ENGINEERING INVESTIGATION & ANALYSIS GEOTECHNICAL & STRUCTURAL ASSESSMENT REPORT

38 CLINTON ROAD FAIRFIELD, NEW JERSEY 08203

MATRIXNEWORLD

Engineering Progress

Prepared for:

State of New Jersey Department of Community Affairs PO Box 800 Trenton, NJ 08625-0800

Prepared by:

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Matrix No. 20-1052

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1.0 PROJECT BACKGROUND

The State of New Jersey Department of Community Affairs (DCA), Division of Disaster Recovery and Mitigation, anticipates receiving approval for grant funding through FEMA's Flood Mitigation Assistance (FMA) appropriation. This funding is provided through FMA to states and local communities to reduce or eliminate flood risk due to repetitive flood damage to buildings insured by the National Flood Insurance Program (NFIP). The DCA intends to use the funding for the State's Mitigation Assistance Program (MAP) to elevate residential properties located in a floodplain in the Township of Fairfield. The properties are to be elevated at least 3 feet above the base flood elevation (BFE). The DCA hosted a town hall meeting for homeowners in Fairfield, focused on homeowners with properties that experience Repetitive Losses or Severe Repetitive Losses.

In preparation of procuring a Design-Build firm to conduct the effort, the DCA has contracted Matrix New World Engineering, Land Surveying and Landscape Architecture, P.C. (Matrix) to conduct a geotechnical analysis, preliminary structural analysis, and elevation certificate for residences anticipated to be included in the program. It is understood that this document will serve as the basis for the development of a Request for Proposal (RFP) to procure Design-Build firms to do final structural design and perform the elevation of the properties.



2.0 PROJECT SCOPE

Matrix has completed a geotechnical and structural assessment and elevation certificate to evaluate the viability of elevating the residential building located at 38 Clinton Road in Fairfield, New Jersey (Site). Matrix provided geotechnical and structural engineering and land surveying services as a consultant to the DCA. The project location is shown on the attached Site Location Map (Figure 1).

The purpose of the engineering study was to compile comprehensive data regarding the existing building's foundations and overall structural composition and condition at the Site. The information obtained will be further utilized to determine the feasibility and proposed design of raising the existing residence 3 feet above the base flood elevation (BFE) as determined by FEMA. A team of Matrix engineers and surveyors performed the evaluation, consisting of a geotechnical soil inspection, test pits to reveal the existing building foundations, an interior inspection of the building's visible foundation walls and frame, and topographic surveying for the development of a flood elevation certificate. A total of 2 geotechnical borings (B-1 and B-2) were completed to a depth of 27 feet bgs (see Figure 2).

Matrix's geotechnical characterization of the property is based on an engineering evaluation of the subsurface conditions as indicated by the field exploration data and geotechnical laboratory test results on representative soil samples.



3.0 SITE LOCATION & PROJECT DESCRIPTION

The project site is located at 38 Clinton Road in Fairfield, New Jersey. The property consists of a two-story timber-framed colonial house with an approximately 840 square foot footprint. The building is situated atop concrete masonry unit (CMU) foundation walls with assumed cast-in-place concrete foundations. The substructure of the house is comprised of a basement level, as well as three crawl space areas in the front and rear of the building. The timber frame of residential structure is covered with a vinyl siding throughout its exterior. The property also contains a stone paver patio at ground level in the rear of the house.

To assist with the geotechnical and structural evaluation, geotechnical borings were advanced in areas around the residence to obtain information regarding the soil's structural properties. The 2 borings were located to provide the most useful information about the subsurface conditions. Refer to Figure 2 of this report for a map of the test pit and boring locations.



4.0 GEOLOGIC SETTING

According to the USDA Soil Survey of Essex County, the site is situated atop Pompton – Urban land. The subsurface composition is typically sand and loamy sands from 8 to 60 inches bgs.

According to the 2014 Bedrock Geologic Map of New Jersey, the Site is underlain by the Sedimentary and Bedded Volcanic Rocks Towaco Formation. Specifically, the subsurface consists of micaceous, reddish-brown sandstone, siltstone and silty mudstone in upward-fining sequences. The Bedrock Geologic Map is shown in Figure 3.

From the Surficial Geologic Map of Northern New Jersey, compiled by and edited by Byron D. Stone, Scott D. Stanford, and Ron W. White in 2002, the natural surface material (beyond fill) is suggested to be in the Pine Brook terrace deposit, which contains sand and gravel, moderately to poorly sorted. The Surficial Geology map is shown in Figure 4.

The documented site conditions presented above are consistent with the findings from the subsurface investigation, in which Sand was encountered followed by layers of Silt and Clay. Groundwater was encountered in the borings at approximately 6 feet bgs. Bedrock was not encountered during this subsurface program.



5.0 SUBSURFACE FIELD PROGRAM

The subsurface investigation was completed by generally accepted practices in the Geotechnical Engineering field and consisted of the advancement of 2 Standard Penetration Test (SPT) borings using mud rotary drilling methods. Matrix retained Boring Brothers, Inc., located in Egg Harbor Township, NJ, to complete the subsurface field program.

A Matrix Geotechnical Engineer provided full-time drilling oversight, soil logging, and sample collection. Matrix prepared the field test pit and boring logs, which included sample depths, SPT-N blow counts, soil recovery, and soil descriptions based on the Burmister Soil Classification System followed by the Unified Soil Classification System (USCS) letter symbol. Test pit and soil boring logs are provided in Appendix A. Classification tables and charts used to determine the soil attributes are included in Appendix B.

Upon the completion of the field program, representative samples were subjected to geotechnical laboratory analyses. Laboratory results aided in soil classification and assessing the relevant engineering properties of the stratigraphic layers which were used in developing the revised geotechnical parameters outlined herein. Geotechnical laboratory reports are included in Appendix C.

5.1 SPT Borings

On May 12, 2021, Boring Brothers advanced 2 geotechnical borings with a Mobile CME 55 track-mounted drill rig using mud rotary drilling techniques.

Split spoon (SS) samples were collected in accordance with *ASTM D-1586*, *Standard Method for Penetration Test and Split-Barrel Sampling of Soils*. A standard 2-inch outer diameter split spoon, two feet in length, was used to collect the soil samples. An automatic 140-pound hammer having a 30-inch drop was used to drive the split spoon sampler. As a part of boring observation, the SPT blow counts were recorded for the 0- to 6-inch interval, the 6- to 12-inch interval, the 12- to 18-inch interval and the 18- to 24-inch interval. The SPT N-values for design purposes are reported as the sum of the SPT N values observed for the above referenced 6- to 12-inch interval and the 12- to 18-inch interval that the split spoon sampler was driven.

The Matrix Geotechnical Engineer observed the split spoon samples and collected representative samples in sealed containers for further examination. All borings were continuously sampled to 12 feet bgs and at every subsequent 5-foot interval thereafter. The 2 borings were each advanced to a depth of 27 feet bgs.



The borings were backfilled with soil cuttings and bentonite hole plug (if necessary) upon completion of the borehole.

5.2 Laboratory Testing

In addition to the field investigation, a laboratory testing program was conducted to determine additional pertinent engineering characteristics of representative samples of on-site soils. The laboratory testing program was performed in general accordance with applicable ASTM standard test methods and included physical/textural testing of representative samples of various strata.

Upon review of the boring logs, Matrix selected representative samples for laboratory testing. Laboratory testing of selected samples was completed by TerraSense, LLC, located in Totowa, New Jersey. The following table presents a summary of the testing program.

The results of the laboratory testing program were utilized to assist in developing geotechnical design parameters and recommendations, and are provided in Appendix C.



Table 5.2-1: Laboratory Testing Program

Test	Testing Procedure	Quantity Performed	Sample Locations and Depth Intervals
Water Content	ASTM D2216	4	B-1: 10-12', 20-22' B-2: 4-6', 25-27'
Sieve Analysis	ASTM D422	2	B-1: 10-12' B-2: 4-6'
Atterberg Limits	ASTM D4318	1	B-2: 25-27'
Combined Sieve & Hydrometer	ASTM D422	1	B-1/2: 20-22'



6.0 SUBSURFACE CONDITIONS

The subsurface conditions beneath the site can be characterized by the following stratigraphy, proceeding from the surface materials downward, unless noted otherwise below. Classification tables and charts used to determine the soil attributes are included in Appendix B.

Surface Cover

The surface cover for boring B-1 and B-2 consisted of grass cover and topsoil, approximately 3-4 inches thick.

Stratum 1: Granular (SP-SM, SW-SM, SM, GM)

Beneath the surface cover in each boring, a soil layer was encountered consisting of brown coarse-to-fine grained Sand with varying amounts of Silt and coarse-to-fine Gravel. This granular layer extended from the bottom of the surface cover to approximately 18.5 feet below the ground surface (bgs) in B-1 and 15.83 feet bgs in B-2.

In boring B-2, the composition of this granular layer changed to predominantly coarse-to-fine Gravel with little Silt from approximately 13.5 to 15.83 feet bgs.

The SPT-N values in this layer ranged from 5 to 21 blows per foot (bpf), which is indicative of loose to medium-dense granular material. The SPT N-values for Stratum 1 are summarized in the tables below.

Table 6.0-1: Very Loose to Loose SPT N-Values for Stratum 1

Soil Boring	USCS Group Symbol	Depth Below	SPT	
Location	USCS Group Symbol	Ground Surface	N-Values	
B-1	SP-SM	0-4'	5-6	
D-1	SW-SM, SM	8-13.5'	9	
B-2	SP-SM	0-2'	7	

Table 6.0-2: Medium-Dense SPT N-Values for Stratum 1

Soil Boring Location	USCS Group Symbol	Depth Below Ground Surface	SPT N-Values
B-1	SW-SM	4-8'	16-21
D-1	SM	13.5-18.5	16
B-2	SP-SM, SW-SM, SM, GM	2-15.83'	12-19



Stratum 2: Clay (CH)

Beneath the granular material of Stratum 1, a soil layer was encountered consisting of highly plastic Silty Clay with trace amounts of fine Sand. This cohesive layer was encountered at approximately 18.5 feet bgs and 15.83 feet bgs in borings B-1 and B-2, respectively. Both borings were terminated within this Clay layer at 27 feet bgs.

The SPT-N values in this layer ranged from 5 to 10 blows per foot (bpf), which is indicative of medium-soft to stiff Clay. The SPT N-values for Stratum 2 are summarized in the tables below.

Table 6.0-3: Medium-Soft SPT N-Values for Stratum 2

Soil Boring Location	USCS Group Symbol	Depth Below Ground Surface	SPT N-Values
B-1	СН	18.5-27'	6-7
B-2	СН	15.83-18.5'	8
D-2	Сп	23.5-27'	5

Table 6.0-4: Stiff SPT N-Values for Stratum 2

Soil Boring Location	USCS Group Symbol	Depth Below Ground Surface	SPT N-Values
B-2	СН	18.5-23.5'	10

Groundwater

Groundwater levels could not be measured during drilling in either boring, due to the use of water and drilling mud to advance the borings. Based on soil saturation levels, the groundwater table lies approximately 6 feet bgs. Saturated soils were encountered in B-1 at 6 feet bgs at 11:23AM and in B-2 at 6 feet bgs at 12:16PM. It should be noted that the groundwater levels will vary with temperature, precipitation, and other climatic factors.



7.0 GEOTECHNICAL SUBSURFACE PARAMETERS

The geotechnical design parameters in this report are derived from the field program and are based on accepted geotechnical standards and practices. At the time of the geotechnical assessment, loading conditions and the final proposed grading plans were not available. Therefore, certain assumptions were made for the recommendations provided in this report.

Table 7.0-1 summarizes the recommended geotechnical design parameters for the various soil strata encountered at the Site. The values are based on review and interpretation of the subsurface field program and laboratory test data results.

Table 1806.2 of the 2018 International Building Code provides allowable coefficients of friction to be used in the evaluation of resistance to sliding.



Table 7.0-1: Geotechnical Design Parameters

	Unit	Friction Angle	Cohesive Strength,			Net Allowable	Lateral	
Stratum	Weight	(Φ)	C _u	Active	Passive	Foundation Pressure*	Bearing	
	(pcf)	(deg)	(psf)	(Ka)	(Kp)	(psf)	(psf/ft. bgs)	
Native Loose Granular Soil (SP, SP-SM, SM) [SPT N ≤ 10]	$\gamma = 105$ $\gamma' = 43$	30°	0	0.33	3.00	2,500	150	
Native Medium-Dense to Dense Granular Soil (SP, SP-SM, SM) [SPT N > 10]	$\gamma = 125$ $\gamma' = 63$	32°	0	0.31	3.26	4,000	200	
Native Clay (CL) Stiff [8 < SPT N <= 30]	$\gamma = 110$ $\gamma' = 48$	-	1,500	-	-	2,000*	100	
Native Clay (CL) Medium-Soft $[4 \leq SPT \ N \leq 8]$	$\gamma = 100$ $\gamma' = 38$	-	1,000	-	-	1,500*	75	

Notations: $\gamma = \text{moist unit weight}, \qquad \gamma' = \text{buoyant unit weight}, \text{ and } \qquad c_u = \text{average undrained shear strength}.$

- + Allowable foundation pressure is contingent upon either replacement of at least two feet of existing fill below the bottom of footing by a Controlled Fill or upon confirmation that the field density of the existing fill material down to four feet below the bottom of footing meets 95% of the maximum dry density of the existing fill material observed in Modified Proctor Tests.
- * These values are based on the 2018 International Building Code, New Jersey Edition, and adjusted for field conditions encountered. To increase the allowable foundation pressure above the values recommended in the table given above, further testing of soil will be required. In Cohesive soils, it should be noted that the shallow footing may fail under the settlement criteria before the footing pressure approaches the anticipated allowable bearing capacity. Allowable Foundation Pressure values assume the water table is below the influence depth of the foundation.
- Coefficient of earth pressure at rest may be computed using Jaky's equation, $K_0 = 1 \sin \phi'$.



8.0 STRUCTURAL INSPECTION

The following sections present the results of the structural inspection of the residential building at 38 Clinton Road in Fairfield, New Jersey. The conclusions presented herein are derived from Matrix's geotechnical and structural investigation of the existing soils and building foundations and framing configurations, along with pertinent survey data as compiled by Matrix's team of land surveyors.

Matrix conducted a subsurface investigation that included soil borings to obtain maximum pertinent information regarding the existing site conditions (refer to Section 6.0 of this report). Two geotechnical borings were conducted to gain information regarding the existing soils beneath the site.

In addition to the geotechnical investigation, Matrix also conducted a structural site inspection to observe the existing foundation walls and framing of the building. Matrix's structural engineer was granted access to the residence's cellar and crawl spaces to observe the building's foundation structure. Substructure composition was recorded, including beam/girder type, building dimensions, and spacing of structural components. Structural defects, if any, were also noted during the inspection and have been included within Section 8.3.

8.1 Existing Building Foundations

The building at 38 Clinton Road sits atop basement foundation walls as well as three separate crawl space areas. The timber frame is supported by 2x8 timber girders spanning the concrete and CMU (8x8x16 block) foundation walls.

The basement area, measuring approximately 24'-7" long x 21'-0" wide, encompasses the two-story portion of the building. The walls of the basement appear to be solid concrete, and measured 93" in height throughout the room's perimeter (measured from basement floor). The subfloor of the building's first-floor level consists of nominal 2x8 timber joists, spaced 16" on center, running north to south (side to side of building). These joists are attached to both sides of a timber girder using metal hangers. The girder, consisting of (3) connected nominal 2x8 timber members, spans the length of the basement (east to west) and is supported along its length by (3) 4" diameter steel posts. The longest clear span of the girder was measured at 7'-10" near the rear of the basement. The basement floor is approximately 8'-6" below the finished first-floor elevation.



An opening in the rear concrete basement wall leads to the southeast crawl space (5'5" long x 7'-6" wide). This area consists of CMU block (8x8x16) foundation walls approximately 40.5" high. The concrete floor of this crawl space is approximately 49" below the finished first-floor elevation. The first floor above the crawl space is supported by nominal 2x8 timber joists, space 16" on center (running east to west), sitting atop the CMU foundation walls.

A second crawl space was observed immediately north of the southeast crawl space (the two spaces share a common wall). This area, measuring 5'-5" long x 12'-10" wide, consists of the same type of CMU foundation walls as the southeast crawl space. These walls measured approximately 45" high, making the concrete floor of this space about 5" lower than that of the southeast crawl space. The timber nominal 2x8 floor joists in this crawl space run east to west, except in the southwest corner, where they run north to south. An 8"x8" square CMU block pedestal, located 4'-1" off the south wall, provides additional support for the floor joists and allows for the change in joist direction in the southwest corner.

A third crawl space was observed west of the basement and supports the front vestibule of the building. This space contains the same type of CMU walls as the other two crawl spaces. A CMU block pedestal is located in the middle of this space to support the subfloor above. The subfloor could not be observed at the time of the inspection due to the presence of insulated panels below the joists/girders.

Due to site constraints and the presence of underground utilities along the perimeter of the building at the Site, no test pits could be completed to reveal the existing foundation conditions of the building. Based on conventional foundation construction, Matrix utilized a 16" wide footing as a minimum value for analysis, but believes the actual footings for the building to likely range from 16" to 24" in width (typical footing size for residential homes). Prior to raising the house, Matrix recommends that the contractor confirm the foundation size and bearing adequacy with multiple test pits around the building perimeter.

8.2 Existing Equipment

All of the equipment and machinery observed at this property was located in the basement of the residential building. A washer/dryer machine was located on the basement floor along the rear (east) wall. An electrical panel and switchboard were on the walls in the southwest corner. In the southeast corner of the basement, a boiler and water well pressure tank system were observed. This entire corner of the basement was elevated approximately 22" above the main basement floor, and the boiler was raised an additional 14" using a pedestal of CMU block.



The southeast crawl space did not contain any machinery, but multiple PVC and metal pipes were observed running through the space.

8.3 Site Observations

The building at 38 Clinton Road appears to have been previously raised in the past. A set of concrete steps was observed in the northeast crawl space leading to an opening in the basement's rear wall. This apparent doorway, with a bottom approximately 31" below the top of the basement wall, has since been boarded up. Due to the presence of this opening, and the difference in wall type, it is also assumed that all three crawl spaces are additions to the original building structure.

The conditions surrounding the existing building (patios, landscaping, ground type, etc.) precluded the use of test pit excavations to reveal the existing building footings below the foundation walls. As such, no measurements could be made of the existing foundation dimensions. Any existing and proposed bearing estimates for the building were made on general assumptions regarding the building's construction methods.

The two rear crawl spaces had exposed insultation between the floor joists throughout the areas.

Timber landings for the front and rear entrances of the building were observed at the Site. Both consisted of timber joists and girders supported by timber posts embedded in concrete Sonotube footings.

8.4 Elevation Requirements

The FEMA 100-year flood elevation at 38 Clinton Road is El. +174.4 (NAVD88). As per the New Jersey Department of Community Affairs (DCA), and in accordance with the New Jersey Flood Hazard Area Control Act, the lowest floor of newly elevated buildings must be at least 3 feet above the base flood elevation. Therefore, the new first floor elevation must be at El. +177.4 or higher to meet the requirements set forth in the program.

The current first-floor elevation at the Site was measured at El. +174.66. To achieve the elevation requirements, the existing building would need to be raised approximately 2.8 feet. Matrix recommends raising the building at least 3.5 feet to allow for the creation of a ground-level beneath the newly raised building.



8.5 Recommendations for Building Elevation

Matrix recommends that the existing foundation system of the residential building at 38 Clinton Road be kept and extended to achieve the required design flood elevation. The existing foundation walls throughout the building's footprint are expected to provide sufficient support for the additional height of the newly raised building. Based on loading estimation and analysis for the existing building, Matrix estimates that the anticipated additional dead load of the required new courses of CMU, or additional height of poured concrete wall, would remain under an allowable bearing capacity of 2,500 psf for the assumed shallow concrete strip footings at the Site (foundation conditions for the building to be verified in field prior to construction).

In accordance with NFIP requirements, it is required that the existing basement and crawl space be filled in to match the lowest adjacent exterior grade following raising. The newly raised house will have approximately 7.7 feet of space beneath (down to existing finished grade), which is enough vertical height for a ground-floor level. This additional space beneath the raised building can be used for storage at the resident's discretion.

The most feasible method of elevation for the building consists of jacking up the entire residential structure from below using steel beams and jack posts. The building will then sit atop temporary cribbing while the existing CMU and concrete basement/crawl space walls are heightened with additional courses of masonry block units or additional poured concrete. Additional vertical reinforcement would need to be installed in ungrouted masonry cells to properly transfer loads through the new heightened wall to the existing wall, and horizontal ladder reinforcement should be installed at a minimum of every other course. For the concrete basement walls, additional rebar should be doweled into the existing walls to form a connection between the existing and new cast-in-place basement walls of the building. The existing steel posts or concrete block pedestals intermittently supporting the existing building's girders must be removed and replaced by new steel, concrete, or masonry block columns. These new columns will need to include a spread footing beneath to sufficiently support the building loads. Additionally, the front porch and deck are anticipated to require raising to match the current ingress/egress at heights of the main structure. This would require replacement or extension of the timber support posts.

Within the new foundation walls, permanent openings are required to allow floodwater to enter the ground level and equalize the hydrostatic pressure during a flood event. As per the 2018 International Residential Code, New Jersey Edition, the total net area of non-engineered openings must comprise at least 1 square



inch for every square foot of enclosed space within the building's ground floor. This equates to approximately 5.83 square feet of total flood openings in the building's new foundation walls. Additionally, a minimum of two openings must be provided for each enclosed area of the new ground floor. These openings must be located no higher than one foot above the adjacent finished exterior grade along the building perimeter. Matrix recommends the use of engineered openings in lieu of non-engineered openings to maximize efficiency and minimize the quantity of openings required.

Additionally, any service equipment, whether outside or in the basement/crawl spaces, such as air conditioning, heat pump compressors, gas meters, electric meters, and hot water heaters, must be elevated 3 feet above the BFE. For interior elements, this may include relocation to an upper floor and thus less usable living space. For this residence, the boiler, water well system, and electrical panel in the basement would require elevating 3 feet above the BFE.



9.0 CLOSURE

This report has been prepared to assist the State of New Jersey Department of Community Affairs with the structural and geotechnical evaluation of the residential building at 38 Clinton Road in Fairfield, New Jersey. The conclusions and recommendations provided within this report were prepared based on our understanding of the project and through the application of generally accepted engineering practices. No warranties, expressed or implied, are made. Matrix should be notified of any changes to the existing building foundation system or if subsurface conditions differing from those described herein are encountered, so the impact on the geotechnical and/or structural recommendations can be evaluated.



10.0 REPRESENTATIVE SITE PHOTOS

Structural Inspection Photos



Photo 1. 38 Clinton Road (Front of Building)



Photo 2. 38 Clinton Road (Rear of Building)



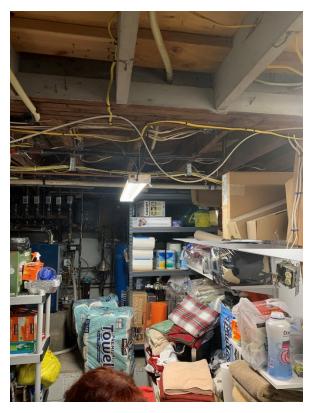


Photo 3. Floor Joists and Girder in Basement



Photo 4. Steel Post Support for Basement Girder (Typ.)



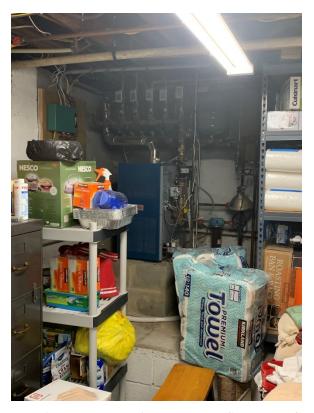


Photo 5. Boiler and Water in Basement (Southeast Corner)



Photo 6. Southeast Crawl Space



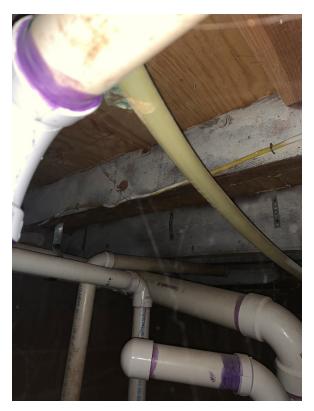


Photo 7. Floor Joist in Southeast Crawl Space



Photo 8. Northeast Crawl Space CMU Pedestal (Looking South)





Photo 9. Concrete Steps and Boarded Up Opening in West Wall of Northeast Crawl Space



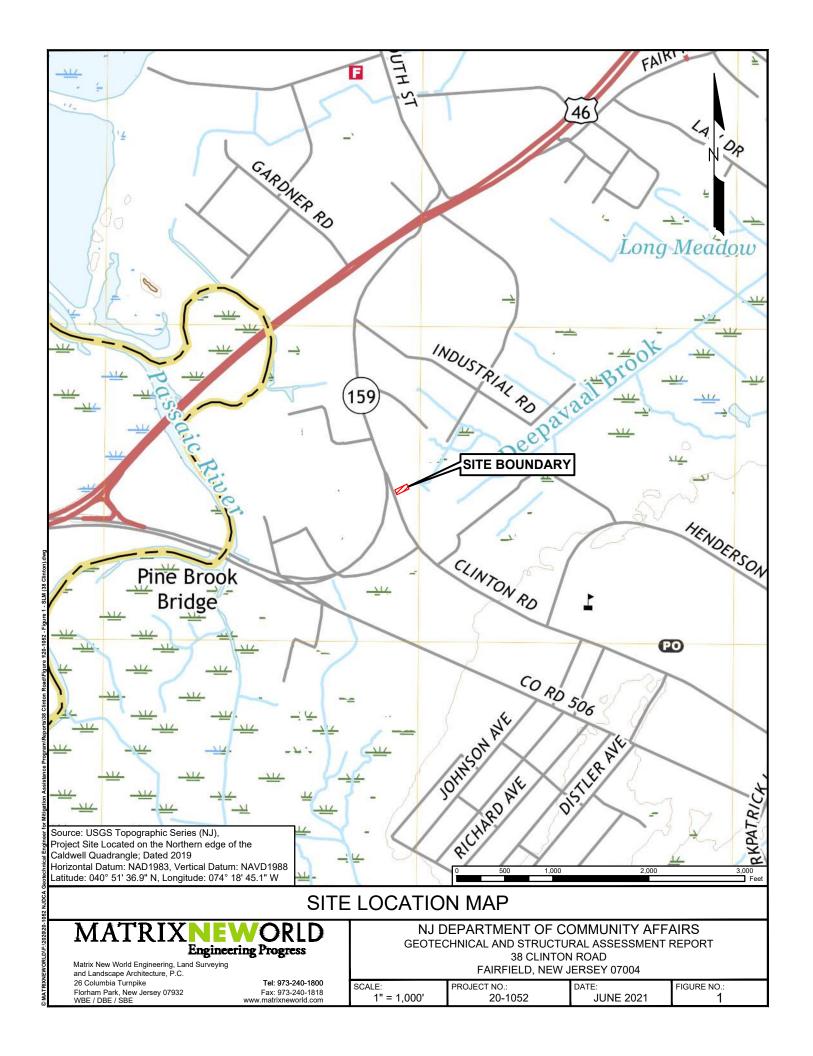
Photo 10. Front Crawl Space CMU Walls and Pedestal (Looking South)



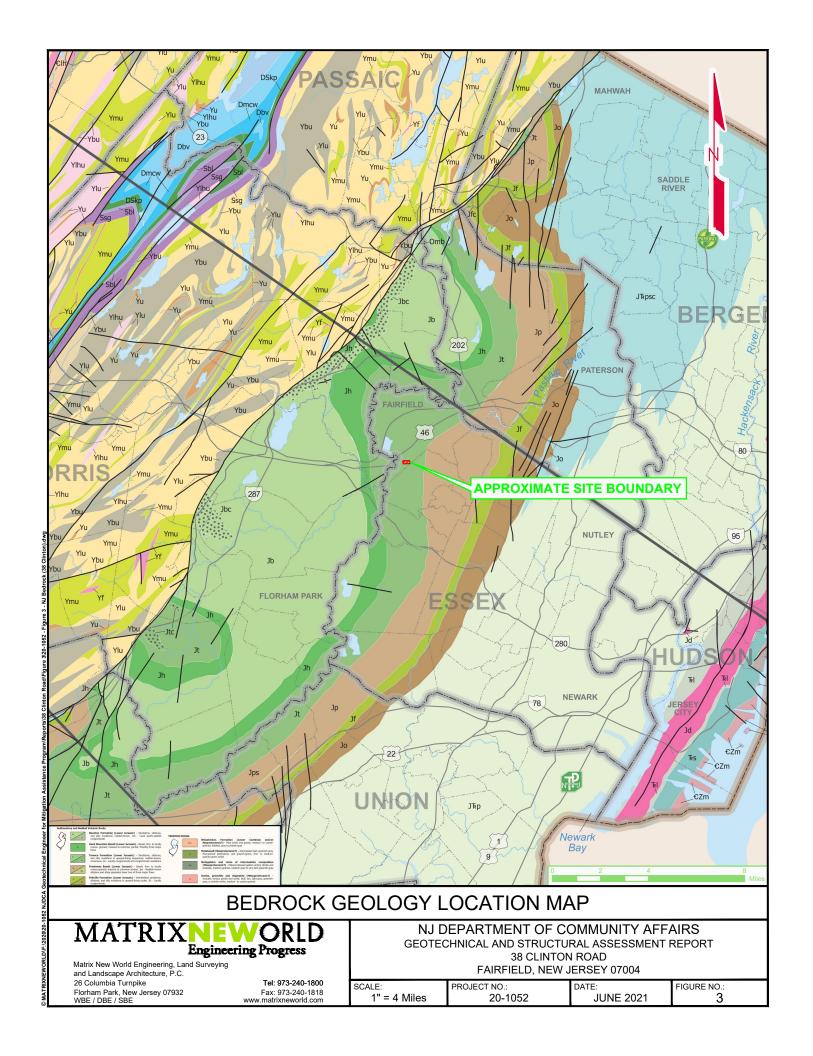


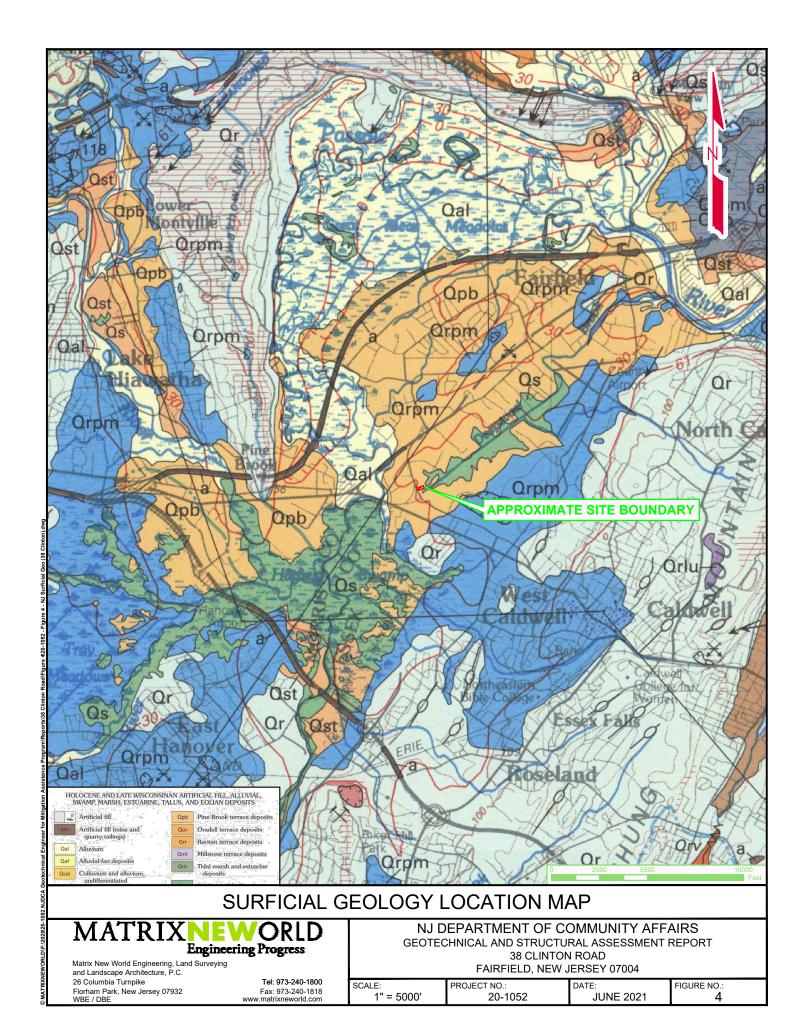
Photo 11. Front Entrance Stairs Frame and Supports











APPENDIX A SOIL BORING LOGS



NEWORLD NO GROUT 20-1052 BORING LOGS.GPJ MATRIX EGS.GDT 7/19/21

Engineering Progress

BORING LOG

												BORING NO.:			-1		
												SHEET	_1_	OF _	1		
PROJEC	T NO.:	20-1	1052	PRO	JECT: N	NJDC	A Ged	otechnical E	ngineer for l	Mitigation A	Assistance	Program DA	TE:	5/20/2	21		
					Fairfield, NJ BORING LOCATION: 38 Clinton Road, Steps							s					
DRILLIN	G EQUIPN	/ENT:		CME 5	55	ANG	GLE:		R.:					AVD88			
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5					(88%	6)											
<u>*</u>	4" Casing												• •				
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_					(100	%)											
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20																	
20		S-8	ss	20-22	4-3-4			S-8: Gray	Silty CLAY, tr	ace fine Sa	nd, wet (CH	1)		Siev			
_					(83%	6)		WC: 34.5%	6, G ravel: 0.0	1%, Sand: 1.	.7%, Fines:	98.3%, <2 μr	n: 67%	Hyd	rometer		
-																	
-																	
-																	
-																	
25		S-9	SS	25-27	3-3-3	1_3		S-0: Grav	Silty CLAY, w	et (CH)							
-		J-9	55	25-21	(100)			U-a. Glay	Only OLAT, W	70t (O11)							
_	[1															

Bottom of Borehole @ 27 ft.

BORING NO.: **B-1**



NEWORLD NO GROUT 20-1052 BORING LOGS.GPJ MATRIX EGS.GDT 7/19/21

Engineering Progress

BORING LOG

												BORING NO.:			B-2		
												SHEET	1	OF _	1		
PROJEC	T NO.:	20-1	1052	PRO	JECT: N	IJDO	A Geo	technical E	ngineer for l	Mitigation A	ssistance	Program DA	TE:	5/20/2	21		
	T LOCATI											Clinton Roa		ard			
DRILLIN	G EQUIPN	/ENT:		CME 5	55	ANG	GLE:	-90.0 DII	٦.: <u></u>	- ELEV	/.:	DATUN	M: NAVD88				
DRILLIN	G CONTR	ACTO	R: _	В	Boring Brothers			. DF	RILLER:	R. Dol	lar	INSPECTO	R:	D. Ali	а		
	CASIN	dG and	I HAMN	/IER				SAMPLER a	nd HAMMER			GROUNDWA	TER LEVE	S			
Туре			Weig		Drop	T	уре	I.D.	Weight	Drop	Date	Time	Depth		ng Depth		
Auto			140	bs	30"	Α	UTO		140 lbs	30"	5/20/21	12:16 pm	6.0		<u> </u>		
FJ Stee	el 4"						SS	1 3/8"									
Depth	CASING		(SAMPLE													
•			Π			/0"	흔현		Do	carintian	Of Matari	o.l		Labo	oratory		
Feet (Elev.)	Blows/ Foot	No.	Туре	Depth Feet	Blows (REC. [RQD	%)	Graphic Symbol		De	scription	Oi Materi	aı		T	ests		
		S-1	SS	0-2	2-4-3	_	11/ ₁ 1	√4" Topsoil						+			
_					(75%	6)			-Black mf* S	AND, little S	Silt, trace roo	ots, dry (SP-	SM)				
_																	
-		S-2	SS	2-4	3-5-7 (63%			S-2: Browr	mf* SAND,	little Silt, dry	(SP-SM)						
-					(00)	٠,											
		S-3	SS	4-6	7-9-10-11		-6 7-9-10				mf* SAND,					Siev	е
5					(75%	6)		WC: 17.8%	, Gravel: 0.6	5%, Sand: 76	6.6%, Fines	: 22.8%					
<u>*</u>	4" Casing							0.4.0						4			
		S-4	SS	6-8	8-7-7			S-4: Browr	cmf SAND,	trace Silt, tr	ace fine Gra	avel, wet (SW	/-SM)				
-					(100)	, • ,											
-		S-5	ss	8-10	7-5-6			S-5: Brown	cmf SAND,	little cf Grav	el, trace Sil	t, wet (SW-S	M)				
_					(1009	%)											
10			00	40.40	40.74			0.0.0	f OAND	E41 - 6 O-	1:441 - 0	:		4			
-		S-6	SS	10-12	10-7-9			S-6: Brown	cmf SAND,	little fine Gr	avel, little S	iit, wet (SM)					
-						,											
-																	
_																	
_																	
15							Pars										
-		S-7	SS	15-17	6-6-6				10"): Brown					_			
-					(007)	0)		S-7B (Botte	om 5"): Gray	Silty CLAY,	trace fine S	Sand, wet (Cl	1)				
-																	
_																	
-																	
20																	
-		S-8	SS	20-22	5-5-5	-5			as Above, w		-0/ =:	00.00/	0=0/	Siev	,		
					(83%	o)		WC: 34.5%	o, Gravel: 0.0	l%, Sand: 1.	/%, Fines:	98.3%, <2 µr	n: 6/%	Hydi	rometer		
_																	
-																	
-																	
_ - 25																	
		S-9	ss	25-27	3-2-3	-3		S-9: Gray	Silty CLAY, w	vet (CH)					rberg		
_					(1009	%)		WC: 39.3%	5, LL: 58, PL:	24, PI: 34				Limi	iS		
			1	r .	1		W W W A	1							,		

Bottom of Borehole @ 27 ft.

BORING NO.: **B-2**

LOG NOTATION

Sample Classifications

SS = Split Spoon

NR = No Recovery

NX = Rock Core

SH = Shelby Tube

REC = Soil Recovery

RQD = Rock Quality Designation

Sand Classifications

c = Coarse

m = Medium

f = Fine

* = Predominant Grain Size

Soil Properties

WC = Water Content

PL = Plastic Limit

LL = Liquid Limit

PI = Plasticity Index

OC = Organic Content

LOG GRAPHICAL LEGEND

	Asphalt
D & 8	Concrete
	Fill
	Topsoil
1.07.	Well graded Gravel (GW)
	Poorly graded Gravel (GP)
	Clayey Gravel (GC)
	Silty Gravel (GM)
	Well graded Gravel with Clay (GW-GC)
	Well graded Gravel with Silt (GW-GM)
	Poorly graded Gravel with Clay (GP-GC)
	Poorly graded Gravel with Silt (GP-GM)
3.44 K	Well graded Sand (SW)
	Poorly graded Sand (SP)
	Clayey Sand (SC)
	Silty Sand (SM)
	Well graded Sand with Clay (SW-SC)
	Well graded Sand with Silt (SW-SM)
	Poorly graded Sand with Clay (SP-SC)
	Poorly graded Sand with Silt (SP-SM)
	Lean Clay (CL)
	Silty Clay (CL-ML)
	Silt (ML)
	Organic Silt or Clay (Low Plasticity) (OL)
	Fat Clay (CH)
\mathbf{m}	Elastic Silt (MH)
****	Organic Silt or Clay (High Plasticity) (OH)
	Peat (PT)
1.11/2	Decomposed Bedrock
	Bedrock
VZAN	

APPENDIX B SOIL CLASSIFICATION TABLES

MA	AJOR DIVISION	vs.	GROUP SYMBOLS	TYPICAL NAMES	(EXCLUDING	ITIFICATION PRO PARTICLES LANGE IG FRACTIONS (WEIGHTS)	RGER THAN 3	INFORMATION REQUIRED FOR DESCRIBING SOILS	ι	.ABORATORY	CLASSIFICATION	CRITERIA						
1	2		3	4		5		6		7								
	urse fraction is sieve size. No. 4 sieve size.) Clean Gravels (Little or no fines)		GW	Well-graded gravels, gravel-sand mixture, little or no fines.	stra		stantial amounts	For undisturbed soils add information on stratification, degree of compactness, cementation, moisture condition, and drainage characteristics.	egas coffine C^*		$C_u = \frac{D_{60}}{D_{10}}$ Greater $C_e = \frac{(D_{30})^2}{D_{10} \times D_{60}}$ Be	than 4						
SIZE.	rels coarse fraction is a. 4 sieve size. he No. 4 sieve siz	Clean Or	GP	Poorly graded gravels or gravel-sand mixture, little or no fines.		one size or a range ate sizes missing.	e of sizes with	moistare condition, and trainage characteristics.		follow	Not meeting all gr requirements for C							
0. 200 steve	Gravels More than half of coarse fractio larger than No. 4 sieve size, as equivalent to the No. 4 sieve	th Fines amount of	GM	Silty gravels, gravel and silt mixtures.	Nonplastic fines (for identification	astic fines or fines with low plasticity entification procedures see ML below).				Depending or classified as symbols.	"A" line or P1 less than 4 b	Above "A" li vith P1 cetween 4 an						
ratione takin into or material is to get man 190, 200 stove size, it visible to the naked eye.	Gr (App		GC	Clayey gravels, gravel and clay mixtures.	Plastic fines (for identification	on procedures see	CL below).	Give typical name; indicate approximate percentages of sand and gravel, maximum size; angularity, surface condition, and hardness of the coarse grains; local or geologic name and other pertinent descriptive information; and symbol in parentheses.	et; indicate approximate percentages el, maximum size; angularity, a, and hardness of the coarse grains; name and other pertinent		Atterberg limits above "A" line with P1 greater than 7	are orderline cases requiring se of dual symbols.						
he naked eye.			sw	Well-graded sands, gravelly sands, little or no fines.	Wide range in g of all intermedia	rain size and subs ate particle sizes.	stantial amounts		as given under field identification	sand from gra size) coarse-g SW, SP, SM, SC. ne cases requir	$Cu = \frac{D_{60}}{D_{10}}$ Greater the $C_e = \frac{(D_{30})^2}{D_{10} \times D_{60}}$ Both	han 6 etween 1 ar						
ible to t	ction is size. n. the '	size. n. the '/,-in. Clean (Little or 1		Poorly graded sands or gravelly sands, little or no fines.		lominantly one size or a range of sizes with e intermediate sizes missing.				tvel and 30 sieve 3W, GF 3M, GC 3orderli	Not meeting all gr requirements for S							
smallest vis	Sands of coarse fractio No 4 sieve size classification. th	n Fines amount of	SM	Silty sands, sand-silt mixtures.	Nonplastic fines (for identification	or fines with low on procedures see	plasticity ML below).	Example: Silty sand, gravelly; about 20% hard, angular gravel particles '/ ₂ -in. maximum size; rounded and subangular sand grains, coarse to fine; about 15%	ns as given u	entage of grant than No. 21	"A" line or P1	Limits plotti n hatched ze vith P1 between 4 ar						
No. 200 sieve size is about the smallest visible to the naked eye	More than half of No (For visual cla	SM Silty sands, sand-silt mixtures. Nonplastic fines or fines with low plasticity (for identification procedures see ML below). SC Clayey sands, sand-clay mixtures. Plastic fines (for identification procedures see CL below).		CL below).	nonplastic fines with low dry strength; well compacted and moist in place; alluvial sand; (SM).	Optermine perconfraction smalle Less than 5% More than 12 5% to 12%	Atterberg 7 limits above "A" line with PI greater than	are corderline cases requiri use of dual symbols.										
The No. 200 sieve s					Identification Procedure on Fraction Smaller than No. 40 Sieve Size.		ion Smaller than		curve in identifying the fractions									
The No. 200					Dry Strength (Crushing Characteristics)	Dilatancy (Reaction to shaking)	Toughness (Consistency near PL)											
I	d Clays mit is less	00 u	ML	Inorganic silts and very fine sands, rock flour, silty or clayey fine sands or clayey silts with slight plasticity.	None to slight	Quick to slow	None	For undisturbed soils add information on structure, stratification, consistency in undisturbed and	Use grain-size	LIQUID LIMIT PLASTICITY CHART For laboratory classification		ART						
		Silts and Clays Liquid limit is le than 50		Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays.	Medium to high	None to very slow	Medium	remolded states, moisture and drainage conditions	ם		fine-grained soil							
	imit is		OL	Organic silts and organic silty clays of low plasticity.	Slight to medium	Slow	Slight	Give typical name; indicate degree and character of		80 60 Cm	aparing Solbs at Espeat Liquid Lim	nde						
	and Clays Liquid limit is greater than 50		МН	Inorganic silts, micaceous or diatomaceous fine sandy or silty soils, elastic silts.	Slight to medium	Slow to none	Slight to medium	Give typical name; indicate degree and character of plasticity; amount and maximum size of coarse grains; color in wet condition; odor, if any; local or geologic name and other pertinent descriptive information; and symbol in parentheses.		plasticity; amount and maximum size of coarse grains; color in wet condition; odor, if any; local or		plasticity; amount and maximum size of coarse grains; color in wet condition; odor, if any; local or geologic name and other pertinent descriptive		plasticity; amount and maximum size of coarse grains; color in wet condition; odor, if any; local or geologic name and other pertinent descriptive		Plasticity 65	gluces and Dry Strength Increase Increasing Placificity Index.	CH ALI
			СН	Inorganic clays of high plasticity, fat clays.	High to very high	None	High			20	CL OI	н						
1	Silts a		ОН	Organic clays of medium to high plasticity, organic silts.	Medium to high	None to very slow	Slight to medium	Example: Clayey silt, brown; slightly plastic; small percentage of fine sand; numerous vertical root holes; firm and dry in place; loess; (ML)		10 4 0 10	ML ML 20 30 40 50 60	70 80 90						
Hig	ghly Organic So	oils	Pt	Peat and other highly organic soils.	Readily identific frequently by fil	ed by color, odor, prous texture	spongy feel and											

All sieve sizes on this chart are U.S. standard.
 Adopted by Corps of Engineers and Bureau of Reclamation, January 1952.

BURMISTER SOIL IDENTIFICATION METHOD

BURMISTER SOIL IDENTIFICATION METHOD

1. SOIL MATERIAL Composition, Gradation, and Plasticity Characteristics

a) Soil Components and Soil Fractions

Sieve	3"	1"	3/8"	No. 10)]	No. 30	No	. 60	No. 200	
				2 mm					0.076 mm	0.02 mm
Granular		GRAV	EL			SAND			SI	LT
Component Fractions	coarse	mediu	m f	ine co	arse	medi	ım	fine	coarse	fine
Clay Soil									CLAY	-SOIL
Components									Defined and	Named on a
									Plastici	ty Basis

Identifying Terms for Granular Soils Composition and Proportion Terms for Components

Component		Proportion	Defining Range
		<u>Terms</u>	of Percentages
Principal Compone (all Uppercase)	nts- GRAVEL, SAND, SILT		50% or more
Minor Components	s- Gravel	and	35 to 50%
	Sand	some	20 to 35%
	Silt	little	10 to 20%
		trace	1 to 10%
Gradation Terms fo	or Granular Soils	ORGA	ANIC SOILS
coarse to fine	all fractions more than 10%	Plastic	city Basis, as
coarse to medium	fine less than 10%		
medium to fine	coarse less than 10%	Organi	c SILT, H. PI
medium	coarse and fine less than 10%		
fine	coarse and medium less than 10%	Organi	ic SILT, L. PI
PLUS or MINUS sig	gns used to indicate upper or lower limits.		

Identifying Terms for CLAY SOILS. Plasticity Basis for Combined Silt and Clay Components, Expressing the Relative Dominance of Clay

Overall Plasticity	Plasticity Index	Principal Component	Minor Component
Non-Plastic	0	SILT	Silt
Slight	1 to 5	Clayey SILT	Clayey Silt
Low	5 to 10	SILT & CLAY	Silt & Clay
Medium	10 to 20	CLAY & SILT	Clay & Silt
High	20 to 40	Silty CLAY	
Very High	more than 40	CLAY	

Example: Soil 60% coarse to fine Sand, 25% medium to fine Gravel, 15% Clayey Silt and color-brown.

Identification: Br. coarse to fine SAND, some medium to fine Gravel, little Clayey Silt.

References: 1) D. M. Burmister, "Principles and Techniques of Soil Identification" 29th Highway Research Board Proceedings, 1949.

 "Identification and Classification of Soils – An appraisal and Statement of Principles", ASTM Special Technical Publication No. 113, 1951.

Field Classification of Soil Using the USCS

Apparent Density of Coarse-Grained Soils

SPT N-Value (corrected)	Apparent Density
0 - 4	Very loose
5 - 10	Loose
11 - 30	Medium Dense
31 - 50	Dense
> 50	Very Dense

Consistency of Fine-Grained Soils

SPT N-Value (uncorrected)	Consistency	Compressive Strength (ksf)	Results of Manual Manipulation
< 2	Very Soft	< 0.5	Specimen (height = twice the diameter) sags under its own weight; extrudes between fingers when squeezed
3 - 4	Soft	> 0.5 - 1.0	Speciment can be pinched in to between the thumb and forefinger; remolded by light finger pressure
5 - 8	Medium stiff	> 1.0 - 2.0	Can be imprinted easily with fingers; remolded by strong finger pressure
9 - 15	Stiff	> 2.0 - 4.0	Can be imprinted with considerable pressure from fingers or indented by thumbnail
16 - 30	Very stiff	> 4.0 - 8.0	Can be barely imprinted by pressure from the fingers or indented by thumbnail
> 30	Hard	> 8.0	Cannot be imprinted by fingers or difficult to indent by thumbnail

APPENDIX C GEOTECHNICAL LABORATORY TESTING RESULTS

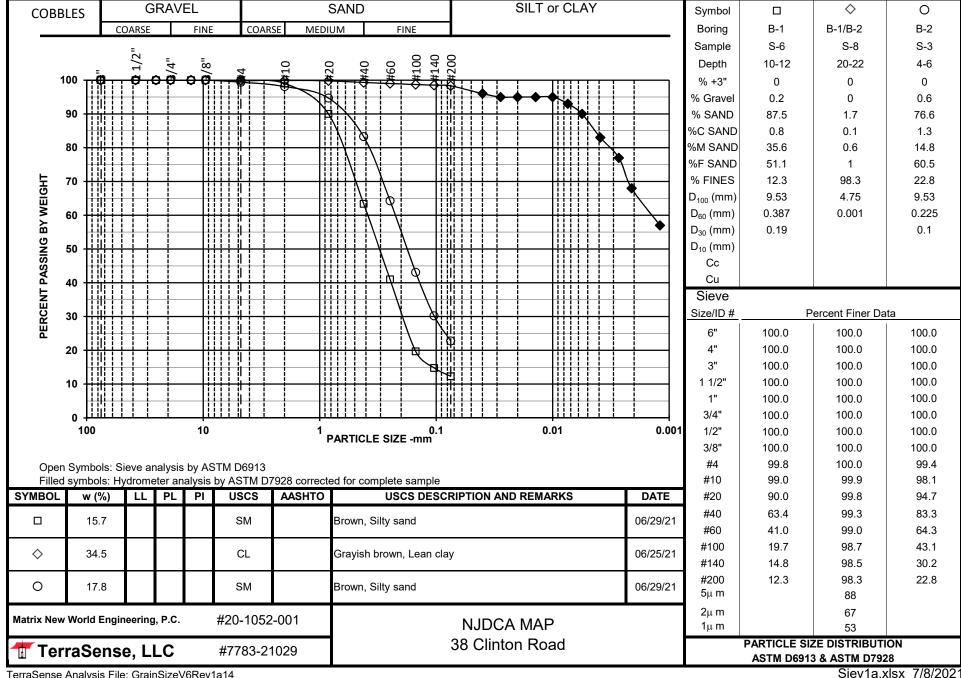
Matrix New World Engineering, P.C. #20-1052-001 NJDCA MAP - 38 Clinton Road LABORATORY TESTING DATA SUMMARY

BORING	SAMPLE	DEPTH		IDENTIFICATION TESTS						
			WATER	LIQUID	PLASTIC	PLAS.	USCS	SIEVE	HYDROMETER	
NO.	NO.		CONTENT	LIMIT	LIMIT	INDEX	SYMB.	MINUS	% MINUS	
							(1)	NO. 200	2 μm	
		(ft)	(%)	(-)	(-)	(-)		(%)	(%)	
B-1	S-6	10-12	15.7				SM	12.3		
B-1/B-2	S-8	20-22	34.5				CL	98.3	67	
B-2	S-3	4-6	17.8				SM	22.8		
B-2	S-9	25-27	39.3	58	24	34	CH			

Note: (1) USCS symbol based on visual observation and Sieve and Atterberg limits reported.

Prepared by: NG Reviewed by: CMJ Date: 7/8/2021

TerraSense, LLC 45H Commerce Way Totowa, NJ 07512 Project No.: 7783-21029 File: Indx1.xlsx Page 1 of 1



APPENDIX D FEMA NFIP ELEVATION CERTIFICATE

U.S. DEPARTMENT OF HOMELAND SECURITY Federal Emergency Management Agency National Flood Insurance Program

OMB No. 1660-0008 Expiration Date: November 30, 2022

ELEVATION CERTIFICATEImportant: Follow the instructions on pages 1–9.

Copy all pages of this Elevation Certificate and all attachments for (1) community official, (2) insurance agent/company, and (3) building owner.

SEC	FOR INSUR	ANCE COMPANY USE									
A1. Building Owner's Name Policy Number:											
A2. Building Street Address (including Apt., Unit, Suite, and/or Bldg. No.) or P.O. Route and Company NAIC Number: 38 Clinton Road											
City State ZIP Code											
Town of Fairfield New Jersey 07004-2910											
A3. Property Description (Lot and Block Numbers, Tax Parcel Number, Legal Description, etc.) Block 601, Lot 32											
A4. Building Use (e.g., Residential, Non-Residential, Addition, Accessory, etc.) Residential											
A5. Latitude/Longitude: Lat. N	40°51'37"	Long. W	/74°18'46"	Horizontal	Datum: NAD 1	927 🕱 NAD 1983					
A6. Attach at least 2 photograp	hs of the building if the	e Certific	ate is being u	sed to obtain floor	d insurance.						
A7. Building Diagram Number	2A										
A8. For a building with a crawls	space or enclosure(s):										
a) Square footage of crawl	space or enclosure(s)			706.00 sq ft							
b) Number of permanent flo	ood openings in the cra	awlspace	e or enclosure	e(s) within 1.0 foot	above adjacent gra	de <u>0</u>					
c) Total net area of flood op	penings in A8.b		0.00 sq in	I							
d) Engineered flood openir	ngs? 🗌 Yes 🕱 N	10									
A9. For a building with an attach	ned garage:										
a) Square footage of attach	ned garage		N/A sq ft								
b) Number of permanent flo	ood openings in the att	tached g	arage within	1.0 foot above adja	acent grade						
c) Total net area of flood or	penings in A9.b		sq	in							
d) Engineered flood openin	igs?	10									
SE	ECTION B – FLOOD I	INSURA	NCE RATE	MAP (FIRM) INF	ORMATION						
B1. NFIP Community Name & 0		1100	B2. County	. ,	011	B3. State					
Fairfield, Township of	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		Essex			New Jersey					
B4. Map/Panel B5. Suffix Number	B6. FIRM Index Date	Effe	LRM Panel ective/ vised Date	B8. Flood Zone(s)	B9. Base Flood El (Zone AO, use	levation(s) e Base Flood Depth)					
**34013C0077 G	04-03-2020	04-03-2		AE	174 (NAVD88)						
R10 Indicate the source of the	Base Flood Flevation	(BFF) d:	ata or hase flu	nod denth entered	in Item B9:						
B10. Indicate the source of the Base Flood Elevation (BFE) data or base flood depth entered in Item B9: FIS Profile FIRM Community Determined Other/Source:											
B11. Indicate elevation datum used for BFE in Item B9: NGVD 1929 X NAVD 1988 Other/Source:											
B12. Is the building located in a Coastal Barrier Resources System (CBRS) area or Otherwise Protected Area (OPA)? \(\subseteq \) Yes \(\subseteq \) No											
Designation Date: CBRS OPA											
			_								

ELEVATION CERTIFICATE

OMB No. 1660-0008 Expiration Date: November 30, 2022

IMPORTANT: In these spaces, copy the corresponding information from Section A.	FOR INSURANCE COMPANY USE								
Building Street Address (including Apt., Unit, Suite, and/or Bldg. No.) or P.O. Route and Box No. 38 Clinton Road	Policy Number:								
City State ZIP Code Town of Fairfield New Jersey 07004-2910	Company NAIC Number								
SECTION C – BUILDING ELEVATION INFORMATION (SURVEY	REQUIRED)								
C1. Building elevations are based on: Construction Drawings* Building Under Const*A new Elevation Certificate will be required when construction of the building is complete. C2. Elevations – Zones A1–A30, AE, AH, A (with BFE), VE, V1–V30, V (with BFE), AR, AR/A, A Complete Items C2.a–h below according to the building diagram specified in Item A7. In Pur Benchmark Utilized: CORS Network NGS Monuments Vertical Datum: NAVD 1988 Indicate elevation datum used for the elevations in items a) through h) below. NGVD 1929 NAVD 1988 Other/Source: Datum used for building elevations must be the same as that used for the BFE. a) Top of bottom floor (including basement, crawlspace, or enclosure floor) b) Top of the next higher floor c) Bottom of the lowest horizontal structural member (V Zones only) d) Attached garage (top of slab) e) Lowest elevation of machinery or equipment servicing the building (Describe type of equipment and location in Comments) f) Lowest adjacent (finished) grade next to building (HAG)	struction*								
h) Lowest adjacent grade at lowest elevation of deck or stairs, including structural support	170.1 X feet meters								
SECTION D – SURVEYOR, ENGINEER, OR ARCHITECT CERTIFICATION									
This certification is to be signed and sealed by a land surveyor, engineer, or architect authorized I certify that the information on this Certificate represents my best efforts to interpret the data avastatement may be punishable by fine or imprisonment under 18 U.S. Code, Section 1001. Were latitude and longitude in Section A provided by a licensed land surveyor? X Yes	ailable. I understand that any false								
Certifier's Name Erank J. Barlowski License Number 24GS03973500									
Title Professional Land Surveyor Company Name Matrix New World Engineering, Land Surveying and Architecture, P.C. Address 442 State Route 35, Second Floor City State ZIP Code Eatontown New Jersey 07724 Signature Date Telephone Copy all pages of this Elevation Certificate and all attachments for (1) community official, (2) insurance Comments (including type of equipment and location, per C2(e), if applicable) **Portions of the property is shown on two Flood Insurance Rate Maps (34013C0077G & 34013C C2(b) Top of the next higher floor, Elev.=170.6' (NAVD88), being within the basement area (split C2(e) Water storage tank was found in the basement area, Base of tank Elev=168.0' (NAVD88).	008G).								

ELEVATION CERTIFICATE

OMB No. 1660-0008 Expiration Date: November 30, 2022

IMPORTAN	T: In these spaces, copy the correspo	ending information fror	n Section A.	FOR INSURANCE COMPANY USE
Building Str 38 Clinton	reet Address (including Apt., Unit, Suite, a Road	and/or Bldg. No.) or P.C	. Route and Box No.	Policy Number:
City Town of Fa	irfield	State New Jersey	ZIP Code 07004-2910	Company NAIC Number
	SECTION E – BUILDING FOR ZO	ELEVATION INFORM ONE AO AND ZONE A		REQUIRED)
	AO and A (without BFE), complete Items ections A, B,and C. For Items E1–E4, us			
the hig	e elevation information for the following a hest adjacent grade (HAG) and the lowe o of bottom floor (including basement,	and check the appropriatest adjacent grade (LAG)	te boxes to show whethe	r the elevation is above or below
cra	awlspace, or enclosure) is of bottom floor (including basement,		feet meter	s above or below the HAG.
cra	wlspace, or enclosure) is with permanent floo	d apopings provided in	feet meter	
the ne	xt higher floor (elevation C2.b in igrams) of the building is	ua openings provided in s	feet meter	
E3. Attach	ed garage (top of slab) is		feet	s above or below the HAG.
E4. Top of servici	platform of machinery and/or equipment ng the building is	·	feet meter	s 🗌 above or 🗌 below the HAG.
	AO only: If no flood depth number is avail lain management ordinance? Yes			cordance with the community's certify this information in Section G.
	SECTION F - PROPERTY C	WNER (OR OWNER'S	REPRESENTATIVE) CE	ERTIFICATION
The proper community	ty owner or owner's authorized represent -issued BFE) or Zone AO must sign here	tative who completes Se . The statements in Sec	ections A, B, and E for Zo tions A, B, and E are cor	ne A (without a FEMA-issued or rect to the best of my knowledge.
Property O	wner or Owner's Authorized Representat	ive's Name		
Address		City	Sta	ate ZIP Code
Signature		Date	Te	lephone
Comments				
				Check here if attachments.

ELEVATION CERTIFICATE

OMB No. 1660-0008 Expiration Date: November 30, 2022

IMPORTANT: In these spaces, copy the corre		FOR INSURANCE COMPANY USE										
Building Street Address (including Apt., Unit, St 38 Clinton Road	No.	Policy Number:										
City Town of Fairfield	State New Jersey	ZIP Code 07004-2910		Company NAIC Number								
,												
	SECTION G - COMMUNITY INFORMATION (OPTIONAL)											
The local official who is authorized by law or ordinance to administer the community's floodplain management ordinance can complete Sections A, B, C (or E), and G of this Elevation Certificate. Complete the applicable item(s) and sign below. Check the measurement used in Items G8–G10. In Puerto Rico only, enter meters.												
The information in Section C was taken from other documentation that has been signed and sealed by a licensed surveyor, engineer, or architect who is authorized by law to certify elevation information. (Indicate the source and date of the elevation data in the Comments area below.)												
G2. A community official completed Section or Zone AO.	on E for a building	located in Zone A (without	t a FEMA	t-issued or community-issued BFE)								
G3. The following information (Items G4–	G10) is provided fo	or community floodplain ma	anageme	ent purposes.								
G4. Permit Number	G5. Date Permit	Issued		ate Certificate of ompliance/Occupancy Issued								
G7. This permit has been issued for:	New Construction	n 🗌 Substantial Improven	nent									
G8. Elevation of as-built lowest floor (including of the building:	g basement)	_	feet	meters Datum								
G9. BFE or (in Zone AO) depth of flooding at t	he building site: _		feet	meters Datum								
G10. Community's design flood elevation:			feet	meters Datum								
Local Official's Name		Title										
Community Name		Telephone										
Signature		Date										
Comments (including type of equipment and loc	cation, per C2(e), if	applicable)										
				Check here if attachments.								

BUILDING PHOTOGRAPHS

ELEVATION CERTIFICATE

See Instructions for Item A6.

OMB No. 1660-0008

Expiration Date: November 30, 2022

IMPORTANT: In these spaces, cop	FOR INSURANCE COMPANY USE		
Building Street Address (including A 38 Clinton Road	Policy Number:		
City	State	ZIP Code	Company NAIC Number
Town of Fairfield	New Jersey	07004-2910	

If using the Elevation Certificate to obtain NFIP flood insurance, affix at least 2 building photographs below according to the instructions for Item A6. Identify all photographs with date taken; "Front View" and "Rear View"; and, if required, "Right Side View" and "Left Side View." When applicable, photographs must show the foundation with representative examples of the flood openings or vents, as indicated in Section A8. If submitting more photographs than will fit on this page, use the Continuation Page.



Photo One

Photo One Caption Front View

Clear Photo One



Photo Two

Photo Two Caption Rear View

Clear Photo Two

BUILDING PHOTOGRAPHS

ELEVATION CERTIFICATE

Continuation Page

OMB No. 1660-0008

Expiration Date: November 30, 2022

			<u> </u>
IMPORTANT: In these spaces, copy the corresponding information from Section A.			FOR INSURANCE COMPANY USE
Building Street Address (including Apt., Unit, Suite, and/or Bldg. No.) or P.O. Route and Box No. 38 Clinton Road			Policy Number:
City	State	ZIP Code	Company NAIC Number
Town of Fairfield	New Jersey	07004-2910	

If submitting more photographs than will fit on the preceding page, affix the additional photographs below. Identify all photographs with: date taken; "Front View" and "Rear View"; and, if required, "Right Side View" and "Left Side View." When applicable, photographs must show the foundation with representative examples of the flood openings or vents, as indicated in Section A8.



Photo Three

Photo Three Caption Ride Side View

Clear Photo Three



Photo Four

Photo Four Caption Left Side View

Clear Photo Four