coefficient | -1.25158 | PF Power Coefficient | 0.78984 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 3.1 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.4 |
|  |  |  |  |  |  |
| Vehicle Results | 53.4 | Percent Followers, \% | 43.7 |  |  |
| Average Speed, mi/h | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 3.1 |  |  |  |
| Segment Travel Time, minutes | B |  |  |  |  |
| Vehicle LOS |  |  |  |  |  |

[^39]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, CO 620 to <br> Brookfield Dr | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 11 | Shoulder Width, ft | 5 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 2.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 378 |
| Directional Demand Flow Rate, veh/h | 296 | Total Trucks, \% | 2.00 |
| Peak Hour Factor | 0.90 | Demand/Capacity (D/C) | 0.17 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.1 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.34841 | Speed Power Coefficient | 0.50055 |
| PF Slope Coefficient | -1.26651 | PF Power Coefficient | 0.78505 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 2.1 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.7 |
|  |  |  |  |  |  |
| Vehicle Results | 53.7 | Percent Followers, \% | 38.5 |  |  |
| Average Speed, mi/h | 1.12 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 2.1 |  |  |
| Segment Travel Time, minutes | A |  |  |  |  |
| Vehicle LOS |  |  |  |  |  |

[^40]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, Reeder Rd to Grist <br> Mill Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 5.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 438 |
| Directional Demand Flow Rate, veh/h | 467 | Total Trucks, \% | 7.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.27 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.2 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.36841 | Speed Power Coefficient | 0.49086 |
| PF Slope Coefficient | -1.27444 | PF Power Coefficient | 0.78305 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 4.4 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.2 |
|  |  |  |  |  |  |
| Vehicle Results | 53.2 | Percent Followers, $\%$ | 50.5 |  |  |
| Average Speed, mi/h | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 4.4 |  |  |  |
| Segment Travel Time, minutes | B |  |  |  |  |
| Vehicle LOS |  |  |  |  |  |

[^41]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, Reeder Rd to Grist <br> Mill Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 5.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 467 |
| Directional Demand Flow Rate, veh/h | 438 | Total Trucks, \% | 7.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.26 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.2 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.37556 | Speed Power Coefficient | 0.48656 |
| PF Slope Coefficient | -1.27833 | PF Power Coefficient | 0.78168 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 4.0 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.2 |
|  |  |  |  |  |  |
| Vehicle Results | 53.2 | Percent Followers, $\%$ | 48.9 |  |  |
| Average Speed, mi/h | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 4.0 |  |  |  |
| Segment Travel Time, minutes | B |  |  |  |  |
| Vehicle LOS |  |  |  |  |  |

[^42]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, Reeder Rd to Grist <br> Mill Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 5.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 557 |
| Directional Demand Flow Rate, veh/h | 547 | Total Trucks, \% | 3.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.32 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.4 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.40322 | Speed Power Coefficient | 0.47492 |
| PF Slope Coefficient | -1.28868 | PF Power Coefficient | 0.77760 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 5.7 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.0 |
|  |  |  |  |  |  |
| Vehicle Results | 53.0 | Percent Followers, \% | 55.3 |  |  |
| Average Speed, mi/h | Followers Density, followers/mi/ln | 5.7 |  |  |  |
| Segment Travel Time, minutes | 1.13 | C |  |  |  |
| Vehicle LOS |  |  |  |  |  |

[^43]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, Reeder Rd to Grist <br> Mill Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 5.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 547 |
| Directional Demand Flow Rate, veh/h | 557 | Total Trucks, \% | 3.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.33 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.4 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.40106 | Speed Power Coefficient | 0.47611 |
| PF Slope Coefficient | -1.28762 | PF Power Coefficient | 0.77801 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 5.9 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.0 |
|  |  |  |  |  |  |
| Vehicle Results | 53.0 | Percent Followers, \% | 55.8 |  |  |
| Average Speed, mi/h | Followers Density, followers/mi/ln | 5.9 |  |  |  |
| Segment Travel Time, minutes | 1.13 | C |  |  |  |
| Vehicle LOS |  |  |  |  |  |

[^44]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 17 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, Fairway Rd to <br> Hillside Ave | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 5 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 4.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 372 |
| Directional Demand Flow Rate, veh/h | 242 | Total Trucks, \% | 3.00 |
| Peak Hour Factor | 0.78 | Demand/Capacity (D/C) | 0.14 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 54.9 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.33416 | Speed Power Coefficient | 0.50158 |
| PF Slope Coefficient | -1.26634 | PF Power Coefficient | 0.78482 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 1.5 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.6 |
| Vehicle Results |  |  |  |  | 53.6 |
| Average Speed, mi/h | Percent Followers, \% |  |  |  |  |
| Segment Travel Time, minutes | 1.12 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 1.5 |  |  |
| Vehicle LOS | A |  | 34.1 |  |  |

[^45]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 17 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, Fairway Rd to <br> Hillside Ave | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 5 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 4.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 203 |
| Directional Demand Flow Rate, veh/h | 312 | Total Trucks, \% | 3.00 |
| Peak Hour Factor | 0.93 | Demand/Capacity (D/C) | 0.18 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 54.9 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.28206 | Speed Power Coefficient | 0.53834 |
| PF Slope Coefficient | -1.23245 | PF Power Coefficient | 0.79531 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 2.3 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.5 |
|  |  |  |  |  |  |
| Vehicle Results |  |  |  |  |  |
| Average Speed, mi/h | 53.5 | Percent Followers, \% | 38.6 |  |  |
| Segment Travel Time, minutes | 1.12 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 2.3 |  |  |
| Vehicle LOS | A |  |  |  |  |

[^46]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 17 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, Fairway Rd to <br> Hillside Ave | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 5 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 4.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 319 |
| Directional Demand Flow Rate, veh/h | 481 | Total Trucks, \% | 3.00 |
| Peak Hour Factor | 0.78 | Demand/Capacity (D/C) | 0.28 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 54.9 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.31949 | Speed Power Coefficient | 0.51132 |
| PF Slope Coefficient | -1.25738 | PF Power Coefficient | 0.78770 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 4.6 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 52.9 |
|  |  |  |  |  |  |
| Vehicle Results | 52.9 | Percent Followers, \% | 50.6 |  |  |
| Average Speed, mi/h | Followers Density, followers/mi/ln | 4.6 |  |  |  |
| Segment Travel Time, minutes | 1.13 | B |  |  |  |
| Vehicle LOS |  |  |  |  |  |

[^47]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 17 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, Fairway Rd to <br> Hillside Ave | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 5 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 4.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 431 |
| Directional Demand Flow Rate, veh/h | 286 | Total Trucks, \% | 3.00 |
| Peak Hour Factor | 0.87 | Demand/Capacity (D/C) | 0.17 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 54.9 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.34950 | Speed Power Coefficient | 0.49192 |
| PF Slope Coefficient | -1.27520 | PF Power Coefficient | 0.78186 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 2.0 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| \# | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Tangent | 5280 | - | - | 53.4 |
| Vehicle Results |  |  |  |  |  |
| Average Speed, mi/h |  | 53.4 | Perce |  | 38.1 |
| Segment Travel Time, minutes |  | 1.12 | Follo | followers/mi/ln | 2.0 |
| Vehicle LOS |  | A |  |  |  |

[^48]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 632, Shurts Rd to Halls <br> Mill Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 3 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 8.0 |  |
| Demand and Capacity | 45 | Opposing Demand Flow Rate, veh/h | 216 |
| Directional Demand Flow Rate, veh/h | 275 | Total Trucks, \% | 6.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.16 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 46.7 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 2.84231 | Speed Power Coefficient | 0.53479 |
| PF Slope Coefficient | -1.25072 | PF Power Coefficient | 0.76831 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 2.2 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 45.6 |

## Vehicle Results

| Average Speed, mi/h | 45.6 | Percent Followers, \% | 37.1 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.32 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 2.2 |
| Vehicle LOS | A |  |  |

[^49]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 632, Shurts Rd to Halls <br> Mill Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 3 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 8.0 |  |
| Demand and Capacity | 45 | Opposing Demand Flow Rate, veh/h | 275 |
| Directional Demand Flow Rate, veh/h | 216 | Total Trucks, \% | 6.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.13 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 46.7 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 2.86175 | Speed Power Coefficient | 0.52056 |
| PF Slope Coefficient | -1.26516 | PF Power Coefficient | 0.76441 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 1.5 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 45.8 |

## Vehicle Results

| Average Speed, mi/h | 45.8 | Percent Followers, \% | 32.5 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.31 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 1.5 |
| Vehicle LOS | A |  |  |

[^50]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 632, Shurts Rd to Halls <br> Mill Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 3 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 8.0 |  |
| Demand and Capacity | 45 | Opposing Demand Flow Rate, veh/h | 334 |
| Directional Demand Flow Rate, veh/h | 263 | Total Trucks, \% | 4.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.15 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 46.8 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 2.88282 | Speed Power Coefficient | 0.50851 |
| PF Slope Coefficient | -1.27779 | PF Power Coefficient | 0.76093 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 2.1 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 45.6 |

## Vehicle Results

| Average Speed, mi/h | 45.6 | Percent Followers, \% | 37.0 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.32 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 2.1 |
| Vehicle LOS | A |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 632, Shurts Rd to Halls <br> Mill Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 3 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 8.0 |  |
| Demand and Capacity | 45 | Opposing Demand Flow Rate, veh/h | 263 |
| Directional Demand Flow Rate, veh/h | 334 | Total Trucks, \% | 4.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.20 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 46.8 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 2.86158 | Speed Power Coefficient | 0.52326 |
| PF Slope Coefficient | -1.26260 | PF Power Coefficient | 0.76509 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 3.1 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 45.4 |

## Vehicle Results

| Average Speed, mi/h | 45.4 | Percent Followers, \% | 42.0 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.32 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 3.1 |
| Vehicle LOS | B |  |  |

[^51]
## 2045 BUILD INTERSECTION ANALYSIS

Timings
3: RT 519 \& US 46

|  | $\rangle$ |  |  |  | 4 | 4 | $p$ | $\checkmark$ |  | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  | $\uparrow$ |  | $\uparrow$ | F |  | $\uparrow$ | 「 |
| Traffic Volume (vph) | 24 | 287 | 132 | 450 | 37 | 206 | 58 | 235 | 441 | 56 |
| Future Volume (vph) | 24 | 287 | 132 | 450 | 37 | 206 | 58 | 235 | 441 | 56 |
| Turn Type | Perm | NA | Perm | NA | Perm | NA | Perm | Perm | NA | Perm |
| Protected Phases |  | 4 |  | 8 |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  | 8 |  | 2 |  | 2 | 6 |  | 6 |
| Detector Phase | 4 | 4 | 8 | 8 | 2 | 2 | 2 | 6 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 40.0 | 40.0 | 40.0 | 40.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Minimum Split (s) | 47.0 | 47.0 | 47.0 | 47.0 | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 |
| Total Split (s) | 47.0 | 47.0 | 47.0 | 47.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 |
| Total Split (\%) | 65.3\% | 65.3\% | 65.3\% | 65.3\% | 34.7\% | 34.7\% | 34.7\% | 34.7\% | 34.7\% | 34.7\% |
| Yellow Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) |  | 0.0 |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |
| Total Lost Time (s) |  | 7.0 |  | 7.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | None | None | None | None | Max | Max | Max | Max | Max | Max |
| Act Effct Green (s) |  | 40.0 |  | 40.0 |  | 20.0 | 20.0 |  | 20.0 | 20.0 |
| Actuated g/C Ratio |  | 0.56 |  | 0.56 |  | 0.28 | 0.28 |  | 0.28 | 0.28 |
| $\mathrm{v} / \mathrm{c}$ Ratio |  | 0.46 |  | 1.06 |  | 2.68 | 0.14 |  | 2.40 | 0.14 |
| Control Delay |  | 11.3 |  | 65.8 |  | 800.2 | 6.6 |  | 659.2 | 8.0 |
| Queue Delay |  | 0.0 |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |
| Total Delay |  | 11.3 |  | 65.8 |  | 800.2 | 6.6 |  | 659.2 | 8.0 |
| LOS |  | B |  | E |  | F | A |  | F | A |
| Approach Delay |  | 11.3 |  | 65.8 |  | 638.1 |  |  | 605.8 |  |
| Approach LOS |  | B |  | E |  | F |  |  | F |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |

Cycle Length: 72
Actuated Cycle Length: 72
Natural Cycle: 150
Control Type: Semi Act-Uncoord
Maximum v/c Ratio: 2.68
Intersection Signal Delay: 315.9
Intersection LOS: F
Intersection Capacity Utilization 135.3\% ICU Level of Service H
Analysis Period (min) 15
Splits and Phases: 3: RT 519 \& US 46


Timings
3: RT 519 \& US 46

|  | $\rangle$ |  |  |  | 4 | 4 | $p$ | $\checkmark$ | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  | $\uparrow$ |  | $\uparrow$ | 7 |  | $\uparrow$ | 7 |
| Traffic Volume (vph) | 51 | 380 | 59 | 498 | 80 | 388 | 102 | 118 | 213 | 43 |
| Future Volume (vph) | 51 | 380 | 59 | 498 | 80 | 388 | 102 | 118 | 213 | 43 |
| Turn Type | Perm | NA | Perm | NA | Perm | NA | Perm | Perm | NA | Perm |
| Protected Phases |  | 4 |  | 8 |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  | 8 |  | 2 |  | 2 | 6 |  | 6 |
| Detector Phase | 4 | 4 | 8 | 8 | 2 | 2 | 2 | 6 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 40.0 | 40.0 | 40.0 | 40.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Minimum Split (s) | 47.0 | 47.0 | 47.0 | 47.0 | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 |
| Total Split (s) | 47.0 | 47.0 | 47.0 | 47.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 |
| Total Split (\%) | 65.3\% | 65.3\% | 65.3\% | 65.3\% | 34.7\% | 34.7\% | 34.7\% | 34.7\% | 34.7\% | 34.7\% |
| Yellow Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) |  | 0.0 |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |
| Total Lost Time (s) |  | 7.0 |  | 7.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | None | None | None | None | Max | Max | Max | Max | Max | Max |
| Act Effct Green (s) |  | 40.0 |  | 40.0 |  | 20.0 | 20.0 |  | 20.0 | 20.0 |
| Actuated g/C Ratio |  | 0.56 |  | 0.56 |  | 0.28 | 0.28 |  | 0.28 | 0.28 |
| $\mathrm{v} / \mathrm{c}$ Ratio |  | 0.65 |  | 0.82 |  | 2.48 | 0.24 |  | 5.70 | 0.11 |
| Control Delay |  | 15.3 |  | 22.3 |  | 695.8 | 5.6 |  | 2155.2 | 6.0 |
| Queue Delay |  | 0.0 |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |
| Total Delay |  | 15.3 |  | 22.3 |  | 695.8 | 5.6 |  | 2155.2 | 6.0 |
| LOS |  | B |  | C |  | F | A |  | F | A |
| Approach Delay |  | 15.3 |  | 22.3 |  | 568.7 |  |  | 1899.0 |  |
| Approach LOS |  | B |  | C |  | F |  |  | F |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |

Cycle Length: 72
Actuated Cycle Length: 72
Natural Cycle: 100
Control Type: Semi Act-Uncoord
Maximum v/c Ratio: 5.70
Intersection Signal Delay: 514.4
Intersection LOS: F
Intersection Capacity Utilization 102.6\% ICU Level of Service G
Analysis Period (min) 15
Splits and Phases: 3: RT 519 \& US 46


HCM Unsignalized Intersection Capacity Analysis
3: CR 519 \& CR 623

|  | 7 | $\rightarrow$ | $\geqslant$ | $\dagger$ |  | 4 | 4 | 4 | 7 | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ${ }_{4}$ |  |  | ¢ |  |  | $\dagger$ |  |  | $\dagger$ |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Stop |  |  | Stop |  |
| Traffic Volume (vph) | 74 | 315 | 44 | 227 | 598 | 199 | 7 | 237 | 62 | 152 | 561 | 152 |
| Future Volume (vph) | 74 | 315 | 44 | 227 | 598 | 199 | 7 | 237 | 62 | 152 | 561 | 152 |
| Peak Hour Factor | 0.92 | 0.80 | 0.92 | 0.92 | 0.80 | 0.92 | 0.92 | 0.80 | 0.92 | 0.92 | 0.80 | 0.92 |
| Hourly flow rate (vph) | 80 | 394 | 48 | 247 | 748 | 216 | 8 | 296 | 67 | 165 | 701 | 165 |


| Direction, Lane \# | EB 1 | WB 1 | NB 1 | SB 1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume Total (vph) | 522 | 1211 | 371 | 1031 |  |
| Volume Left (vph) | 80 | 247 | 8 | 165 |  |
| Volume Right (vph) | 48 | 216 | 67 | 165 |  |
| Hadj (s) | 0.01 | -0.03 | -0.07 | -0.03 |  |
| Departure Headway (s) | 9.5 | 9.5 | 9.5 | 9.5 |  |
| Degree Utilization, x | 1.38 | 3.19 | 0.98 | 2.72 |  |
| Capacity (veh/h) | 387 | 393 | 371 | 390 |  |
| Control Delay (s) | 213.2 | 1011.0 | 72.5 | 799.1 |  |
| Approach Delay (s) | 213.2 | 1011.0 | 72.5 | 799.1 |  |
| Approach LOS | F | F | F | F |  |
| Intersection Summary |  |  |  |  |  |
| DelayLevel of Service |  |  | 697.4 |  |  |
|  |  |  | F |  |  |
| Intersection Capacity Utilization |  |  | 156.5\% | ICU Level of Service | H |
| Analysis Period (min) |  |  | 15 |  |  |

HCM Unsignalized Intersection Capacity Analysis
3: CR 519 \& CR 623

|  | $\stackrel{ }{*}$ | $\rightarrow$ | \% | 7 | $\checkmark$ | 4 | 4 | $\uparrow$ | $>$ | , | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | ¢ |  |  | ${ }_{4}$ |  |  | ¢ |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Stop |  |  | Stop |  |
| Traffic Volume (vph) | 105 | 397 | 48 | 57 | 288 | 43 | 155 | 802 | 224 | 60 | 253 | 73 |
| Future Volume (vph) | 105 | 397 | 48 | 57 | 288 | 43 | 155 | 802 | 224 | 60 | 253 | 73 |
| Peak Hour Factor | 0.92 | 0.80 | 0.92 | 0.92 | 0.80 | 0.92 | 0.92 | 0.80 | 0.92 | 0.92 | 0.80 | 0.92 |
| Hourly flow rate (vph) | 114 | 496 | 52 | 62 | 360 | 47 | 168 | 1003 | 243 | 65 | 316 | 79 |


| Direction, Lane \# | EB 1 | WB 1 | NB 1 | SB 1 |
| :--- | ---: | ---: | ---: | ---: |
| Volume Total (vph) | 662 | 469 | 1414 | 460 |
| Volume Left (vph) | 114 | 62 | 168 | 65 |
| Volume Right (vph) | 52 | 47 | 243 | 79 |
| Hadj (s) | 0.02 | 0.00 | -0.05 | -0.04 |
| Departure Headway (s) | 9.6 | 9.6 | 9.5 | 9.5 |
| Degree Utilization, x | 1.76 | 1.25 | 3.74 | 1.22 |
| Capacity (veh/h) | 380 | 382 | 382 | 383 |
| Control Delay (s) | 376.7 | 159.7 | 1257.9 | 148.5 |
| Approach Delay (s) | 376.7 | 159.7 | 1257.9 | 148.5 |
| Approach LOS | F | F | F | F |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | :--- |
| Delay | 722.6 |  | H |
| Level of Service | F | ICU Level of Service |  |
| Intersection Capacity Utilization | $132.3 \%$ |  |  |
| Analysis Period (min) | 15 |  |  |




HCM Unsignalized Intersection Capacity Analysis
3: CR 519 Belvidere Rd \& Foul Lift Rd





[^52]HCM Unsignalized Intersection Capacity Analysis
3: CR 519 Belvidere Rd \& CR 622 Roxbury Station Rd/CR 622 Roxbury Hill Rd

|  | 4 | $\rightarrow$ | $\rangle$ | 7 | $\leftarrow$ | 4 | 4 | $\uparrow$ | $>$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \$ |  |  | ¢ |  |  | ¢ |  |  | \$ |  |  |
| Traffic Volume (veh/h) | 189 | 1 | 17 | 8 | 51 | 12 | 1055 | 1735 | 4 | 1 | 656 | 1485 |
| Future Volume (Veh/h) | 189 | 1 | 17 | 8 | 51 | 12 | 1055 | 1735 | 4 | 1 | 656 | 1485 |
| Sign Control | Stop |  |  | Stop |  |  | Free |  |  | Free |  |  |
| Grade | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |  |
| Peak Hour Factor | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.90 | 0.80 | 0.80 | 0.90 | 0.80 |
| Hourly flow rate (vph) | 236 | 1 | 21 | 10 | 64 | 15 | 1319 | 1928 | 5 | 1 | 729 | 1856 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |

Lane Width ( ft )
Walking Speed (tt/s)
Percent Blockage

| Right turn flare $($ veh $)$ | None | None |
| :--- | :--- | :--- |
| Median type |  |  |
| Median storage veh) |  |  |

Upstream signal (ft)

| pX, platoon unblocked |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| vC, conflicting volume | 6274 | 6230 | 1657 | 6249 | 7156 | 1930 | 2585 | 1933 |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  |  |  |  |  |
| vCu, unblocked vol | 6274 | 6230 | 1657 | 6249 | 7156 | 1930 | 2585 | 1933 |


|  | 6274 | 6230 | 16.5 | 6249 | 756 | 193 | 2585 | 4.1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| CCC, single (s) | 7.2 | 6.5 | 6.5 | 7.2 | 6.5 | 6.3 | 4.2 |  |
| TC, 2 stage (s) | 3.6 | 4.0 | 3.6 | 3.6 | 4.0 | 3.4 | 2.3 | 2.2 |
| tF (s) | 0 | 0 | 80 | 0 | 0 | 81 | 0 | 100 |
| p0 queue free \% | 0 | 0 | 103 | 0 | 0 | 79 | 157 | 309 |


| Direction, Lane \# | EB 1 | WB 1 | NB 1 | SB1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume Total | 258 | 89 | 3252 | 2586 |  |
| Volume Left | 236 | 10 | 1319 | 1 |  |
| Volume Right | 21 | 15 | 5 | 1856 |  |
| cSH | 0 | 0 | 157 | 309 |  |
| Volume to Capacity | Err | Err | 8.40 | 0.00 |  |
| Queue Length 95th (t) | Err | Err | Err | 0 |  |
| Control Delay (s) | Err | Err | 1372.7 | 0.0 |  |
| Lane LOS | F | F | F | A |  |
| Approach Delay (s) | Err | Err | 1372.7 | 0.0 |  |
| Approach LOS | F | F |  |  |  |
| Intersection Summary |  |  |  |  |  |
| Average Delay |  |  | Err |  |  |
| Intersection Capacity Utilization |  |  | 304.0\% | ICU Level of Service | H |
| Analysis Period (min) |  |  | 15 |  |  |

HCM Unsignalized Intersection Capacity Analysis
3: CR 519 Belvidere Rd \& CR 622 Roxbury Station Rd/CR 622 Roxbury Hill Rd

|  | 4 | $\rightarrow$ | $\geqslant$ | 7 |  | 4 | 4 | $\uparrow$ | $>$ | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ¢ |  |  | ¢ |  |  | ¢ |  |  | ¢ |  |  |
| Traffic Volume (veh/h) | 570 | 430 | 1027 | 5 | 1 | 1 | 14 | 586 | 4 | 1144 | 450 | 471 |
| Future Volume (Veh/h) | 570 | 430 | 1027 | 5 | 1 | 1 | 14 | 586 | 4 | 1144 | 450 | 471 |
| Sign Control | Stop |  |  | Stop |  |  | Free |  |  | Free |  |  |
| Grade | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |  |
| Peak Hour Factor | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.90 | 0.80 | 0.80 | 0.90 | 0.80 |
| Hourly flow rate (vph) | 713 | 538 | 1284 | 6 | 1 | 1 | 18 | 651 | 5 | 1430 | 500 | 589 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |

Lane Width ( ft )
Walking Speed (tt/s)
Percent Blockage

| Right turn flare (veh) | None | None |
| :--- | :--- | :--- |
| Median type |  |  |
| Median storage veh) |  |  |

Upstream signal (ft)

| pX, platoon unblocked |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| VC , conflicting volume | 4346 | 4346 | 794 | 5897 | 4638 | 654 | 1089 | 656 |
| $\mathrm{VC1}$, stage 1 conf vol |  |  |  |  |  |  |  |  |
| $\mathrm{VC2}$, stage 2 conf vol |  |  |  |  |  |  |  |  |
| vCu, unblocked vol | 4346 | 4346 | 794 | 5897 | 4638 | 654 | 1089 | 656 |
| tC , single (s) | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.6 | 4.1 |
| $\mathrm{tC}, 2$ stage (s) |  |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.7 | 2.2 |
| p0 queue free \% | 0 | 0 | 0 | 0 | 0 | 100 | 96 | 0 |
| cM capacity (veh/h) | 0 | 0 | 385 | 0 | 0 | 471 | 491 | 941 |


| Direction, Lane \# | EB 1 | WB 1 | NB 1 | SB1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume Total | 2535 | 8 | 674 | 2519 |  |
| Volume Left | 713 | 6 | 18 | 1430 |  |
| Volume Right | 1284 | 1 | 5 | 589 |  |
| cSH | 0 | 0 | 491 | 941 |  |
| Volume to Capacity | Err | Err | 0.04 | 1.52 |  |
| Queue Length 95th (t) | Err | Err | 3 | 1723 |  |
| Control Delay (s) | Err | Err | 1.1 | 253.4 |  |
| Lane LOS | F | F | A | F |  |
| Approach Delay (s) | Err | Err | 1.1 | 253.4 |  |
| Approach LOS | F | F |  |  |  |
| Intersection Summary |  |  |  |  |  |
| Average Delay |  |  | Err |  |  |
| Intersection Capacity Utilization |  |  | 272.3\% | ICU Level of Service | H |
| Analysis Period (min) |  |  | 15 |  |  |

HCM Unsignalized Intersection Capacity Analysis
3: CR 519 Belvidere Rd \& CR 621 Brainards Rd


HCM Unsignalized Intersection Capacity Analysis
3: CR 519 Belvidere Rd \& CR 621 Brainards Rd


HCM Unsignalized Intersection Capacity Analysis
2: CR 646 Belvidere Rd/CR 519 Belvidere Rd \& CR 519 Uniontown Rd


HCM Unsignalized Intersection Capacity Analysis
2: CR 646 Belvidere Rd/CR 519 Belvidere Rd \& CR 519 Uniontown Rd

|  | $\cdots$ | 「 | $\nearrow$ | $\not$ | \% | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | NBL | NBR | NET | NER | SWL | SWT |  |
| Lane Configurations | Y |  | $\uparrow$ |  |  | $\uparrow$ |  |
| Traffic Volume (veh/h) | 12 | 340 | 358 | 5 | 702 | 1334 |  |
| Future Volume (Veh/h) | 12 | 340 | 358 | 5 | 702 | 1334 |  |
| Sign Control | Stop |  | Free |  |  | Free |  |
| Grade | 0\% |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.80 | 0.90 | 0.90 | 0.80 | 0.90 | 0.90 |  |
| Hourly flow rate (vph) | 15 | 378 | 398 | 6 | 780 | 1482 |  |
| Pedestrians |  |  |  |  |  |  |  |
| Lane Width (ft) |  |  |  |  |  |  |  |
| Walking Speed (tt/s) |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |
| Median type |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |
| Upstream signal (tt) |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |
| VC , conflicting volume | 3443 | 401 |  |  | 404 |  |  |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  |  |  |  |
| vCu, unblocked vol | 3443 | 401 |  |  | 404 |  |  |
| tC , single (s) | 6.4 | 6.2 |  |  | 4.1 |  |  |
| $\mathrm{tC}, 2$ stage (s) |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 3.3 |  |  | 2.2 |  |  |
| p0 queue free \% | 0 | 41 |  |  | 31 |  |  |
| cM capacity (veh/h) | 2 | 643 |  |  | 1139 |  |  |
| Direction, Lane \# | NB 1 | NE 1 | SW 1 |  |  |  |  |
| Volume Total | 393 | 404 | 2262 |  |  |  |  |
| Volume Left | 15 | 0 | 780 |  |  |  |  |
| Volume Right | 378 | 6 | 0 |  |  |  |  |
| cSH | 59 | 1700 | 1139 |  |  |  |  |
| Volume to Capacity | 6.66 | 0.24 | 0.69 |  |  |  |  |
| Queue Length 95th (tt) | Err | 0 | 144 |  |  |  |  |
| Control Delay (s) | Err | 0.0 | 14.7 |  |  |  |  |
| Lane LOS | F |  | B |  |  |  |  |
| Approach Delay (s) | Err | 0.0 | 14.7 |  |  |  |  |
| Approach LOS | F |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 1295.5 |  |  |  |  |
| Intersection Capacity UtilizationAnalysis Period (min) |  |  | 159.9\% |  | CU Level of | Service | H |
|  |  |  | 15 |  |  |  |  |

Timings
3: CR 519 Uniontown Rd \& NJ 57

|  | 4 | $\rightarrow$ | 6 | $\Perp$ | 4 | $\dagger$ | - |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT |
| Lane Configurations |  | $\ddagger$ |  | $\ddagger$ |  | \$ |  |  |
| Traffic Volume (vph) | 284 | 356 | 28 | 290 | 36 | 330 | 3 | 125 |
| Future Volume (vph) | 284 | 356 | 28 | 290 | 36 | 330 | 3 | 125 |
| Turn Type | Perm | NA | Perm | NA | Perm | NA | Perm | NA |
| Protected Phases |  | 4 |  | 8 |  | 2 |  | 6 |
| Permitted Phases | 4 |  | 8 |  | 2 |  | 6 |  |
| Detector Phase | 4 | 4 | 8 | 8 | 2 | 2 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 50.0 | 50.0 | 50.0 | 50.0 | 15.0 | 15.0 | 15.0 | 15.0 |
| Minimum Split (s) | 57.0 | 57.0 | 57.0 | 57.0 | 23.0 | 23.0 | 23.0 | 23.0 |
| Total Split (s) | 57.0 | 57.0 | 57.0 | 57.0 | 33.0 | 33.0 | 33.0 | 33.0 |
| Total Split (\%) | 63.3\% | 63.3\% | 63.3\% | 63.3\% | 36.7\% | 36.7\% | 36.7\% | 36.7\% |
| Yellow Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lost Time Adjust (s) |  | 0.0 |  | 0.0 |  | 0.0 |  | 0.0 |
| Total Lost Time (s) |  | 7.0 |  | 7.0 |  | 8.0 |  | 8.0 |
| Lead/Lag |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |
| Recall Mode | C-Max | C-Max | C-Max | C-Max | Min | Min | Min | Min |
| Act Effct Green (s) |  | 50.0 |  | 50.0 |  | 25.0 |  | 25.0 |
| Actuated g/C Ratio |  | 0.56 |  | 0.56 |  | 0.28 |  | 0.28 |
| v/c Ratio |  | 1.18 |  | 0.47 |  | 1.09 |  | 0.42 |
| Control Delay |  | 120.2 |  | 13.7 |  | 100.2 |  | 27.4 |
| Queue Delay |  | 0.0 |  | 0.0 |  | 0.0 |  | 0.0 |
| Total Delay |  | 120.2 |  | 13.7 |  | 100.2 |  | 27.4 |
| LOS |  | F |  | B |  | F |  | C |
| Approach Delay |  | 120.2 |  | 13.7 |  | 100.2 |  | 27.4 |
| Approach LOS |  | F |  | B |  | F |  | C |
| Intersection Summary |  |  |  |  |  |  |  |  |

Cycle Length: 90
Actuated Cycle Length: 90
Offset: 10.9 (12\%), Referenced to phase 4:EBTL and 8:WBTL, Start of Yellow
Natural Cycle: 140

| Control Type: Actuated-Coordinated |  |
| :--- | :--- |
| Maximum v/c Ratio: 1.18 |  |
| Intersection Signal Delay: 81.5 | Intersection LOS: F |
| Intersection Capacity Utilization 142.5\% | ICU Level of Service H |
| Analysis Period (min) 15 |  |

Splits and Phases: 3: CR 519 Uniontown Rd \& NJ 57


Timings
3: CR 519 Uniontown Rd \& NJ 57


Cycle Length: 90
Actuated Cycle Length: 90
Offset: 10.9 (12\%), Referenced to phase 4:EBTL and 8:WBTL, Start of Yellow
Natural Cycle: 140
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 1.57
Intersection Signal Delay: $157.5 \quad$ Intersection LOS: F
Intersection Capacity Utilization 125.5\% ICU Level of Service H
Analysis Period (min) 15
Splits and Phases: 3: CR 519 Uniontown Rd \& NJ 57




HCM Unsignalized Intersection Capacity Analysis
4: CO 632 \& I-78 WB ramp


| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Configurations | M | $\mathbf{7}$ |  | $\boldsymbol{\uparrow}$ | $\boldsymbol{\uparrow}$ |  |
| Traffic Volume e (veh/h $)$ | 1059 | 129 | 0 | 385 | 105 | 0 |
| Future Volume (Veh/h) | 1059 | 129 | 0 | 385 | 105 | 0 |
| Sign Control | Stop |  |  | Free | Free | 0 |
| Grade | $0 \%$ |  |  | $0 \%$ | $0 \%$ |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 1151 | 140 | 0 | 418 | 114 | 0 |
| Pedestrians |  |  |  |  |  |  |

Lane Width ( t )
Walking Speed (tt/s)
Percent Blockage

| Right turn flare (veh) | 6 |  |
| :--- | :--- | :--- |
| Median type | None | None |
| Median storage veh) |  |  |

Upstream signal (ft)

| pX, platoon unblocked |  |  |  |
| :--- | :--- | :--- | :--- |
| VC, conflicting volume | 532 | 114 | 114 |

VC 1 , stage 1 conf vol
$\mathrm{vC2}$, stage 2 conf vol

| vC, , unblocked vol | 532 | 114 | 114 |
| :--- | ---: | ---: | ---: |
| tC , single (s) | 6.4 | 6.2 | 4.1 |


| $\mathrm{tC}, 2$ stage $(\mathrm{s})$ |  |  |  |
| :--- | :--- | :--- | :--- |
| $\mathrm{tF}(\mathrm{s})$ | 3.5 | 3.3 | 2.2 |


| p0 queue free \% | 0 | 85 | 100 |
| :--- | ---: | ---: | ---: |
| cM capacity (veh/h) | 508 | 939 | 1475 |


| Direction, Lane \# | EB 1 | NB 1 | SB 1 |
| :--- | ---: | ---: | ---: |
| Volume Total | 1291 | 418 | 114 |
| Volume Left | 1151 | 0 | 0 |
| Volume Right | 140 | 0 | 0 |
| cSH | 536 | 1700 | 1700 |
| Volume to Capacity | 2.41 | 0.25 | 0.07 |
| Queue Length 95th (tt) | 2482 | 0 | 0 |
| Control Delay (s) | 657.2 | 0.0 | 0.0 |
| Lane LOS | F |  |  |
| Approach Delay (s) | 657.2 | 0.0 | 0.0 |
| Approach LOS | F |  |  |

Intersection Summary
Average Delay 465.4

Intersection Capacity Utilization 85.6\%
Analysis Period (min) $\quad 15$

HCM Unsignalized Intersection Capacity Analysis
4: CO 632 \& I-78 WB ramp


| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Configurations | $\mathbf{T}$ | $\mathbf{7}$ |  | $\mathbf{4}$ | $\boldsymbol{\uparrow}$ |  |
| Traffic Volume (veh/h) | 261 | 52 | 0 | 124 | 328 | 0 |
| Future Volume (Veh/h) | 261 | 52 | 0 | 124 | 328 | 0 |
| Sign Control | Stop |  |  | Free | Free | 0 |
| Grade | $0 \%$ |  |  | $0 \%$ | $0 \%$ |  |
| Peak Hour Factor | 0.92 | 0.92 | 1.00 | 0.92 | 0.92 | 1.00 |
| Hourly flow rate (vph) | 284 | 57 | 0 | 135 | 357 | 0 |
| Pedestrians |  |  |  |  |  |  |

Lane Width ( ft )
Walking Speed (tt/s)
Percent Blockage

| Right turn flare (veh) | 6 |  |  |  |
| :--- | :---: | :--- | :--- | :--- |
| Median type |  | None | None |  |
| Median storage veh) |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |
| vC, conflicting volume | 492 | 357 | 357 |  |

VC1, stage 1 conf vol

| vCu, unblocked vol | 492 | 357 | 357 |
| :--- | :--- | :--- | :--- |


| tC , single (s) | 6.4 | 6.2 | 4.1 |
| :--- | :--- | :--- | :--- |


| $\mathrm{tC}, 2$ stage $(\mathrm{s})$ |  |  |  |
| :--- | :--- | :--- | :--- |
| $\mathrm{tF}(\mathrm{s})$ | 3.5 | 3.3 | 2.2 |


| p0 queue free \% | 47 | 92 | 100 |
| :--- | ---: | ---: | ---: |
| cM capacity (veh/h) | 536 | 687 | 1202 |


| Direction, Lane \# | EB 1 | NB 1 | SB 1 |
| :--- | ---: | ---: | ---: |
| Volume Total | 341 | 135 | 357 |
| Volume Left | 284 | 0 | 0 |
| Volume Right | 57 | 0 | 0 |
| cSH | 644 | 1700 | 1700 |
| Volume to Capacity | 0.53 | 0.08 | 0.21 |
| Queue Length 95th (tt) | 78 | 0 | 0 |
| Control Delay (s) | 17.6 | 0.0 | 0.0 |
| Lane LOS | C |  |  |
| Approach Delay (s) | 17.6 | 0.0 | 0.0 |
| Approach LOS | C |  |  |

Intersection Summary

| Average Delay | 7.2 |  |  |
| :--- | ---: | :--- | :--- |
| Intersection Capacity Utilization | $38.4 \%$ | ICU Level of Service | A |
| Analysis Period (min) | 15 |  |  |

2045 BUILD MID-BLOCK ANALYSIS

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/16/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, northeast of CO <br> 610 | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 3 |
| Speed Limit, mi/h | Access Point Density, pts $/ \mathrm{mi}$ | 9.0 |  |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 343 | Opposing Demand Flow Rate, veh/h | 879 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.92 | Total Trucks, \% | 2.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.20 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 52.6 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.31611 | Speed Power Coefficient | 0.44498 |
| PF Slope Coefficient | -1.32825 | PF Power Coefficient | 0.75770 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 3.0 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 50.8 |

## Vehicle Results

| Average Speed, mi/h | 50.8 | Percent Followers, \% | 44.6 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.18 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 3.0 |
| Vehicle LOS | B |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/16/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, northeast of CO <br> 610 | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 3 |
| Speed Limit, mi/h | Access Point Density, pts $/ \mathrm{mi}$ | 9.0 |  |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 879 | Opposing Demand Flow Rate, veh/h | 343 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.92 | Total Trucks, \% | 2.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.52 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 52.6 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.20083 | Speed Power Coefficient | 0.50667 |
| PF Slope Coefficient | -1.26944 | PF Power Coefficient | 0.77916 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 12.1 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 49.8 |

## Vehicle Results

| Average Speed, mi/h | 49.8 | Percent Followers, \% | 68.3 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.21 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 12.1 |
| Vehicle LOS | D |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/16/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, northeast of CO <br> 610 | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 3 |
| Speed Limit, mi/h | Access Point Density, pts $/ \mathrm{mi}$ | 9.0 |  |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 614 | Opposing Demand Flow Rate, veh/h | 399 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.92 | Total Trucks, \% | 2.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.36 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 52.6 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.21576 | Speed Power Coefficient | 0.49701 |
| PF Slope Coefficient | -1.27872 | PF Power Coefficient | 0.77628 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 7.1 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 50.3 |

## Vehicle Results

| Average Speed, mi/h | 50.3 | Percent Followers, \% | 58.3 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.19 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 7.1 |
| Vehicle LOS | C |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, northeast of CO <br> 610 | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 3 |
| Speed Limit, mi/h | Access Point Density, pts/mi | 9.0 |  |
| Demand and Capacity | 50 | Opposing Demand Flow Rate, veh/h | 303 |
| Directional Demand Flow Rate, veh/h | 399 | Total Trucks, \% | 2.00 |
| Peak Hour Factor | 0.92 | Demand/Capacity (D/C) | 0.23 |
| Segment Capacity, veh/h | 1700 |  |  |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 52.6 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.18924 | Speed Power Coefficient | 0.51453 |
| PF Slope Coefficient | -1.26192 | PF Power Coefficient | 0.78143 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 3.6 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, mi/h |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 50.9 |

## Vehicle Results

| Average Speed, mi/h | 50.9 | Percent Followers, \% | 46.0 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.18 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 3.6 |
| Vehicle LOS | B |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/17/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, Stone Hedge Rd <br> to Hope Crossing Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Constrained | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts $/ \mathrm{mi}$ | 0.0 |  |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 385 | Opposing Demand Flow Rate, veh/h | - |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.80 | Total Trucks, \% | 3.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.23 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 56.9 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.64416 | Speed Power Coefficient | 0.41674 |
| PF Slope Coefficient | -1.32222 | PF Power Coefficient | 0.75266 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 3.3 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 54.7 |

## Vehicle Results

| Average Speed, mi/h | 54.7 | Percent Followers, \% | 47.5 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.10 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 3.3 |
| Vehicle LOS | B |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/17/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, Stone Hedge Rd <br> to Hope Crossing Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Constrained | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts $/ \mathrm{mi}$ | 0.0 |  |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 887 | Opposing Demand Flow Rate, veh/h | - |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.84 | Total Trucks, \% | 3.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.52 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 56.9 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.64416 | Speed Power Coefficient | 0.41674 |
| PF Slope Coefficient | -1.32222 | PF Power Coefficient | 0.75266 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 11.6 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.6 |

## Vehicle Results

| Average Speed, mi/h | 53.6 | Percent Followers, \% | 70.1 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.12 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 11.6 |
| Vehicle LOS | D |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/17/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, Stone Hedge Rd <br> to Hope Crossing Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Constrained | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts $/ \mathrm{mi}$ | 0.0 |  |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 334 | Opposing Demand Flow Rate, veh/h | - |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.90 | Total Trucks, \% | 3.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.20 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 56.9 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.64416 | Speed Power Coefficient | 0.41674 |
| PF Slope Coefficient | -1.32222 | PF Power Coefficient | 0.75266 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 2.7 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 54.9 |

## Vehicle Results

| Average Speed, mi/h | 54.9 | Percent Followers, \% | 44.0 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.09 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 2.7 |
| Vehicle LOS | B |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/17/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, Stone Hedge Rd <br> to Hope Crossing Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Constrained | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts $/ \mathrm{mi}$ | 0.0 |  |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 427 | Opposing Demand Flow Rate, veh/h | - |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.82 | Total Trucks, \% | 3.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.25 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 56.9 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.64416 | Speed Power Coefficient | 0.41674 |
| PF Slope Coefficient | -1.32222 | PF Power Coefficient | 0.75266 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 3.9 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 54.6 |

## Vehicle Results

| Average Speed, mi/h | 54.6 | Percent Followers, \% | 50.2 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.10 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 3.9 |
| Vehicle LOS | B |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/16/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, CO 623 Brass <br> Castle Rd to Pequest Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | 50 | Access Point Density, pts $/ \mathrm{mi}$ | 4.0 |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 567 | Opposing Demand Flow Rate, veh/h | 1159 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.88 | Total Trucks, \% | 0.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.33 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.7 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.53055 | Speed Power Coefficient | 0.42884 |
| PF Slope Coefficient | -1.32485 | PF Power Coefficient | 0.75803 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 6.2 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.2 |

## Vehicle Results

| Average Speed, mi/h | 53.2 | Percent Followers, \% | 57.8 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.13 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 6.2 |
| Vehicle LOS | C |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/16/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, CO 623 Brass <br> Castle Rd to Pequest Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | 50 | Access Point Density, pts $/ \mathrm{mi}$ | 4.0 |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 1109 | Opposing Demand Flow Rate, veh/h | 542 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.92 | Total Trucks, \% | 0.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.65 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.7 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.41906 | Speed Power Coefficient | 0.47664 |
| PF Slope Coefficient | -1.28592 | PF Power Coefficient | 0.77876 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 15.9 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 52.3 |

## Vehicle Results

| Average Speed, mi/h | 52.3 | Percent Followers, \% | 75.2 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.15 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 15.9 |
| Vehicle LOS | E |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/16/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, CO 623 Brass <br> Castle Rd to Pequest Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | 50 | Access Point Density, pts/mi | 4.0 |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 971 | Opposing Demand Flow Rate, veh/h | 481 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.85 | Total Trucks, \% | 7.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.57 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.5 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.39239 | Speed Power Coefficient | 0.48463 |
| PF Slope Coefficient | -1.27901 | PF Power Coefficient | 0.78178 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 13.2 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 52.3 |

## Vehicle Results

| Average Speed, mi/h | 52.3 | Percent Followers, $\%$ | 71.3 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.15 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 13.2 |
| Vehicle LOS | D |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/16/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, CO 623 Brass <br> Castle Rd to Pequest Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | 50 | Access Point Density, pts/mi | 4.0 |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 431 | Opposing Demand Flow Rate, veh/h | 868 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.95 | Total Trucks, \% | 7.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.25 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.5 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.47048 | Speed Power Coefficient | 0.44577 |
| PF Slope Coefficient | -1.31265 | PF Power Coefficient | 0.76717 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 4.0 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.3 |

## Vehicle Results

| Average Speed, mi/h | 53.3 | Percent Followers, \% | 49.7 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.12 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 4.0 |
| Vehicle LOS | B |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, CO 620 to <br> Brookfield Dr | Unit | United States Customary |

Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 11 | Shoulder Width, ft | 5 |
| Speed Limit, mi/h | 50 | Access Point Density, pts/mi | 2.0 |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 369 | Opposing Demand Flow Rate, veh/h | 1759 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.85 | Total Trucks, \% | 2.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.22 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.1 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.58166 | Speed Power Coefficient | 0.41151 |
| PF Slope Coefficient | -1.33664 | PF Power Coefficient | 0.74144 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 3.3 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.0 |

## Vehicle Results

| Average Speed, $\mathrm{mi} / \mathrm{h}$ | 53.0 | Percent Followers, $\%$ | 47.2 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.13 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 3.3 |
| Vehicle LOS | B |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, CO 620 to <br> Brookfield Dr | Unit | United States Customary |

Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 11 | Shoulder Width, ft | 5 |
| Speed Limit, mi/h | 50 | Access Point Density, pts $/ \mathrm{mi}$ | 2.0 |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 1718 | Opposing Demand Flow Rate, veh/h | 361 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.87 | Total Trucks, \% | 2.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 1.01 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.1 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.34386 | Speed Power Coefficient | 0.50350 |
| PF Slope Coefficient | -1.26381 | PF Power Coefficient | 0.78594 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 1.9 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.7 |

## Vehicle Results

| Average Speed, mi/h | 53.7 | Percent Followers, $\%$ | 36.7 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.12 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 1.9 |
| Vehicle LOS | F |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, CO 620 to <br> Brookfield Dr | Unit | United States Customary |

Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 11 | Shoulder Width, ft | 5 |
| Speed Limit, mi/h | 50 | Access Point Density, pts/mi | 2.0 |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 1420 | Opposing Demand Flow Rate, veh/h | 292 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.91 | Total Trucks, \% | 2.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.84 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.1 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.32416 | Speed Power Coefficient | 0.51681 |
| PF Slope Coefficient | -1.25158 | PF Power Coefficient | 0.78984 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 22.4 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 51.3 |

## Vehicle Results

| Average Speed, mi/h | 51.3 | Percent Followers, $\%$ | 80.8 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.17 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 22.4 |
| Vehicle LOS | E |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | $6 / 16 / 2020$ |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, CO 620 to <br> Brookfield Dr | Unit | United States Customary |

Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 11 | Shoulder Width, ft | 5 |
| Speed Limit, mi/h | Access Point Density, pts $/ \mathrm{mi}$ | 2.0 |  |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 296 | Opposing Demand Flow Rate, veh/h | 1436 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.90 | Total Trucks, \% | 2.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.17 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.1 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.53968 | Speed Power Coefficient | 0.41853 |
| PF Slope Coefficient | -1.33454 | PF Power Coefficient | 0.74933 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 2.3 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.3 |

## Vehicle Results

| Average Speed, mi/h | 53.3 | Percent Followers, \% | 41.5 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.12 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 2.3 |
| Vehicle LOS | A |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/16/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, Reeder Rd to Grist <br> Mill Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts $/ \mathrm{mi}$ | 5.0 |  |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 2948 | Opposing Demand Flow Rate, veh/h | 635 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.92 | Total Trucks, \% | 7.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 1.73 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.2 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.36841 | Speed Power Coefficient | 0.49086 |
| PF Slope Coefficient | -1.27444 | PF Power Coefficient | 0.78305 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 4.4 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.2 |

## Vehicle Results

| Average Speed, mi/h | 53.2 | Percent Followers, \% | 50.5 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.13 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 4.4 |
| Vehicle LOS | F |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/16/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, Reeder Rd to Grist <br> Mill Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | 50 | Access Point Density, pts/mi | 5.0 |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 635 | Opposing Demand Flow Rate, veh/h | 2948 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.92 | Total Trucks, \% | 7.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.37 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.2 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.71426 | Speed Power Coefficient | 0.41457 |
| PF Slope Coefficient | -1.31276 | PF Power Coefficient | 0.71807 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 7.4 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 52.4 |

## Vehicle Results

| Average Speed, $\mathrm{mi} / \mathrm{h}$ | 52.4 | Percent Followers, \% | 61.2 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.15 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 7.4 |
| Vehicle LOS | C |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/16/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, Reeder Rd to Grist <br> Mill Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | Access Point Density, pts $/ \mathrm{mi}$ | 5.0 |  |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 547 | Opposing Demand Flow Rate, veh/h | 1650 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.92 | Total Trucks, \% | 3.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.32 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.4 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.57974 | Speed Power Coefficient | 0.41336 |
| PF Slope Coefficient | -1.33472 | PF Power Coefficient | 0.74476 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 5.9 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 52.8 |

## Vehicle Results

| Average Speed, mi/h | 52.8 | Percent Followers, \% | 57.3 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.14 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 5.9 |
| Vehicle LOS | C |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/16/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, Reeder Rd to Grist <br> Mill Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 6 |
| Speed Limit, mi/h | 50 | Access Point Density, pts/mi | 5.0 |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 1650 | Opposing Demand Flow Rate, veh/h | 547 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.92 | Total Trucks, \% | 3.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.97 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 55.4 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.40106 | Speed Power Coefficient | 0.47611 |
| PF Slope Coefficient | -1.28762 | PF Power Coefficient | 0.77801 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 27.4 |
| \%lmproved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 51.2 |

## Vehicle Results

| Average Speed, mi/h | 51.2 | Percent Followers, \% | 85.1 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.17 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 27.4 |
| Vehicle LOS | E |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/17/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, Fairway Rd to <br> Hillside Ave | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 5 |
| Speed Limit, mi/h | 50 | Access Point Density, pts/mi | 4.0 |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 985 | Opposing Demand Flow Rate, veh/h | 372 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.78 | Total Trucks, \% | 3.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.58 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 54.9 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.33416 | Speed Power Coefficient | 0.50158 |
| PF Slope Coefficient | -1.26634 | PF Power Coefficient | 0.78482 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 13.6 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 51.8 |

## Vehicle Results

| Average Speed, mi/h | 51.8 | Percent Followers, \% | 71.4 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.16 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 13.6 |
| Vehicle LOS | D |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/17/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 519, Fairway Rd to <br> Hillside Ave | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 5 |
| Speed Limit, mi/h | 50 | Access Point Density, pts/mi | 4.0 |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 312 | Opposing Demand Flow Rate, veh/h | 826 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.93 | Total Trucks, \% | 3.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.18 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 54.9 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.43217 | Speed Power Coefficient | 0.44894 |
| PF Slope Coefficient | -1.31349 | PF Power Coefficient | 0.76638 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 2.4 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 53.2 |

## Vehicle Results

| Average Speed, $\mathrm{mi} / \mathrm{h}$ | 53.2 | Percent Followers, $\%$ | 41.6 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.13 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 2.4 |
| Vehicle LOS | A |  |  |

[^53]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/17/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, Fairway Rd to <br> Hillside Ave | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 5 |
| Speed Limit, mi/h | 50 | Access Point Density, pts $/ \mathrm{mi}$ | 4.0 |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 481 | Opposing Demand Flow Rate, veh/h | 896 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.78 | Total Trucks, \% | 3.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.28 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 54.9 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.44460 | Speed Power Coefficient | 0.44381 |
| PF Slope Coefficient | -1.31778 | PF Power Coefficient | 0.76409 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 4.8 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 52.7 |

## Vehicle Results

| Average Speed, mi/h | 52.7 | Percent Followers, \% | 52.9 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.14 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 4.8 |
| Vehicle LOS | B |  |  |

[^54]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/17/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 519, Fairway Rd to <br> Hillside Ave | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 5 |
| Speed Limit, mi/h | 50 | Access Point Density, pts/mi | 4.0 |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 803 | Opposing Demand Flow Rate, veh/h | 431 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.87 | Total Trucks, \% | 3.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.47 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 54.9 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 3.34950 | Speed Power Coefficient | 0.49192 |
| PF Slope Coefficient | -1.27520 | PF Power Coefficient | 0.78186 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 10.2 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 52.1 |

## Vehicle Results

| Average Speed, mi/h | 52.1 | Percent Followers, \% | 65.9 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.15 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 10.2 |
| Vehicle LOS | D |  |  |

[^55]
## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/16/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 632, Shurts Rd to Halls <br> Mill Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 3 |
| Speed Limit, mi/h | Access Point Density, pts $/ \mathrm{mi}$ | 8.0 |  |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 565 | Opposing Demand Flow Rate, veh/h | 305 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.92 | Total Trucks, \% | 6.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.33 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 46.7 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 2.87101 | Speed Power Coefficient | 0.51408 |
| PF Slope Coefficient | -1.27182 | PF Power Coefficient | 0.76259 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 7.1 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 44.8 |

## Vehicle Results

| Average Speed, mi/h | 44.8 | Percent Followers, \% | 56.1 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.34 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 7.1 |
| Vehicle LOS | C |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/16/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 632, Shurts Rd to Halls <br> Mill Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 3 |
| Speed Limit, mi/h | Access Point Density, pts $/ \mathrm{mi}$ | 8.0 |  |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 590 | Opposing Demand Flow Rate, veh/h | 529 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.92 | Total Trucks, \% | 4.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.35 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 46.8 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 2.93196 | Speed Power Coefficient | 0.47827 |
| PF Slope Coefficient | -1.30994 | PF Power Coefficient | 0.75172 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 7.7 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 44.7 |

## Vehicle Results

| Average Speed, mi/h | 44.7 | Percent Followers, \% | 58.6 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.34 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 7.7 |
| Vehicle LOS | C |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/16/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | AM Peak Hour |
| Project Description | CR 632, Shurts Rd to Halls <br> Mill Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 3 |
| Speed Limit, mi/h | Access Point Density, pts $/ \mathrm{mi}$ | 8.0 |  |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 305 | Opposing Demand Flow Rate, veh/h | 565 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.92 | Total Trucks, \% | 6.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.18 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 46.7 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 2.93629 | Speed Power Coefficient | 0.47388 |
| PF Slope Coefficient | -1.31456 | PF Power Coefficient | 0.75033 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 2.8 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 45.3 |

## Vehicle Results

| Average Speed, mi/h | 45.3 | Percent Followers, $\%$ | 41.7 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.32 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 2.8 |
| Vehicle LOS | B |  |  |

## HCS7 Two-Lane Highway Report

## Project Information

| Analyst | MAA | Date | 6/16/2020 |
| :--- | :--- | :--- | :--- |
| Agency | WSP | Analysis Year | 2020 |
| Jurisdiction |  | Time Period Analyzed | PM Peak Hour |
| Project Description | CR 632, Shurts Rd to Halls <br> Mill Rd | Unit | United States Customary |

## Segment 1

## Vehicle Inputs

| Segment Type | Passing Zone | Length, ft | 5280 |
| :--- | :--- | :--- | :--- |
| Lane Width, ft | 12 | Shoulder Width, ft | 3 |
| Speed Limit, mi/h | Access Point Density, pts $/ \mathrm{mi}$ | 8.0 |  |

## Demand and Capacity

| Directional Demand Flow Rate, veh/h | 529 | Opposing Demand Flow Rate, veh/h | 590 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.92 | Total Trucks, \% | 4.00 |
| Segment Capacity, veh/h | 1700 | Demand/Capacity (D/C) | 0.31 |

## Intermediate Results

| Segment Vertical Class | 1 | Free-Flow Speed, mi/h | 46.8 |
| :--- | :--- | :--- | :--- |
| Speed Slope Coefficient | 2.94529 | Speed Power Coefficient | 0.47099 |
| PF Slope Coefficient | -1.31790 | PF Power Coefficient | 0.74929 |
| In Passing Lane Effective Length? | No | Total Segment Density, veh/mi/ln | 6.6 |
| \%Improved \% Followers | 0.0 | \% Improved Avg Speed | 0.0 |

## Subsegment Data

| $\#$ | Segment Type | Length, ft | Radius, ft | Superelevation, \% | Average Speed, $\mathrm{mi} / \mathrm{h}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | Tangent | 5280 | - | - | 44.8 |

## Vehicle Results

| Average Speed, mi/h | 44.8 | Percent Followers, \% | 55.9 |
| :--- | :--- | :--- | :--- |
| Segment Travel Time, minutes | 1.34 | Followers Density, followers $/ \mathrm{mi} / \mathrm{ln}$ | 6.6 |
| Vehicle LOS | C |  |  |

## 2045 BUILD MITIGATION ANALYSIS

Timings
3: RT 519 \& US 46


## Cycle Length: 90

Actuated Cycle Length: 90
Natural Cycle: 110
Control Type: Semi Act-Uncoord
Maximum v/c Ratio: 1.07
Intersection Signal Delay: 63.0
Intersection LOS: E
Intersection Capacity Utilization 118.7\% ICU Level of Service H
Analysis Period (min) 15
Splits and Phases: 3: RT 519 \& US 46


Timings
3: RT 519 \& US 46


Cycle Length: 90
Actuated Cycle Length: 90
Natural Cycle: 90
Control Type: Semi Act-Uncoord
Maximum v/c Ratio: 1.05
Intersection Signal Delay: 46.6
Intersection LOS: D
Intersection Capacity Utilization 93.2\%
ICU Level of Service F
Analysis Period (min) 15
Splits and Phases: 3: RT 519 \& US 46


Timings
3: CR 519 \& CR 623


## Cycle Length: 90

Actuated Cycle Length: 88.7
Natural Cycle: 75
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 1.08
Intersection Signal Delay: $46.8 \quad$ Intersection LOS: D
Intersection Capacity Utilization 96.3\% ICU Level of Service F
Analysis Period (min) 15
Splits and Phases: 3: CR 519 \& CR 623


Timings
3: CR 519 \& CR 623


Cycle Length: 90
Actuated Cycle Length: 85.2
Natural Cycle: 60
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.91
Intersection Signal Delay: 30.0
Intersection LOS: C
Intersection Capacity Utilization 87.9\%
ICU Level of Service E
Analysis Period (min) 15
Splits and Phases: 3: CR 519 \& CR 623


Timings
3: CO 620 \& RT 519

|  |  |  |  |  | $\pm$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | 71 | T | 44 | F | ${ }^{1}$ | 44 |
| Traffic Volume (vph) | 1501 | 75 | 843 | 300 | 13 | 1734 |
| Future Volume (vph) | 1501 | 75 | 843 | 300 | 13 | 1734 |
| Turn Type | Prot | Perm | NA | Perm | Perm | NA |
| Protected Phases | 8 |  | 2 |  |  | 6 |
| Permitted Phases |  | 8 |  | 2 | 6 |  |
| Detector Phase | 8 | 8 | 2 | 2 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 |
| Total Split (s) | 43.0 | 43.0 | 47.0 | 47.0 | 47.0 | 47.0 |
| Total Split (\%) | 47.8\% | 47.8\% | 52.2\% | 52.2\% | 52.2\% | 52.2\% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Lead/Lag |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |
| Recall Mode | None | None | C-Max | C-Max | C-Max | C-Max |
| Act Effct Green (s) | 38.5 | 38.5 | 42.5 | 42.5 | 42.5 | 42.5 |
| Actuated g/C Ratio | 0.43 | 0.43 | 0.47 | 0.47 | 0.47 | 0.47 |
| v/c Ratio | 1.14 | 0.13 | 0.56 | 0.36 | 0.09 | 1.15 |
| Control Delay | 96.7 | 5.6 | 18.7 | 2.8 | 14.8 | 101.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 96.7 | 5.6 | 18.7 | 2.8 | 14.8 | 101.2 |
| LOS | F | A | B | A | B | F |
| Approach Delay | 91.9 |  | 14.5 |  |  | 100.5 |
| Approach LOS | F |  | B |  |  | F |
| Intersection Summary |  |  |  |  |  |  |
| Cycle Length: 90 |  |  |  |  |  |  |
| Actuated Cycle Length: 90 |  |  |  |  |  |  |
| Offset: 0 (0\%), Referenced to phase 2:NBT and 6:SBTL, Start of Green |  |  |  |  |  |  |
| Natural Cycle: 130 |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.15 |  |  |  |  |  |  |
| Intersection Signal Delay: 75.5 |  |  |  | In | tersectio | LOS: E |
| Intersection Capacity Utilization 98.3\% |  |  |  |  | U Level | of Service F |
| Analysis Period (min) 15 |  |  |  |  |  |  |

Splits and Phases: 3: CO 620 \& RT 519


[^56] WSP

Timings
3: CO 620 \& RT 519

|  |  |  |  |  | - |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | ${ }^{1 / 1}$ | F | 44 | 「 | ${ }^{1}$ | 44 |
| Traffic Volume (vph) | 364 | 513 | 2236 | 1280 | 9 | 756 |
| Future Volume (vph) | 364 | 513 | 2236 | 1280 | 9 | 756 |
| Turn Type | Prot | Perm | NA | Perm | Perm | NA |
| Protected Phases | 8 |  | 2 |  |  | 6 |
| Permitted Phases |  | 8 |  | 2 | 6 |  |
| Detector Phase | 8 | 8 | 2 | 2 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 |
| Total Split (s) | 30.0 | 30.0 | 60.0 | 60.0 | 60.0 | 60.0 |
| Total Split (\%) | 33.3\% | 33.3\% | 66.7\% | 66.7\% | 66.7\% | 66.7\% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Lead/Lag |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |
| Recall Mode | None | None | C-Max | C-Max | C-Max | C-Max |
| Act Effct Green (s) | 25.5 | 25.5 | 55.5 | 55.5 | 55.5 | 55.5 |
| Actuated g/C Ratio | 0.28 | 0.28 | 0.62 | 0.62 | 0.62 | 0.62 |
| v/c Ratio | 0.42 | 1.42 | 1.14 | 1.02 | 0.13 | 0.38 |
| Control Delay | 27.8 | 230.6 | 88.3 | 36.0 | 11.9 | 9.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 27.8 | 230.6 | 88.3 | 36.0 | 11.9 | 9.3 |
| LOS | C | F | F | D | B | A |
| Approach Delay | 152.2 |  | 69.3 |  |  | 9.3 |
| Approach LOS | F |  | E |  |  | A |
| Intersection Summary |  |  |  |  |  |  |
| Cycle Length: 90 |  |  |  |  |  |  |
| Actuated Cycle Length: 90 |  |  |  |  |  |  |
| Offset: $0(0 \%)$, Referenced to phase 2:NBT and 6:SBTL, Start of Green |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.42 |  |  |  |  |  |  |
| Intersection Signal Delay: 75.4 |  |  |  |  | tersectio | LOS: E |
| Intersection Capacity Utilization 101.1\% |  |  |  |  | U Level | of Servic |
| Analysis Period (min) 15 |  |  |  |  |  |  |

Splits and Phases: $\quad 3:$ CO 620 \& RT 519


[^57]Timings
3: CR 519 Belvidere Rd \& Foul Lift Rd


Cycle Length: 90
Actuated Cycle Length: 90
Offset: $0(0 \%)$, Referenced to phase 2:NBTL and $6: S B T$, Start of Green
Natural Cycle: 55
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 5.72
Intersection Signal Delay: $305.3 \quad$ Intersection LOS: F
Intersection Capacity Utilization 103.6\% ICU Level of Service G
Analysis Period (min) 15
Splits and Phases: 3: CR 519 Belvidere Rd \& Foul Lift Rd


Timings
3: CR 519 Belvidere Rd \& Foul Lift Rd


Cycle Length: 90
Actuated Cycle Length: 90
Offset: $0(0 \%)$, Referenced to phase $2:$ NBTL and $6: S B T$, Start of Green
Natural Cycle: 150

| Control Type: Actuated-Coordinated |  |
| :--- | :--- |
| Maximum v/c Ratio: 1.40 |  |
| Intersection Signal Delay: 127.2 | Intersection LOS: F |
| Intersection Capacity Utilization 101.8\% | ICU Level of Service G |
| Analysis Period (min) 15 |  |

Splits and Phases: 3: CR 519 Belvidere Rd \& Foul Lift Rd


Timings
3: RT 519 \& CO 626

|  | 7 |  | 4 |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | WBL | WBR | NBT | SBL | SBT |
| Lane Configurations | \% | $\overline{7}$ | 个t |  | *个4 |
| Traffic Volume (vph) | 188 | 250 | 427 | 100 | 3060 |
| Future Volume (vph) | 188 | 250 | 427 | 100 | 3060 |
| Turn Type | Prot | Perm | NA | Perm | NA |
| Protected Phases | 8 |  | 2 |  | 6 |
| Permitted Phases |  | 8 |  | 6 |  |
| Detector Phase | 8 | 8 | 2 | 6 | 6 |
| Switch Phase |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 |
| Total Split (s) | 22.5 | 22.5 | 67.5 | 67.5 | 67.5 |
| Total Split (\%) | 25.0\% | 25.0\% | 75.0\% | 75.0\% | 75.0\% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 |  | 0.0 |
| Total Lost Time (s) | 4.5 | 4.5 | 4.5 |  | 4.5 |
| Lead/Lag |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |
| Recall Mode | None | None | Min | Min | Min |
| Act Effct Green (s) | 15.4 | 15.4 | 63.1 |  | 63.1 |
| Actuated g/C Ratio | 0.18 | 0.18 | 0.72 |  | 0.72 |
| v/c Ratio | 0.75 | 0.58 | 0.18 |  | 1.05 |
| Control Delay | 50.0 | 8.7 | 4.4 |  | 45.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 |  | 0.0 |
| Total Delay | 50.0 | 8.7 | 4.4 |  | 45.6 |
| LOS | D | A | A |  | D |
| Approach Delay | 26.4 |  | 4.4 |  | 45.6 |
| Approach LOS | C |  | A |  | D |
| Intersection Summary |  |  |  |  |  |

## Cycle Length: 90

Actuated Cycle Length: 87.5
Natural Cycle: 110
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 1.05
Intersection Signal Delay: 38.9 Intersection LOS: D
Intersection Capacity Utilization 94.7\% ICU Level of Service F
Analysis Period (min) 15
Splits and Phases: 3: RT 519 \& CO 626


Timings
3: RT 519 \& CO 626


## Cycle Length: 90

Actuated Cycle Length: 69.6
Natural Cycle: 60
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.64
Intersection Signal Delay: 5.9
Intersection LOS: A
Intersection Capacity Utilization 57.8\%
ICU Level of Service B
Analysis Period (min) 15
Splits and Phases: 3: RT 519 \& CO 626


Timings
3: CR 519 Belvidere Rd \& CR 622 Roxbury Station Rd/CR 622 Roxbury Hill Rd

|  |  |  |  |  |  | 4 | $\dagger$ |  |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | F |  | ¢ | \% | 个 ${ }^{\text {a }}$ | ${ }^{7}$ | 个4 | F |
| Traffic Volume (vph) | 189 | 1 | 17 | 8 | 51 | 1055 | 1735 | 1 | 656 | 1485 |
| Future Volume (vph) | 189 | 1 | 17 | 8 | 51 | 1055 | 1735 | 1 | 656 | 1485 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | NA | Perm | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 2 |  | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 2 |  | 6 |  | 6 |
| Detector Phase | 4 | 4 | 4 | 8 | 8 | 2 | 2 | 6 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 |
| Total Split (s) | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 67.5 | 67.5 | 67.5 | 67.5 | 67.5 |
| Total Split (\%) | 25.0\% | 25.0\% | 25.0\% | 25.0\% | 25.0\% | 75.0\% | 75.0\% | 75.0\% | 75.0\% | 75.0\% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) |  | 4.5 | 4.5 |  | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | None | None | None | None | None | C-Max | C-Max | C-Max | C-Max | C-Max |
| Act Effct Green (s) |  | 18.0 | 18.0 |  | 18.0 | 63.0 | 63.0 | 63.0 | 63.0 | 63.0 |
| Actuated g/C Ratio |  | 0.20 | 0.20 |  | 0.20 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 |
| v/c Ratio |  | 0.98 | 0.08 |  | 0.25 | 3.05 | 0.83 | 0.01 | 0.31 | 1.58 |
| Control Delay |  | 91.4 | 13.3 |  | 29.1 | 944.8 | 13.6 | 5.0 | 5.6 | 280.9 |
| Queue Delay |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 91.4 | 13.3 |  | 29.1 | 944.8 | 13.6 | 5.0 | 5.6 | 280.9 |
| LOS |  | F | B |  | C | F | B | A | A | F |
| Approach Delay |  | 85.0 |  |  | 29.1 |  | 391.3 |  | 203.2 |  |
| Approach LOS |  | F |  |  | c |  | F |  | F |  |

## Intersection Summary

Cycle Length: 90
Actuated Cycle Length: 90
Offset: $0(0 \%)$, Referenced to phase 2:NBTL and 6:SBTL, Start of Green
Natural Cycle: 150
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 3.05
Intersection Signal Delay: 294.7 Intersection LOS: F
Intersection Capacity Utilization 165.8\% ICU Level of Service H
Analysis Period (min) 15
Splits and Phases: 3: CR 519 Belvidere Rd \& CR 622 Roxbury Station Rd/CR 622 Roxbury Hill Rd


Timings
3：CR 519 Belvidere Rd \＆CR 622 Roxbury Station Rd／CR 622 Roxbury Hill Rd

|  |  |  |  |  |  | 4 | $\dagger$ | $\checkmark$ | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | 「 |  | ¢ | 7 | 性 | \％ | 个 $\uparrow$ | 「 |
| Traffic Volume（vph） | 570 | 430 | 1027 | 5 | 1 | 14 | 586 | 1144 | 450 | 471 |
| Future Volume（vph） | 570 | 430 | 1027 | 5 | 1 | 14 | 586 | 1144 | 450 | 471 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | NA | Perm | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 2 |  | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 2 |  | 6 |  | 6 |
| Detector Phase | 4 | 4 | 4 | 8 | 8 | 2 | 2 | 6 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split（s） | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 |
| Total Split（s） | 41.0 | 41.0 | 41.0 | 41.0 | 41.0 | 49.0 | 49.0 | 49.0 | 49.0 | 49.0 |
| Total Split（\％） | 45．6\％ | 45．6\％ | 45．6\％ | 45．6\％ | 45．6\％ | 54．4\％ | 54．4\％ | 54．4\％ | 54．4\％ | 54．4\％ |
| Yellow Time（s） | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All－Red Time（s） | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust（s） |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） |  | 4.5 | 4.5 |  | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Lead／Lag |  |  |  |  |  |  |  |  |  |  |
| Lead－Lag Optimize？ |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | None | None | None | None | None | C－Max | C－Max | C－Max | C－Max | C－Max |
| Act Effct Green（s） |  | 36.5 | 36.5 |  | 36.5 | 44.5 | 44.5 | 44.5 | 44.5 | 44.5 |
| Actuated g／C Ratio |  | 0.41 | 0.41 |  | 0.41 | 0.49 | 0.49 | 0.49 | 0.49 | 0.49 |
| v／c Ratio |  | 2.04 | 1.60 |  | 0.02 | 0.07 | 0.40 | 4.41 | 0.31 | 0.65 |
| Control Delay |  | 495.5 | 295.2 |  | 15.3 | 12.9 | 15.3 | 1554.9 | 14.2 | 5.0 |
| Queue Delay |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 495.5 | 295.2 |  | 15.3 | 12.9 | 15.3 | 1554.9 | 14.2 | 5.0 |
| LOS |  | F | F |  | B | B | B | F | B | A |
| Approach Delay |  | 394.0 |  |  | 15.3 |  | 15.2 |  | 886.7 |  |
| Approach LOS |  | F |  |  | B |  | B |  | F |  |

## Intersection Summary

Cycle Length： 90
Actuated Cycle Length： 90
Offset： $0(0 \%)$ ，Referenced to phase 2：NBTL and 6：SBTL，Start of Green
Natural Cycle： 150
Control Type：Actuated－Coordinated
Maximum v／c Ratio： 4.41
Intersection Signal Delay： $565.3 \quad$ Intersection LOS：F
Intersection Capacity Utilization 148．8\％ICU Level of Service H
Analysis Period（min） 15
Splits and Phases：3：CR 519 Belvidere Rd \＆CR 622 Roxbury Station Rd／CR 622 Roxbury Hill Rd


Timings
3: CR 519 Belvidere Rd \& CR 621 Brainards Rd


Cycle Length: 90
Actuated Cycle Length: 90
Offset: $0(0 \%)$, Referenced to phase $2:$ NBTL and $6: S B T$, Start of Green
Natural Cycle: 150
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 3.55
Intersection Signal Delay: $507.3 \quad$ Intersection LOS: F
Intersection Capacity Utilization 137.4\% ICU Level of Service H
Analysis Period (min) 15
Splits and Phases: 3: CR 519 Belvidere Rd \& CR 621 Brainards Rd


Timings
3: CR 519 Belvidere Rd \& CR 621 Brainards Rd


Cycle Length: 90
Actuated Cycle Length: 90
Offset: $0(0 \%)$, Referenced to phase 2:NBTL and 6:SBT, Start of Green
Natural Cycle: 90
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 2.55
Intersection Signal Delay: 340.1 Intersection LOS: F
Intersection Capacity Utilization 137.6\% ICU Level of Service H
Analysis Period (min) 15
Splits and Phases: 3: CR 519 Belvidere Rd \& CR 621 Brainards Rd


Timings
2: CR 646 Belvidere Rd/CR 519 Belvidere Rd \& CR 519 Uniontown Rd

|  | $\cdots$ | $\nearrow$ | \% | 4 |
| :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NET | SWL | SWT |
| Lane Configurations | \% | 1 | ${ }^{7}$ | 4 |
| Traffic Volume (vph) | 2 | 1176 | 302 | 430 |
| Future Volume (vph) | 2 | 1176 | 302 | 430 |
| Turn Type | Prot | NA | Perm | NA |
| Protected Phases | 2 | 4 |  | 8 |
| Permitted Phases |  |  | 8 |  |
| Detector Phase | 2 | 4 | 8 | 8 |
| Switch Phase |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 22.5 | 22.5 | 22.5 | 22.5 |
| Total Split (s) | 35.0 | 55.0 | 55.0 | 55.0 |
| Total Split (\%) | 38.9\% | 61.1\% | 61.1\% | 61.1\% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 4.5 | 4.5 | 4.5 |
| Lead/Lag |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |
| Recall Mode | C-Max | None | None | None |
| Act Effct Green (s) | 30.5 | 50.5 | 50.5 | 50.5 |
| Actuated g/C Ratio | 0.34 | 0.56 | 0.56 | 0.56 |
| v/c Ratio | 1.50 | 1.30 | 4.20 | 0.47 |
| Control Delay | 258.1 | 164.1 | 1480.9 | 13.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 258.1 | 164.1 | 1480.9 | 13.7 |
| LOS | F | F | F | B |
| Approach Delay | 258.1 | 164.1 |  | 619.3 |
| Approach LOS | F | F |  | F |

Intersection Summary
Cycle Length: 90
Actuated Cycle Length: 90
Offset: $0(0 \%)$, Referenced to phase 2:NBL and 6:, Start of Green
Natural Cycle: 60
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 4.20
Intersection Signal Delay: $315.4 \quad$ Intersection LOS: F
Intersection Capacity Utilization 137.2\% ICU Level of Service H
Analysis Period (min) 15

Splits and Phases: 2: CR 646 Belvidere Rd/CR 519 Belvidere Rd \& CR 519 Uniontown Rd


[^58]WSP

Timings
2: CR 646 Belvidere Rd/CR 519 Belvidere Rd \& CR 519 Uniontown Rd

|  | $\cdots$ | $\nearrow$ | 7 | 4 |
| :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NET | SWL | SWT |
| Lane Configurations | Y | $\uparrow$ | \% | 4 |
| Traffic Volume (vph) | 12 | 358 | 702 | 1334 |
| Future Volume (vph) | 12 | 358 | 702 | 1334 |
| Turn Type | Prot | NA | Perm | NA |
| Protected Phases | 2 | 4 |  | 8 |
| Permitted Phases |  |  | 8 |  |
| Detector Phase | 2 | 4 | 8 | 8 |
| Switch Phase |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 22.5 | 22.5 | 22.5 | 22.5 |
| Total Split (s) | 23.0 | 67.0 | 67.0 | 67.0 |
| Total Split (\%) | 25.6\% | 74.4\% | 74.4\% | 74.4\% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 4.5 | 4.5 | 4.5 |
| Lead/Lag |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |
| Recall Mode | C-Max | None | None | None |
| Act Effct Green (s) | 18.5 | 62.5 | 62.5 | 62.5 |
| Actuated g/C Ratio | 0.21 | 0.69 | 0.69 | 0.69 |
| v/c Ratio | 0.63 | 0.32 | 1.25 | 1.18 |
| Control Delay | 9.3 | 6.2 | 145.0 | 107.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 9.3 | 6.2 | 145.0 | 107.3 |
| LOS | A | A | F | F |
| Approach Delay | 9.3 | 6.2 |  | 120.3 |
| Approach LOS | A | A |  | F |

## Intersection Summary

Cycle Length: 90
Actuated Cycle Length: 90
Offset: $0(0 \%)$, Referenced to phase 2:NBL and 6:, Start of Green
Natural Cycle: 150
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 1.25
Intersection Signal Delay: $91.0 \quad$ Intersection LOS: F
Intersection Capacity Utilization 99.4\% ICU Level of Service F
Analysis Period (min) 15
Splits and Phases: 2: CR 646 Belvidere Rd/CR 519 Belvidere Rd \& CR 519 Uniontown Rd


[^59]Synchro 10 Report
WSP

Timings
3: CR 519 Uniontown Rd \& NJ 57


Cycle Length: 90
Actuated Cycle Length: 90
Offset: 10.9 (12\%), Referenced to phase 4:EBTL and 8:WBTL, Start of Yellow
Natural Cycle: 90
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 0.95
Intersection Signal Delay: 28.7 Intersection LOS: C
Intersection Capacity Utilization 131.6\% ICU Level of Service H
Analysis Period (min) 15
Splits and Phases: 3: CR 519 Uniontown Rd \& NJ 57


Timings
3: CR 519 Uniontown Rd \& NJ 57


Cycle Length: 90
Actuated Cycle Length: 90
Offset: 10.9 (12\%), Referenced to phase 4:EBTL and 8:WBTL, Start of Yellow
Natural Cycle: 110
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 1.50
Intersection Signal Delay: $99.3 \quad$ Intersection LOS: F
Intersection Capacity Utilization 139.9\% ICU Level of Service H
Analysis Period (min) 15
Splits and Phases: 3: CR 519 Uniontown Rd \& NJ 57


Timings
4: CR 519 Uniontown Rd \& Strykers Rd


Cycle Length: 90
Actuated Cycle Length: 40.6
Natural Cycle: 60
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.70
Intersection LOS: A
Intersection Signal Delay: 9.7 ICU Level of Service B
Intersection Capacity Utilization 63.4\%
Analysis Period (min) 15
Splits and Phases: 4: CR 519 Uniontown Rd \& Strykers Rd


Timings
4: CR 519 Uniontown Rd \& Strykers Rd


Cycle Length: 90
Actuated Cycle Length: 90
Offset: $0(0 \%)$, Referenced to phase 2:NBTL and $6: S B T$, Start of Green
Natural Cycle: 130
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 1.09
Intersection Signal Delay: $38.6 \quad$ Intersection LOS: D
Intersection Capacity Utilization 92.1\% ICU Level of Service F
Analysis Period (min) 15
Splits and Phases: 4: CR 519 Uniontown Rd \& Strykers Rd


Timings
4: CO 632 \& I-78 WB ramp


Cycle Length: 90
Actuated Cycle Length: 89.6
Natural Cycle: 90
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.98
Intersection Signal Delay: 41.9
Intersection LOS: D
Intersection Capacity Utilization 86.4\% ICU Level of Service E
Analysis Period (min) 15

Splits and Phases: 4: CO 632 \& I-78 WB ramp


Timings
4: CO 632 \& I-78 WB ramp


Cycle Length: 90
Actuated Cycle Length: 34.7
Natural Cycle: 45
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.49
Intersection Signal Delay: 10.5
Intersection LOS: B
Intersection Capacity Utilization 39.2\% ICU Level of Service A
Analysis Period (min) 15
Splits and Phases: 4: CO 632 \& I-78 WB ramp


## APPENDIX E - CRASH TABLES

## US 22, Downtown Phillipsburg

|  |  | Statewide/ <br> Average (reference) <br> \% of <br> Total | CrashHotspot Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category |  |  | MorningPeak <br> Period(07:00 AM- 09:00AM) |  | EveningPeakPeriod(04:00 PM- 06:00PM) |  | All Day <br> (24Hours) |  |
|  |  |  | Number | $\begin{aligned} & \text { \% of } \\ & \text { Total } \end{aligned}$ | Number | $\begin{aligned} & \text { \% of } \\ & \text { Total } \end{aligned}$ | Number | $\begin{aligned} & \text { \% of } \\ & \text { Total } \end{aligned}$ |
| By Type |  |  |  |  |  |  |  |  |
| Same Direction - Rear End |  | 47.82\% | 23 | 19.66\% | 65 | 31.86\% | 272 | 22.52\% |
| Right Angle |  | 10.27\% | 22 | 18.80\% | 38 | 18.63\% | 211 | 17.47\% |
| Same Direction - Sideswipe |  | 19.11\% | 18 | 15.38\% | 31 | 15.20\% | 235 | 19.45\% |
| Fixed Object |  | 8.78\% | 22 | 18.80\% | 13 | 6.37\% | 142 | 11.75\% |
| Struck Parked Vehicle |  | 1.31\% | 18 | 15.38\% | 25 | 12.25\% | 192 | 15.89\% |
| Left Turn/U Turn |  | 2.29\% | 2 | 1.71\% | 3 | 1.47\% | 12 | 0.99\% |
| Opposite Direction (Head On |  | 1.61\% | 1 | 0.85\% | 3 | 1.47\% | 23 | 1.90\% |
| Overturned |  | 0.53\% | 1 | 0.85\% | 1 | 0.49\% | 4 | 0.33\% |
| Backing |  | 0.84\% | 4 | 3.42\% | 8 | 3.92\% | 45 | 3.73\% |
| Non-fixed Object |  | 0.88\% | 0 | 0.00\% | 0 | 0.00\% | 4 | 0.33\% |
| Animal |  | 4.13\% | 0 | 0.00\% | 1 | 0.49\% | 8 | 0.66\% |
| Pedestrian |  | 0.85\% | 3 | 2.56\% | 4 | 1.96\% | 19 | 1.57\% |
| Other |  | 1.58\% | 3 | 2.56\% | 12 | 5.88\% | 41 | 3.39\% |
|  | Total | 100.00\% | 117 | 100.00\% | 204 | 100.00\% | 1208 | 100.00\% |
| By Surface Condition |  |  |  |  |  |  |  |  |
| Dry |  | 79.65\% | 78 | 66.67\% | 166 | 81.37\% | 918 | 75.99\% |
| Wet |  | 17.89\% | 30 | 25.64\% | 33 | 16.18\% | 238 | 19.70\% |
| Other |  | 2.46\% | 9 | 7.69\% | 5 | 2.45\% | 52 | 4.30\% |
|  | Total | 100.00\% | 117 | 100.00\% | 204 | 100.00\% | 1208 | 100.00\% |
| By Lighting Conditions |  |  |  |  |  |  |  |  |
| Daylight |  | 70.21\% | 110 | 94.02\% | 157 | 76.96\% | 893 | 73.92\% |
| Dusk |  | 2.59\% | 1 | 0.85\% | 8 | 3.92\% | 23 | 1.90\% |
| Night |  | 25.32\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Other |  | 1.88\% | 6 | 5.13\% | 39 | 19.12\% | 292 | 24.17\% |
|  | Total | 100.00\% | 117 | 100.00\% | 204 | 100.00\% | 1208 | 100.00\% |
| By Severity |  |  |  |  |  |  |  |  |
| Property Damage Only |  | 74.26\% | 93 | 79.49\% | 161 | 78.92\% | 978 | 80.96\% |
| Complaint of Pain |  | 21.22\% | 18 | 15.38\% | 38 | 18.63\% | 186 | 15.40\% |
| Moderate Injury |  | 3.82\% | 5 | 4.27\% | 5 | 2.45\% | 40 | 3.31\% |
| Killed |  | 0.28\% | 1 | 0.85\% | 0 | 0.00\% | 1 | 0.08\% |
| Incapacitated |  | 0.42\% | 0 | 0.00\% | 0 | 0.00\% | 3 | 0.25\% |
|  | Total | 100.00\% | 117 | 100.00\% | 204 | 100.00\% | 1208 | 100.00\% |
| Vehicle Type |  |  |  |  |  |  |  |  |
| Autos |  | \#N/A | 107 | 91.45\% | 190 | 93.14\% | 1105 | 91.47\% |
| Heavy Vehicles |  | \#N/A | 10 | 8.55\% | 14 | 6.86\% | 103 | 8.53\% |
|  | Total | \#N/A | 117 | 100.00\% | 204 | 100.00\% | 1208 | 100.00\% |

Source: New Jersey Department of Transportation
Note: Statewide Average (2016-2018)

## US 46, NJ 182, CR 517, \& CR 604

|  |  |  | Crash Hotspot Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category |  | Statewide |  | g.Peak <br> riod $\begin{aligned} & M-09: 00 \\ & M) \\ & \hline \end{aligned}$ |  | ```gPeak iod M-09:00 M)``` | $\begin{array}{r}\text { Al } \\ \\ \hline 24\end{array}$ | Day <br> ours) |
|  |  | \% of Total | Number | \% of Total | Number | \% of Total | Number | \% of Total |
| By Type |  |  |  |  |  |  |  |  |
| Same Direction - Rear End |  | 47.82\% | 25 | 38.46\% | 32 | 31.37\% | 227 | 37.90\% |
| Right Angle |  | 10.27\% | 14 | 21.54\% | 23 | 22.55\% | 146 | 24.37\% |
| Same Direction - Sideswipe |  | 19.11\% | 8 | 12.31\% | 10 | 9.80\% | 50 | 8.35\% |
| Fixed Object |  | 8.78\% | 4 | 6.15\% | 2 | 1.96\% | 26 | 4.34\% |
| Struck Parked Vehicle |  | 1.31\% | 4 | 6.15\% | 9 | 8.82\% | 63 | 10.52\% |
| Left Turn/U Turn |  | 2.29\% | 2 | 3.08\% | 5 | 4.90\% | 18 | 3.01\% |
| Opposite Direction (Head On |  | 1.61\% | 1 | 1.54\% | 6 | 5.88\% | 13 | 2.17\% |
| Overturned |  | 0.53\% | 0 | 0.00\% | 0 | 0.00\% | 1 | 0.17\% |
| Backing |  | 0.84\% | 2 | 3.08\% | 4 | 3.92\% | 17 | 2.84\% |
| Non-fixed Object |  | 0.88\% | 0 | 0.00\% | 1 | 0.98\% | 2 | 0.33\% |
| Animal |  | 4.13\% | 0 | 0.00\% | 3 | 2.94\% | 7 | 1.17\% |
| Pedestrian |  | 0.85\% | 2 | 3.08\% | 1 | 0.98\% | 8 | 1.34\% |
| Other |  | 1.58\% | 3 | 4.62\% | 6 | 5.88\% | 21 | 3.51\% |
|  | Total | 100.00\% | 65 | 100.00\% | 102 | 100.00\% | 599 | 100.00\% |
| By Surface Condition |  |  |  |  |  |  |  |  |
| Dry |  | 79.65\% | 49 | 75.38\% | 82 | 80.39\% | 482 | 80.47\% |
| Wet |  | 17.89\% | 15 | 23.08\% | 16 | 15.69\% | 104 | 17.36\% |
| Other |  | 2.46\% | 1 | 1.54\% | 4 | 3.92\% | 13 | 2.17\% |
|  | Total | 100.00\% | 65 | 100.00\% | 102 | 100.00\% | 599 | 100.00\% |
| By Lighting Conditions |  |  |  |  |  |  |  |  |
| Daylight |  | 70.21\% | 61 | 93.85\% | 80 | 78.43\% | 468 | 78.13\% |
| Dusk |  | 2.59\% | 0 | 0.00\% | 6 | 5.88\% | 13 | 2.17\% |
| Night |  | 25.32\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Other |  | 1.88\% | 4 | 6.15\% | 16 | 15.69\% | 118 | 19.70\% |
|  | Total | 100.00\% | 65 | 100.00\% | 102 | 100.00\% | 599 | 100.00\% |
| By Severity |  |  |  |  |  |  |  |  |
| Property Damage Only |  | 74.26\% | 49 | 75.38\% | 83 | 81.37\% | 457 | 76.29\% |
| Complaint of Pain |  | 21.22\% | 14 | 21.54\% | 12 | 11.76\% | 114 | 19.03\% |
| Moderate Injury |  | 3.82\% | 2 | 3.08\% | 6 | 5.88\% | 25 | 4.17\% |
| Killed |  | 0.28\% | 0 | 0.00\% | 0 | 0.00\% | 1 | 0.17\% |
| Incapacitated |  | 0.42\% | 0 | 0.00\% | 1 | 0.98\% | 2 | 0.33\% |
|  | Total | 100.00\% | 65 | 100.00\% | 102 | 100.00\% | 599 | 100.00\% |
| Vehicle Type |  |  |  |  |  |  |  |  |
| Autos |  | \#N/A | 60 | 92.31\% | 99 | 97.06\% | 554 | 92.49\% |
| Heavy Vehicles |  | \#N/A | 5 | 7.69\% | 3 | 2.94\% | 45 | 7.51\% |
|  | Total | \#N/A | 65 | 100.00\% | 102 | 100.00\% | 599 | 100.00\% |

Source: New Jersey Department of Transportation
Note: Statewide Average (2016-2018)

## US @ CR 638 and @ CR 519



Source: New Jersey Department of Transportation
Note: Statewide Average (2016-2018)

## US 22 @ CR 519

| Category |  | Statewide Average | Crash Hotspot Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MorningPeak <br> Period(07:00 AM-09:00AM) | EveningPeakPeriod(04:00 PM-06:00PM) |  | All Day(24Hours) |  |
|  |  | $\begin{aligned} & \hline \% \text { of } \\ & \text { Total } \end{aligned}$ | Number | \% of Total | Number | $\begin{aligned} & \text { \% of } \\ & \text { Total } \end{aligned}$ | Number | $\begin{aligned} & \hline \% \text { of } \\ & \text { Total } \end{aligned}$ |
| By Type |  |  |  |  |  |  |  |  |
| Same Direction - Rear End |  |  | 47.82\% | 1 | 20.00\% | 4 | 25.00\% | 38 | 41.30\% |
| Right Angle |  | 10.27\% | 0 | 0.00\% | 2 | 12.50\% | 13 | 14.13\% |
| Same Direction - Sideswipe |  | 19.11\% | 3 | 60.00\% | 5 | 31.25\% | 21 | 22.83\% |
| Fixed Object |  | 8.78\% | 0 | 0.00\% | 0 | 0.00\% | 1 | 1.09\% |
| Struck Parked Vehicle |  | 1.31\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Left Turn/U Turn |  | 2.29\% | 0 | 0.00\% | 1 | 6.25\% | 1 | 1.09\% |
| Opposite Direction (Head On |  | 1.61\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Overturned |  | 0.53\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Backing |  | 0.84\% | 0 | 0.00\% | 0 | 0.00\% | 4 | 4.35\% |
| Non-fixed Object |  | 0.88\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Animal |  | 4.13\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Pedestrian |  | 0.85\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Other |  | 1.58\% | 1 | 20.00\% | 4 | 25.00\% | 14 | 15.22\% |
|  | Total | 100.00\% | 5 | 100.00\% | 16 | 100.00\% | 92 | 100.00\% |
| By Surface Condition |  |  |  |  |  |  |  |  |
| Dry |  | 79.65\% | 3 | 60.00\% | 13 | 81.25\% | 73 | 79.35\% |
| Wet |  | 17.89\% | 1 | 20.00\% | 3 | 18.75\% | 16 | 17.39\% |
| Other |  | 2.46\% | 1 | 20.00\% | 0 | 0.00\% | 3 | 3.26\% |
|  | Total | 100.00\% | 5 | 100.00\% | 16 | 100.00\% | 92 | 100.00\% |
| By Lighting Conditions |  |  |  |  |  |  |  |  |
| Daylight |  | 70.21\% | 4 | 80.00\% | 12 | 75.00\% | 72 | 78.26\% |
| Dusk |  | 2.59\% | 0 | 0.00\% | 1 | 6.25\% | 1 | 1.09\% |
| Night |  | 25.32\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Other |  | 1.88\% | 1 | 20.00\% | 3 | 18.75\% | 19 | 20.65\% |
|  | Total | 100.00\% | 5 | 100.00\% | 16 | 100.00\% | 92 | 100.00\% |
| By Severity |  |  |  |  |  |  |  |  |
| Property Damage Only |  | 74.26\% | 5 | 100.00\% | 15 | 93.75\% | 75 | 81.52\% |
| Complaint of Pain |  | 21.22\% | 0 | 0.00\% | 1 | 6.25\% | 14 | 15.22\% |
| Moderate Injury |  | 3.82\% | 0 | 0.00\% | 0 | 0.00\% | 3 | 3.26\% |
| Killed |  | 0.28\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Incapacitated |  | 0.42\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
|  | Total | 100.00\% | 5 | 100.00\% | 16 | 100.00\% | 92 | 100.00\% |
| Vehicle Type |  |  |  |  |  |  |  |  |
| Autos |  | - | 5 | 100.00\% | 14 | 87.50\% | 89 | 96.74\% |
| Heavy Vehicles |  |  | 0 | 0.00\% | 2 | 12.50\% | 3 | 3.26\% |
|  | Total |  | 5 | 100.00\% | 16 | 100.00\% | 92 | 100.00\% |

Source: New Jersey Department of Transportation Note: Statewide Average (2016-2018)

## US 46 @ CR 517

| Category |  | Statewide Average | Crash Hotspot Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Morming Peak <br> Period(07:00 AM- 09:00 <br> AM) | EveningPeakPeriod(04:00 PM- 06:00PM) |  | All Day <br> (24Hours) |  |
|  |  | $\begin{aligned} & \hline \% \text { of } \\ & \text { Total } \end{aligned}$ | Number | $\begin{aligned} & \hline \% \text { of } \\ & \text { Total } \end{aligned}$ | Number | \% of | Number | $\begin{aligned} & \hline \text { \% of } \\ & \text { Total } \end{aligned}$ |
| By Type |  |  |  |  |  |  |  |  |
| Same Direction - Rear End |  |  | 47.82\% | 5 | 55.56\% | 3 | 27.27\% | 23 | 37.70\% |
| Right Angle |  | 10.27\% | 0 | 0.00\% | 2 | 18.18\% | 10 | 16.39\% |
| Same Direction - Sideswipe |  | 19.11\% | 1 | 11.11\% | 4 | 36.36\% | 6 | 9.84\% |
| Fixed Object |  | 8.78\% | 1 | 11.11\% | 0 | 0.00\% | 9 | 14.75\% |
| Struck Parked Vehicle |  | 1.31\% | 0 | 0.00\% | 1 | 9.09\% | 4 | 6.56\% |
| Left Turn/U Turn |  | 2.29\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Opposite Direction (Head On |  | 1.61\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Overturned |  | 0.53\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Backing |  | 0.84\% | 0 | 0.00\% | 0 | 0.00\% | 2 | 3.28\% |
| Non-fixed Object |  | 0.88\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Animal |  | 4.13\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Pedestrian |  | 0.85\% | 0 | 0.00\% | 1 | 9.09\% | 2 | 3.28\% |
| Other |  | 1.58\% | 2 | 22.22\% | 0 | 0.00\% | 5 | 8.20\% |
|  | Total | 100.00\% | 9 | 100.00\% | 11 | 100.00\% | 61 | 100.00\% |
| By Surface Condition |  |  |  |  |  |  |  |  |
| Dry |  | 79.65\% | 6 | 66.67\% | 10 | 90.91\% | 49 | 80.33\% |
| Wet |  | 17.89\% | 3 | 33.33\% | 1 | 9.09\% | 12 | 19.67\% |
| Other |  | 2.46\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
|  | Total | 100.00\% | 9 | 100.00\% | 11 | 100.00\% | 61 | 100.00\% |
| By Lighting Conditions |  |  |  |  |  |  |  |  |
| Daylight |  | 70.21\% | 7 | 77.78\% | 11 | 100.00\% | 43 | 70.49\% |
| Dusk |  | 2.59\% | 0 | 0.00\% | 0 | 0.00\% | 3 | 4.92\% |
| Night |  | 25.32\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Other |  | 1.88\% | 2 | 22.22\% | 0 | 0.00\% | 15 | 24.59\% |
|  | Total | 100.00\% | 9 | 100.00\% | 11 | 100.00\% | 61 | 100.00\% |
| By Severity |  |  |  |  |  |  |  |  |
| Property Damage Only |  | 74.26\% | 7 | 77.78\% | 9 | 81.82\% | 47 | 77.05\% |
| Complaint of Pain |  | 21.22\% | 2 | 22.22\% | 1 | 9.09\% | 11 | 18.03\% |
| Moderate Injury |  | 3.82\% | 0 | 0.00\% | 1 | 9.09\% | 2 | 3.28\% |
| Killed |  | 0.28\% | 0 | 0.00\% | 0 | 0.00\% | 1 | 1.64\% |
| Incapacitated |  | 0.42\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
|  | Total | 100.00\% | 9 | 100.00\% | 11 | 100.00\% | 61 | 100.00\% |
| Vehicle Type |  |  |  |  |  |  |  |  |
| Autos |  | - | 9 | 100.00\% | 11 | 100.00\% | 57 | 93.44\% |
| Heavy Vehicles |  | - | 0 | 0.00\% | 0 | 0.00\% | 4 | 6.56\% |
|  | Total | - | 9 | 100.00\% | 11 | 100.00\% | 61 | 100.00\% |

Source: New Jersey Department of Transportation
Note: Statewide Average (2016-2018)

## I-80 @ CR 517

|  |  |  | CrashHotspot Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category |  | Statewide Average | MorningPeak <br> Period(07:00 AM-09:00AM) |  | EveningPeakPeriod(04:00 PM-06:00PM) |  | AllDay <br> (24Hours) |  |
|  |  | \% of Total | Number | \% of Total | Number | $\begin{aligned} & \hline \% \text { of } \\ & \text { Total } \end{aligned}$ | Number | $\begin{aligned} & \hline \% \text { of } \\ & \text { Total } \end{aligned}$ |
| By Type |  |  |  |  |  |  |  |  |
| Same Direction - Rear End |  | 47.82\% | 2 | 28.57\% | 4 | 57.14\% | 21 | 43.75\% |
| Right Angle |  | 10.27\% | 0 | 0.00\% | 2 | 28.57\% | 4 | 8.33\% |
| Same Direction - Sideswipe |  | 19.11\% | 1 | 14.29\% | 0 | 0.00\% | 3 | 6.25\% |
| Fixed Object |  | 8.78\% | 2 | 28.57\% | 0 | 0.00\% | 5 | 10.42\% |
| Struck Parked Vehicle |  | 1.31\% |  | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Left Turn/U Turn |  | 2.29\% | 0 | 0.00\% | 0 | 0.00\% | 4 | 8.33\% |
| Opposite Direction (Head On |  | 1.61\% | 0 | 0.00\% | 0 | 0.00\% | 2 | 4.17\% |
| Overturned |  | 0.53\% | 0 | 0.00\% | 1 | 14.29\% | 1 | 2.08\% |
| Backing |  | 0.84\% | 1 | 14.29\% | 0 | 0.00\% | 3 | 6.25\% |
| Non-fixed Object |  | 0.88\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Animal |  | 4.13\% | 1 | 14.29\% | 0 | 0.00\% | 3 | 6.25\% |
| Pedestrian |  | 0.85\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Other |  | 1.58\% | 0 | 0.00\% | 0 | 0.00\% | 2 | 4.17\% |
|  | Total | 100.00\% | 7 | 100.00\% | 7 | 100.00\% | 48 | 100.00\% |
| By Surface Condition |  |  |  |  |  |  |  |  |
| Dry |  | 79.65\% | 6 | 85.71\% | 5 | 71.43\% | 39 | 81.25\% |
| Wet |  | 17.89\% | 1 | 14.29\% | 2 | 28.57\% | 6 | 12.50\% |
| Other |  | 2.46\% | 0 | 0.00\% | 0 | 0.00\% | 3 | 6.25\% |
|  | Total | 100.00\% | 7 | 100.00\% | 7 | 100.00\% | 48 | 100.00\% |
| By Lighting Conditions |  |  |  |  |  |  |  |  |
| Daylight |  | 70.21\% | 7 | 100.00\% | 5 | 71.43\% | 36 | 75.00\% |
| Dusk |  | 2.59\% | 0 | 0.00\% | 2 | 28.57\% | 4 | 8.33\% |
| Night |  | 25.32\% | O | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Other |  | 1.88\% | 0 | 0.00\% | 0 | 0.00\% | 8 | 16.67\% |
|  | Total | 100.00\% | 7 | 100.00\% | 7 | 100.00\% | 48 | 100.00\% |
| By Severity |  |  |  |  |  |  |  |  |
| Property Damage Only |  | 74.26\% | 7 | 100.00\% | 5 | 71.43\% | 41 | 85.42\% |
| Complaint of Pain |  | 21.22\% | 0 | 0.00\% | 0 | 0.00\% | 4 | 8.33\% |
| Moderate Injury |  | 3.82\% | 0 | 0.00\% | 1 | 14.29\% | 2 | 4.17\% |
| Killed |  | 0.28\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Incapacitated |  | 0.42\% | 0 | 0.00\% | 1 | 14.29\% | 1 | 2.08\% |
|  | Total | 100.00\% | 7 | 100.00\% | 7 | 100.00\% | 48 | 100.00\% |
| Vehicle Type |  |  |  |  |  |  |  |  |
| Autos |  | - | 5 | 71.43\% | 7 | \#\#\#\#\#\#\# | 43 | 89.58\% |
| Heavy Vehicles |  | - | 2 | 28.57\% | 0 | 0.00\% | 5 | 10.42\% |
|  | Total |  | 7 | 100.00\% | 7 | 100.00\% | 48 | 100.00\% |

Source: New Jersey Department of Transportation
Note: Statewide Average (2016-2018)

## US 22 @ Morris Stand CR 646

|  |  |  | Crash Hotspot Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category |  | Statewide Average | MorningPeakPeriod(07:00 AM-09:00AM) |  | EveningPeakPeriod(04:00 PM- 06:00PM) |  | $\begin{aligned} & \text { All Day } \\ & \text { (24 Hours) } \end{aligned}$ |  |
|  |  | $\% \text { of }$ Total | Number | $\begin{aligned} & \hline \text { \% of } \\ & \text { Total } \end{aligned}$ | Number | $\begin{aligned} & \% \text { of } \\ & \text { Total } \end{aligned}$ | Number | $\begin{aligned} & \hline \% \text { of } \\ & \text { Total } \end{aligned}$ |
| By Type |  |  |  |  |  |  |  |  |
| Same Direction - Rear End |  | 47.82\% | 5 | 83.33\% | 4 | 80.00\% | 23 | 58.97\% |
| Right Angle |  | 10.27\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Same Direction - Sideswipe |  | 19.11\% | 0 | 0.00\% | 0 | 0.00\% | 5 | 12.82\% |
| Fixed Object |  | 8.78\% | 0 | 0.00\% | 1 | 20.00\% | 5 | 12.82\% |
| Struck Parked Vehicle |  | 1.31\% | 1 | 16.67\% | 0 | 0.00\% | 4 | 10.26\% |
| Left Turn/U Turn |  | 2.29\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Opposite Direction (Head On |  | 1.61\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Overturned |  | 0.53\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Backing |  | 0.84\% | 0 | 0.00\% | 0 | 0.00\% | 1 | 2.56\% |
| Non-fixed Object |  | 0.88\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Animal |  | 4.13\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Pedestrian |  | 0.85\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Other |  | 1.58\% | 0 | 0.00\% | 0 | 0.00\% | 1 | 2.56\% |
|  | Total | 100.00\% | 6 | 100.00\% | 5 | 100.00\% | 39 | 100.00\% |
| By Surface Condition |  |  |  |  |  |  |  |  |
| Dry |  | 79.65\% | 4 | 66.67\% | 4 | 80.00\% | 28 | 71.79\% |
| Wet |  | 17.89\% | 2 | 33.33\% | 1 | 20.00\% | 10 | 25.64\% |
| Other |  | 2.46\% | 0 | 0.00\% | 0 | 0.00\% | 1 | 2.56\% |
|  | Total | 100.00\% | 6 | 100.00\% | 5 | 100.00\% | 39 | 100.00\% |
| By Lighting Conditions |  |  |  |  |  |  |  |  |
| Daylight |  | 70.21\% | 6 | 100.00\% | 3 | 60.00\% | 30 | 76.92\% |
| Dusk |  | 2.59\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Night |  | 25.32\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Other |  | 1.88\% | 0 | 0.00\% | 2 | 40.00\% | 9 | 23.08\% |
|  | Total | 100.00\% | 6 | 100.00\% | 5 | 100.00\% | 39 | 100.00\% |
| By Severity |  |  |  |  |  |  |  |  |
| Property Damage Only |  | 74.26\% | 5 | 83.33\% | 2 | 40.00\% | 32 | 82.05\% |
| Complaint of Pain |  | 21.22\% | 0 | 0.00\% | 3 | 60.00\% | 4 | 10.26\% |
| Moderate Injury |  | 3.82\% | 1 | 16.67\% | 0 | 0.00\% | 2 | 5.13\% |
| Killed |  | 0.28\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Incapacitated |  | 0.42\% | 0 | 0.00\% | 0 | 0.00\% | 1 | 2.56\% |
|  | Total | 100.00\% | 6 | 100.00\% | 5 | 100.00\% | 39 | 100.00\% |
| Vehicle Type |  |  |  |  |  |  |  |  |
| Autos |  | - | 6 | 100.00\% | 5 | \#\#\#\#\#\#\# | 37 | 94.87\% |
| Heavy Vehicles |  | - | 0 | 0.00\% | 0 | 0.00\% | 2 | 5.13\% |
|  | Total | - | 6 | 100.00\% | 5 | 100.00\% | 39 | 100.00\% |

Source: New Jersey Department of Transportation
Note: Statewide Average (2016-2018)

## CR 630 @ CR 640

| Category |  | Statewide Average | Crash Hotspot Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | MormingPeak <br> Period(07:00 AM-09:00AM) |  | EveningPeakPeriod(04:00 PM-06:00PM) |  | All Day <br> (24Hours) |  |
|  |  | \% of <br> Total | Number | $\begin{aligned} & \text { \% of } \\ & \text { Total } \end{aligned}$ | Number | $\begin{aligned} & \text { \% of } \\ & \text { Total } \end{aligned}$ | Number | $\begin{aligned} & \hline \% \text { of } \\ & \text { Total } \end{aligned}$ |
| By Type |  |  |  |  |  |  |  |  |
| Same Direction - Rear End |  | 47.82\% | 6 | 85.71\% | 5 | 71.43\% | 23 | 58.97\% |
| Right Angle |  | 10.27\% | 0 | 0.00\% | 0 | 0.00\% | 2 | 5.13\% |
| Same Direction - Sideswipe |  | 19.11\% | 0 | 0.00\% | 1 | 14.29\% | 4 | 10.26\% |
| Fixed Object |  | 8.78\% | 1 | 14.29\% | 0 | 0.00\% | 5 | 12.82\% |
| Struck Parked Vehicle |  | 1.31\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Left Turn/U Turn |  | 2.29\% | 0 | 0.00\% | 0 | 0.00\% | 1 | 2.56\% |
| Opposite Direction (Head On |  | 1.61\% | 0 | 0.00\% | 1 | 14.29\% | 2 | 5.13\% |
| Overturned |  | 0.53\% | 0 | 0.00\% | 0 | 0.00\% | 1 | 2.56\% |
| Backing |  | 0.84\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Non-fixed Object |  | 0.88\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Animal |  | 4.13\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Pedestrian |  | 0.85\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Other |  | 1.58\% | 0 | 0.00\% | 0 | 0.00\% | 1 | 2.56\% |
|  | Total | 100.00\% | 7 | 100.00\% | 7 | 100.00\% | 39 | 100.00\% |
| By Surface Condition |  |  |  |  |  |  |  |  |
| Dry |  | 79.65\% | 5 | 71.43\% | 7 | 100.00\% | 29 | 74.36\% |
| Wet |  | 17.89\% | 2 | 28.57\% | 0 | 0.00\% | 10 | 25.64\% |
| Other |  | 2.46\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
|  | Total | 100.00\% | 7 | 100.00\% | 7 | 100.00\% | 39 | 100.00\% |
| By Lighting Conditions |  |  |  |  |  |  |  |  |
| Daylight |  | 70.21\% | 7 | 100.00\% | 4 | 57.14\% | 32 | 82.05\% |
| Dusk |  | 2.59\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Night |  | 25.32\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Other |  | 1.88\% | 0 | 0.00\% | 3 | 42.86\% | 7 | 17.95\% |
|  | Total | 100.00\% | 7 | 100.00\% | 7 | 100.00\% | 39 | 100.00\% |
| By Severity |  |  |  |  |  |  |  |  |
| Property Damage Only |  | 74.26\% | 4 | 57.14\% | 6 | 85.71\% | 25 | 64.10\% |
| Complaint of Pain |  | 21.22\% | 3 | 42.86\% | 0 | 0.00\% | 12 | 30.77\% |
| Moderate Injury |  | 3.82\% | 0 | 0.00\% | 1 | 14.29\% | 2 | 5.13\% |
| Killed |  | 0.28\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Incapacitated |  | 0.42\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
|  | Total | 100.00\% | 7 | 100.00\% | 7 | 100.00\% | 39 | 100.00\% |
| Vehicle Type |  |  |  |  |  |  |  |  |
| Autos |  | - | 7 | 100.00\% | 7 | 100.00\% | 38 | 97.44\% |
| Heavy Vehicles |  | - | 0 | 0.00\% | 0 | 0.00\% | 1 | 2.56\% |
|  | Total |  | 7 | 100.00\% | 7 | 100.00\% | 39 | 100.00\% |

Source: New Jersey Department of Transportation Note: Statewide Average (2016-2018)

CR 521@ CR 621

| Category |  | Statewide Average <br> \% of <br> Total | Crash Hotspot Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MormingPeakPeriod(07:00 AM- 09:00AM) | EveningPeakPeriod(04:00 PM-06:00PM) |  | All Day <br> (24 Hours) |  |
|  |  | Number | $\begin{aligned} & \hline \% \text { of } \\ & \text { Total } \end{aligned}$ | Number | $\begin{aligned} & \hline \% \text { of } \\ & \text { Total } \end{aligned}$ | Number | $\begin{aligned} & \hline \% \text { of } \\ & \text { Total } \end{aligned}$ |
| By Type |  |  |  |  |  |  |  |  |
| Same Direction - Rear End |  |  | 47.82\% | 1 | 33.33\% | 0 | 0.00\% | 7 | 25.93\% |
| Right Angle |  |  | 10.27\% | 1 | 33.33\% | 0 | 0.00\% | 2 | 7.41\% |
| Same Direction - Sideswipe |  | 19.11\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Fixed Object |  | 8.78\% | 1 | 33.33\% | 0 | 0.00\% | 3 | 11.11\% |
| Struck Parked Vehicle |  | 1.31\% | 0 | 0.00\% | 3 | 37.50\% | 7 | 25.93\% |
| Left Turn/U Turn |  | 2.29\% | 0 | 0.00\% | 1 | 12.50\% | 1 | 3.70\% |
| Opposite Direction (Head On |  | 1.61\% | 0 | 0.00\% | 1 | 12.50\% | 1 | 3.70\% |
| Overturned |  | 0.53\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Backing |  | 0.84\% | 0 | 0.00\% | 2 | 25.00\% | 5 | 18.52\% |
| Non-fixed Object |  | 0.88\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Animal |  | 4.13\% | 0 | 0.00\% | 1 | 12.50\% | 1 | 3.70\% |
| Pedestrian |  | 0.85\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Other |  | 1.58\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
|  | Total | 100.00\% | 3 | 100.00\% | 8 | 100.00\% | 27 | 100.00\% |
| By Surface Condition |  |  |  |  |  |  |  |  |
| Dry |  | 79.65\% | 2 | 66.67\% | 7 | 87.50\% | 24 | 88.89\% |
| Wet |  | 17.89\% | 0 | 0.00\% | 1 | 12.50\% | 2 | 7.41\% |
| Other |  | 2.46\% | 1 | 33.33\% | 0 | 0.00\% | 1 | 3.70\% |
|  | Total | 100.00\% | 3 | 100.00\% | 8 | 100.00\% | 27 | 100.00\% |
| By Lighting Conditions |  |  |  |  |  |  |  |  |
| Daylight |  | 70.21\% | 3 | 100.00\% | 4 | 50.00\% | 21 | 77.78\% |
| Dusk |  | 2.59\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Night |  | 25.32\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Other |  | 1.88\% | 0 | 0.00\% | 4 | 50.00\% | 6 | 22.22\% |
|  | Total | 100.00\% | 3 | 100.00\% | 8 | 100.00\% | 27 | 100.00\% |
| By Severity |  |  |  |  |  |  |  |  |
| Property Damage Only |  | 74.26\% | 3 | 100.00\% | 8 | 100.00\% | 26 | 96.30\% |
| Complaint of Pain |  | 21.22\% | 0 | 0.00\% | 0 | 0.00\% | 1 | 3.70\% |
| Moderate Injury |  | 3.82\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Killed |  | 0.28\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
| Incapacitated |  | 0.42\% | 0 | 0.00\% | 0 | 0.00\% | 0 | 0.00\% |
|  | Total | 100.00\% | 3 | 100.00\% | 8 | 100.00\% | 27 | 100.00\% |
| Vehicle Type |  |  |  |  |  |  |  |  |
| Autos |  | - | 1 | 33.33\% | 8 | 100.00\% | 25 | 92.59\% |
| Heavy Vehicles |  | - | 2 | 66.67\% | 0 | 0.00\% | 2 | 7.41\% |
|  | Total | - | 3 | 100.00\% | 8 | 100.00\% | 27 | 100.00\% |

Source: New Jersey Department of Transportation
Note: Statewide Average (2016-2018)


[^0]:    ${ }^{1}$ Logistics Trends and Specific Industries that Will Drive Warehouse and Distribution Growth and Demand for Space. National Association for Industrial and Office Parks, NAIOP, 2010.

[^1]:    Warren County Capacity Assess 12:00 pm 06/17/2020 2020 EXISTING - PM PEAK HOUR

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