#### ENGINEERING INVESTIGATION & ANALYSIS GEOTECHNICAL & STRUCTURAL ASSESSMENT REPORT

### 93 GLENROY ROAD EAST FAIRFIELD, NEW JERSEY 07004

# MATRIXNEWORLD Engineering Progress

### **Prepared for:**

State of New Jersey Department of Community Affairs PO Box 800 Trenton, NJ 08625-0800

### **Prepared by:**

Matrix New World Engineering, Land Surveying and Landscape Architecture, PC 26 Columbia Turnpike Florham Park, New Jersey 07932

Matrix No. 20-1052

September 2021

Michael J. Soltys, P.E. Director of Structural & Geotechnical Engineering

**Engineering Progress** 

### **TABLE OF CONTENTS**

1.0	PROJECT BACKGROUND1
2.0	PROJECT SCOPE
3.0	SITE LOCATION & PROJECT DESCRIPTION
4.0	GEOLOGIC SETTING
5.0	SUBSURFACE FIELD PROGRAM
5.1	Test Pits5
5.2	SPT Borings
5.3	Laboratory Testing
6.0	SUBSURFACE CONDITIONS
7.0	GEOTECHNICAL SUBSURFACE PARAMETERS11
8.0	STRUCTURAL INSPECTION
8.1	Existing Building Foundations13
8.2	Existing Equipment14
8.3	Site Observations
8.4	Elevation Requirements
8.5	Recommendations for Building Elevation16
9.0	CLOSURE
10.0	REPRESENTATIVE SITE PHOTOS

### **FIGURES**

1	Site Location Map
2	As-Drilled Boring & Test Pit Location Plan
3	Bedrock Geology Location Map
4	Surficial Geology Location Map

### APPENDICES

- Soil Boring & Test Pit Logs А
- В
- Soil Classification Tables Geotechnical Laboratory Testing Results С
- FEMA NFIP Elevation Certificate D

**Engineering Progress** 

#### **1.0 PROJECT BACKGROUND**

The State of New Jersey Department of Community Affairs (DCA), Division of Disaster Recovery and Mitigation, anticipates receiving approval for grant funding through FEMA's Flood Mitigation Assistance (FMA) appropriation. This funding is provided through FMA to states and local communities to reduce or eliminate flood risk due to repetitive flood damage to buildings insured by the National Flood Insurance Program (NFIP). The DCA intends to use the funding for the State's Mitigation Assistance Program (MAP) to elevate residential properties located in a floodplain in the Township of Fairfield. The properties are to be elevated at least 3 feet above the base flood elevation (BFE). The DCA hosted a town hall meeting for homeowners in Fairfield, focused on homeowners with properties that experience Repetitive Losses or Severe Repetitive Losses.

In preparation of procuring a Design-Build firm to conduct the effort, the DCA has contracted Matrix New World Engineering, Land Surveying and Landscape Architecture, P.C. (Matrix) to conduct a geotechnical analysis, preliminary structural analysis, and elevation certificate for residences anticipated to be included in the program. It is understood that this document will serve as the basis for the development of a Request for Proposal (RFP) to procure Design-Build firms to do final structural design and perform the elevation of the properties.

**Engineering Progress** 

#### 2.0 PROJECT SCOPE

Matrix has completed a geotechnical and structural assessment and elevation certificate to evaluate the viability of elevating the residential building located at 93 Glenroy Road East in Fairfield, New Jersey (Site). Matrix provided geotechnical and structural engineering and land surveying services as a consultant to the DCA. The project location is shown on the attached Site Location Map (Figure 1).

The purpose of the engineering study was to compile comprehensive data regarding the existing building's foundations and overall structural composition and condition at the Site. The information obtained will be further utilized to determine the feasibility and proposed design of raising the existing residence 3 feet above the base flood elevation (BFE) as determined by FEMA. A team of Matrix engineers and surveyors performed the evaluation, consisting of a geotechnical soil inspection, test pits to reveal the existing building foundations, an interior inspection of the building's visible foundation walls and frame, and topographic surveying for the development of a flood elevation certificate. One test pit (TP-1) was completed to a depth of 48 inches below the ground surface (bgs) and 2 geotechnical borings (B-1 and B-2) were completed to a depth of 27 feet bgs (see Figure 2).

Matrix's geotechnical characterization of the property is based on an engineering evaluation of the subsurface conditions as indicated by the field exploration data and geotechnical laboratory test results on representative soil samples.

**Engineering Progress** 

### 3.0 SITE LOCATION & PROJECT DESCRIPTION

The project site is located at 93 Glenroy Road East in Fairfield, New Jersey. The property consists of a twostory timber-frame colonial-style house with an approximately 2,130 square foot footprint. The house is situated atop concrete masonry unit (CMU) foundation walls on assumed cast-in-place concrete foundations. The residence contains a basement area that encompasses the entire living area footprint, as well as an attached garage on the west side of the building. The timber frame of the structure is covered in brick façade throughout its front exterior on the garage and first floor, while the rest of the building is covered in vinyl or polymer shingle siding.

To assist with the geotechnical and structural evaluation, test pits and geotechnical borings were advanced in areas around the residence to obtain information regarding the soil's structural properties and building's existing foundation. The test pit and 2 borings were located to provide the most useful information about the subsurface conditions. Refer to Figure 2 of this report for a map of the test pit and boring locations.

**Engineering Progress** 

### 4.0 **GEOLOGIC SETTING**

According to the USDA Soil Survey of Essex County, the site is entirely situated atop Horseneck-Urban land. The subsurface composition is typically sand and loamy sands from 8 to 60 inches bgs.

According to the 2014 Bedrock Geologic Map of New Jersey, the Site is underlain by the Sedimentary and Bedded Volcanic Rocks Towaco Formation. Specifically, the subsurface consists of micaceous, reddishbrown sandstone, siltstone, and silty mudstone in upward-fining sequences. The Bedrock Geologic Map is shown in Figure 3.

From the Surficial Geologic Map of Northern New Jersey, compiled by and edited by Byron D. Stone, Scott D. Stanford, and Ron W. White in 2002, the natural surface material (beyond fill) is suggested to be in the Alluvium deposit, which consists of poorly sorted Gravel and Sand overlain by laminated and thinly bedded Sand, Silt and Clay. The Surficial Geology map is shown in Figure 4.

The documented site conditions presented above are consistent with the findings from the subsurface investigation, in which Sand overlayed a layer of Clay, followed by a lower layer of Sand. Groundwater was encountered in the borings at approximately 8 to 10 feet bgs. Bedrock was not encountered during this subsurface program.

**Engineering Progress** 

#### 5.0 SUBSURFACE FIELD PROGRAM

The subsurface investigation was completed by generally accepted practices in the Geotechnical Engineering field and consisted of the advancement of 1 test pit and 2 Standard Penetration Test (SPT) borings using mud rotary drilling methods. Matrix retained Boring Brothers, Inc., located in Egg Harbor Township, NJ, to complete the subsurface field program.

A Matrix Geotechnical Engineer provided full-time drilling oversight, soil logging, and sample collection. Matrix prepared the field test pit and boring logs, which included sample depths, SPT-N blow counts, soil recovery, and soil descriptions based on the Burmister Soil Classification System followed by the Unified Soil Classification System (USCS) letter symbol. Test pit and soil boring logs are provided in Appendix A. Classification tables and charts used to determine the soil attributes are included in Appendix B.

Upon the completion of the field program, representative samples were subjected to geotechnical laboratory analyses. Laboratory results aided in soil classification and assessing the relevant engineering properties of the stratigraphic layers which were used in developing the revised geotechnical parameters outlined herein. Geotechnical laboratory reports are included in Appendix C.

#### 5.1 Test Pits

On August 9, 2021, Boring Brothers completed a foundation survey which included a test pit to a depth of 48 inches below the ground surface. The test pit was dug using a Kubota KX057-5 excavator and shovel to prevent any damage to the existing building foundations. The exterior edge of the building's foundation wall was exposed at the test pit location to analyze the conditions of the concrete foundation.

The Matrix Geotechnical Engineer also observed the subsurface soil conditions encountered within the test pits, noting the type and composition of the soils surrounding and beneath the existing footings. Test Pit TP-1 was conducted on the front wall of the building in the southwest corner. The test pit was backfilled with the original soils upon completion of the test pit log. No test pit samples were collected at the site for further analysis.

### MATRIX**NEWORLD** Engineering Progress

#### 5.2 SPT Borings

On August 9, 2021, Boring Brothers advanced 2 geotechnical borings with a Mobile CME 55 trackmounted drill rig using mud rotary drilling techniques.

Split spoon (SS) samples were collected in accordance with *ASTM D-1586*, *Standard Method for Penetration Test and Split-Barrel Sampling of Soils*. A standard 2-inch outer diameter split spoon, two feet in length, was used to collect the soil samples. An automatic 140-pound hammer having a 30-inch drop was used to drive the split spoon sampler. As a part of boring observation, the SPT blow counts were recorded for the 0- to 6-inch interval, the 6- to 12-inch interval, the 12- to 18-inch interval and the 18- to 24-inch interval. The SPT N-values for design purposes are reported as the sum of the SPT N values observed for the above referenced 6- to 12-inch interval and the 12- to 18-inch interval that the split spoon sampler was driven.

The Matrix Geotechnical Engineer observed the split spoon samples and collected representative samples in sealed containers for further examination. All borings were continuously sampled to 12 feet bgs and at every subsequent 5-foot interval thereafter. The 2 borings were advanced to depths of 25.5 and 27 feet bgs. The borings were backfilled with soil cuttings and bentonite hole plug (if necessary) upon completion of the borehole.

### 5.3 Laboratory Testing

In addition to the field investigation, a laboratory testing program was conducted to determine additional pertinent engineering characteristics of representative samples of on-site soils. The laboratory testing program was performed in general accordance with applicable ASTM standard test methods and included physical/textural testing of representative samples of various strata.

Upon review of the boring logs, Matrix selected representative samples for laboratory testing. Laboratory testing of selected samples was completed by TerraSense, LLC, located in Totowa, New Jersey. The following table presents a summary of the testing program.

The results of the laboratory testing program were utilized to assist in developing geotechnical design parameters and recommendations, and are provided in Appendix C.

Engineering Progress

Test	Testing Procedure	Quantity Performed	Sample Locations and Depth Intervals
Water Content	ASTM D2216	5	B-1: 4-6', 8-10', 15-17' B-2: 6-8', 20-22'
Sieve Analysis	ASTM D422	1	B-2: 6-8'
Atterberg Limits	ASTM D4318	3	B-1: 15-17' B-2: 20-22'
Percent Fines	ASTM D1140	1	B-1: 8-10' B-2: 20-22'
Combined Sieve & Hydrometer	ASTM D422	1	B-1: 4-6'

### Table 5.3-1: Laboratory Testing Program

**Engineering Progress** 

#### 6.0 SUBSURFACE CONDITIONS

The subsurface conditions beneath the site can be characterized by the following stratigraphy, proceeding from the surface materials downward, unless noted otherwise below. Classification tables and charts used to determine the soil attributes are included in Appendix B.

#### <u>Test Pit</u>

Test pit TP-1 was completed along the front basement wall, in the southwest corner of the building. Due to limited access, the concrete footing could not be reached during test pit excavation. The excavation was terminated along the length of the foundation wall at 48" bgs.

#### Surface Cover

The surface cover for boring B-1 and B-2 consisted of grass cover and topsoil, approximately 6 inches thick.

### Stratum 1: Upper Granular (SM)

Beneath the surface cover in each boring, a soil layer was encountered consisting of mostly brown coarseto-fine Sand with varying amounts of Silt and fine Gravel. This Sand layer extended from the bottom of the surface cover to 11.5 feet below the ground surface (bgs) in B-1 and approximately 13.5 feet bgs in B-2.

The SPT-N values in this layer ranged from 2 to 18 blows per foot (bpf), which is indicative of very loose to medium-dense Sand. The SPT N-values for Stratum 1 are summarized in the tables below.

Soil Boring Location	USCS Group Symbol	Depth Below Ground Surface	SPT N-Values	
B-1	SM	4-6'	2	
B-2	SM	0-8'	2-9	

Table 6.0-1: Very Loose to Loose SPT N-Values for Stratum 1

Soil Boring Location	USCS Group Symbol	Depth Below Ground Surface	SPT N-Values
B-1	SM	0-4'	10-14
D-1	51VI	6-11.5'	17-18
B-2	SM	8-13.5'	13-18

**Engineering Progress** 

### Stratum 2: Clay (CH, CL)

Beneath the granular material of Stratum 1 in both borings, a soil layer was encountered consisting of grey to brown Silty Clay. This layer was encountered at 11.5 and approximately 13.5 feet bgs in borings B-1 and B-2, respectively. The layer extended to approximately 23 to 23.5 feet bgs in both borings. Deeper in the layer, the Clay material also contained varying amounts of fine Sand and Gravel.

The SPT N-values in this layer increased with depth, and typically ranged from 3 to 5 bpf, which is indicative of soft to medium-soft Clay. In boring B-1, an N-value of 18 bpf was recorded at the 20-22-foot soil sample, signifying very stiff cohesive material. The SPT N-values for Stratum 2 are summarized in the tables below.

<b>Table 6.0-3</b>	<b>3: Soft Clay</b>	SPT N-V	alues for	Stratum 2

Soil Boring Location	oil Boring Location USCS Group Symbol		SPT N-Values
B-1	СН	11.5-18.5'	3
B-2	СН	13.5-18.5'	4

Table 6.0-4: Medium-Soft Clay SPT N-Values for Stratum 2

Soil Boring Location	oring Location USCS Group Symbol		SPT N-Values
B-2	CL	18.5-23'	5

Table 6.0-5: Very Stiff Clay SPT N-Values for Stratum 2

Soil Boring Location	USCS Group Symbol	Depth Below Ground Surface	SPT N-Values
B-1	CL	18.5-23.5'	18

### Stratum 3: Lower Granular (GP, SC)

Beneath the Clay layer (Stratum 2) in both borings, a soil layer was encountered with varying composition. In boring B-1, this layer consisted of grey fine Gravel. In boring B-2, this layer consisted of red-brown coarse-to-fine Sand with some Clay and Silt and little coarse-to-fine Gravel. This Lower Granular layer was encountered at approximately 23.5 feet bgs in both borings, and each boring was terminated within this layer at 25.5 feet bgs (B-1) and 27 feet bgs (B-2).

The SPT-N value in this layer was recorded at 41 bpf in boring B-2, which is indicative of dense Sand. In boring B-1, split spoon refusal (no movement in 100 blows) was encountered at 25.5 feet bgs. The SPT N-values for Stratum 3 are summarized in the tables below.

Soil Boring Location	USCS Group Symbol	Depth Below Ground Surface	SPT N-Values	
B-1	GP	23.5-25.5'	100/0"	
B-2	SC	23-27'	41	

Table 6.0-6: Dense to Very Dense SPT N-Values for Stratum 3

### **Groundwater**

Groundwater levels could not be measured during drilling in either boring, due to the use of water and drilling mud to advance the borings. Based on soil saturation levels, the groundwater table was expected to lie approximately between 8 and 10 feet bgs during the drilling program. Saturated soils were encountered in B-1 at 8 feet bgs and in B-2 at 10 feet bgs. It should be noted that the groundwater levels will vary with temperature, precipitation, and other climatic factors.

**Engineering Progress** 

### 7.0 GEOTECHNICAL SUBSURFACE PARAMETERS

The geotechnical design parameters in this report are derived from the field program and are based on accepted geotechnical standards and practices. At the time of the geotechnical assessment, loading conditions and the final proposed grading plans were not available. Therefore, certain assumptions were made for the recommendations provided in this report.

Table 7.0-1 summarizes the recommended geotechnical design parameters for the various soil strata encountered at the Site. The values are based on review and interpretation of the subsurface field program and laboratory test data results.

Table 1806.2 of the 2018 International Building Code provides allowable coefficients of friction to be used in the evaluation of resistance to sliding.

**Engineering Progress** 

	Unit	Friction Angle	Cohesive Strength,		ressure ïcient	Net Allowable	Lateral
Stratum	Weight	(Φ)	cu	Active	Passive	Foundation Pressure*	Bearing
	(pcf)	(deg)	(psf)	(Ka)	(Kp)	(psf)	(psf/ft. bgs)
Native Medium-Dense to							
Dense Granular Soil	$\gamma = 125$	32°	0	0.31	3.26	4,000	200
(SM, SC, GP)	$\gamma' = 63$	52	0	0.51	5.20	4,000	200
[SPT N > 10]							
Native Loose Granular Soil	n = 120						
(SM, SC, GP)	$\gamma = 120$ $\gamma' = 58$	30°	0	0.33	3.00	2,500	150
[SPT N ≤ 10]							
Native Clay Material (CL)	$\gamma = 120$						
Very Stiff - Hard		-	2,000	-	-	3,000*	100
[SPT N > 30]	γ' = 58						
Native Clay Material (CL)	$\gamma = 100$						
Medium-Soft		-	1,000	-	-	1,500*	75
$[4 \leq \text{SPT N} \leq 8]$	γ' = 38						
Native Clay (CL, CL-ML)	$\gamma = 90$						
Very Soft - Soft		-	500	-	-	1,000*	N/A
[SPT N < 4]	γ' = 28						

#### Table 7.0-1: Geotechnical Design Parameters

Notations: γ = moist unit weight, γ ' = buoyant unit weight, and c<sub>u</sub> = average undrained shear strength.
 + Allowable foundation pressure is contingent upon either replacement of at least two feet of existing fill below the bottom of footing by a Controlled Fill, or upon confirmation that the field density of the existing fill material down to four feet below the bottom of footing meets 95% of the maximum dry density of the existing fill material observed in Modified Proctor Tests.

- \* These values are based on the 2018 International Building Code, New Jersey Edition, and adjusted for field conditions encountered. To increase the allowable foundation pressure above the values recommended in the table given above, further testing of soil will be required. In Cohesive soils, it should be noted that the shallow footing may fail under the settlement criteria before the footing pressure approaches the anticipated allowable bearing capacity. Allowable Foundation Pressure values assume the water table is below the influence depth of the foundation.
- Coefficient of earth pressure at rest may be computed using Jaky's equation,  $K_0 = 1 Sin \phi'$ .

**Engineering Progress** 

#### 8.0 STRUCTURAL INSPECTION

The following sections present the results of the structural inspection of the residential building at 93 Glenroy Road East in Fairfield, New Jersey. The conclusions presented herein are derived from Matrix's geotechnical and structural investigation of the existing soils and building foundations and framing configurations, along with pertinent survey data as compiled by Matrix's team of land surveyors.

Matrix conducted a subsurface investigation that included both a test pit and soil borings to obtain maximum pertinent information regarding the existing site conditions (refer to Section 6.0 of this report). The test pit performed at the site exposed the exterior portion of the building's foundation wall, allowing for measurement of dimensions of the structure and assessment of the construction methods utilized. Two geotechnical borings were also conducted to gain further information regarding the existing soils beneath the site.

In addition to the geotechnical investigation, Matrix also conducted a structural site inspection to observe the existing foundation walls and framing of the building. Matrix's structural engineer was granted access to the residence's basement and garage to observe the building's foundation structure. Substructure composition was recorded, including beam/girder type, building dimensions, and spacing of structural components. Structural defects, if any, were also noted during the inspection and have been included within Section 8.3.

#### 8.1 Existing Building Foundations

The building at 93 Glenroy Road East is supported by concrete masonry unit (CMU) walls throughout its foundation. The structure is broken up into two separate foundation sections (basement and garage), each with a different finished floor elevation.

The basement area of the building encompasses the full living area of the structural footprint beneath the first and second floors, measuring approximately 32'-8" long x 48'-9" wide. The basement walls consist of 8"x8"x16" CMU blocks and extend 84 inches in height (measured from the floor surface). The rear and east walls of the basement widen by 4" approximately 60 inches above the floor surface, protruding inward into the basement area. The basement measures 8'-1" in height from the floor to the bottom of the first-floor floorboards. The floor of the basement consists of poured concrete with a painted finish. An approximately 1" wide x 3" deep gap was observed between the floor slab and walls of the basement throughout the perimeter of the area. The foundation walls of the basement support the timber subfloor

**Engineering Progress** 

above, which consists of nominal 2x10 timber floor joists, spaced 16" on center. The floor joists vary in span direction, as the rear half, southwest corner, and southeast corner joists run north to south (front to rear), while the rest of the joists run east to west. The floor joists are connected to the sides of timber girders, which consist of (4) nominal 2x12 timber members. A total of 5 girders were observed supporting the first floor, and three of these girders were further supported along their length by 4" diameter steel post columns. The longest clear span of a girder, located in the southeast corner of the house, was measured at 15'-4" long.

A test pit excavation was performed at the southwest corner of the basement to determine the type and size of the building's wall footings. However, due to site constraints, the foundation wall footings could not be reached to determine the structural dimensions. Based on conventional foundation construction, Matrix assumed a 16" wide concrete spread footing as a minimum value for analysis, but expects the building footings to be within 16" to 24" wide. Prior to raising the house, Matrix recommends that the contractor confirm the foundation size and bearing adequacy with multiple test pits around the building perimeter.

The garage area, adjacent to and west of the basement, is located at ground level (approximately 65" above basement floor) with brick stairs leading up to the first floor in the northwest corner of the garage. The CMU foundation walls continue around the perimeter of the garage to support the timber building frame, and extend 18" to 19.5" above the garage floor surface (top of wall consistent in elevation throughout building footprint). The garage is about 10'-8" in height measured from the concrete slab floor surface, and the first floor of the house is approximately 33" above the garage floor.

#### 8.2 Existing Equipment

Various pieces of equipment and machinery were observed within the basement at the time of the inspection. The northwest corner of the basement contained a boiler unit and hot water heater, both raised atop CMU blocks (11" and 8" above the floor surface, respectively). Also in this corner, a sump pit was observed within the ground and a central vacuum cleaner was elevated 39" above the floor surface. The southeast corner of the basement contained a gas meter (54" above the floor), electrical panel (60" above the floor), and a water meter (27.5" above the floor). Also, along the front wall near the southwest corner, a security system panel was observed approximately 66.5" above the floor surface. Various metal and PVC conduits, as well as electrical cables, were also observed running along the timber members of the first-floor joists and girders.

No equipment was observed in the garage area of the building.

Outside the building, in the northwest corner (rear yard), a single air conditioner unit was observed situated atop a concrete slab platform (elevated approximately 6" above the adjacent concrete ground surface). A generator was also observed at the ground level along the east wall of the house.

#### 8.3 Site Observations

The basement/garage walls and visible first-floor floor joists were in good condition at the time of the inspection. No notable damages or abnormalities were observed.

The second floor of the house was seen to overhang the first floor by approximately 1 foot in the front of the building only. Above the front entrance, the roof overhangs the rest of the house by about 6 feet. Two columns support this roof overhang at the southwest and southeast corners of the front entrance porch. These columns are encased in a decorative wood covering, so the type and size of the columns could not be determined at the time of the inspection.

A stove/oven was observed in the basement at the time of the inspection, situated along the center of the rear wall at floor level. Though a gas line appeared to be connected to the appliance, it was unclear if the stove was in working order.

A CMU block exhaust chimney was observed behind the boiler and hot water heater in the basement, and extends up along the second-floor west wall of the house.

The exposed portions of the foundation walls along the exterior of the building are covered in a stucco coating. This coating exhibited minor to moderate cracking throughout, and the coating was missing in some areas of the wall.

The rear and east walls of the house are surrounded by a concrete walkway and patio around the building perimeter. Also, in the rear yard and adjacent to the southwest corner of the building, an elevated brick patio has been constructed with its floor surface level with the first floor of the house. Measuring approximately 9'-9" long x 16'-4" wide, the patio also contains brick stairs to connect the structure to the adjacent concrete slabs that make up the rear ground-level patio at the site.

**Engineering Progress** 

#### 8.4 Elevation Requirements

The FEMA 100-year flood elevation at 93 Glenroy Road East is El. +174 (NAVD88). As per the New Jersey Department of Community Affairs (DCA), and in accordance with the New Jersey Flood Hazard Area Control Act, the lowest floor of newly elevated buildings must be at least 3 feet above the base flood elevation. Therefore, the new first floor elevation must be at El. +177 or higher to meet the requirements set forth in the program.

The current first-floor elevation at the Site is at El. +173.23, with the adjacent garage floor at El. +170.49. To achieve the elevation requirements, the existing building would need to be raised approximately 3.7 feet. Matrix recommends raising the building at least 4.7 feet to allow for the creation of a ground-level beneath the newly raised building.

#### 8.5 **Recommendations for Building Elevation**

Matrix recommends that the existing foundation system of the residential building at 93 Glenroy Road East be kept and extended to achieve the required design flood elevation. The presence of both basement and crawl space foundation walls is expected to provide sufficient support for the additional height of the newly raised building. Based on loading estimation and analysis for the existing building, Matrix estimates that the anticipated additional dead load of the required new courses of CMU would remain under an allowable bearing capacity as low as 1,000 psf (design capacity of soft Clay encountered at the Site) for the shallow concrete strip footings at the Site.

In accordance with NFIP requirements, it is required that the existing basement and crawl space be filled in to match the lowest adjacent exterior grade following raising. The newly raised house will have approximately 7.4 feet of space beneath (down to existing finished grade), which is enough vertical height for a ground-level floor. This additional space beneath the raised building can be used for storage at the resident's discretion.

The most feasible method of elevation for the building consists of jacking up the entire residential structure from below using steel beams and jack posts. The building will then sit atop temporary cribbing while the existing CMU basement and garage walls are heightened with additional courses of masonry block units. Additional vertical reinforcement would need to be installed in ungrouted masonry cells to properly transfer loads through the new heightened wall to the existing wall, and horizontal ladder reinforcement should be installed at a minimum of every other course. Also, the existing steel post columns intermittently supporting

**Engineering Progress** 

the building's girders must be removed and replaced by new steel, concrete or masonry block columns. These new columns will need to include a spread footing beneath to sufficiently support the building loads.

The garage door located in the front of the house will need to be removed prior to raising, and the opening replaced with a new timber-framed wall to match the rest of the building. The garage door will then be replaced at the ground level once the house is elevated. The existing brick exhaust chimney will also require extending during raising of the house to keep the top of the chimney above the roof level.

The rear brick patio is anticipated to require raising to match the proposed ingress/egress heights of the main structure. This would require reconstruction of the brick patio to raise the walls of the structure to the new first floor elevation. If additional brick is deemed infeasible, the existing stationary brick patio can be removed and replaced with an elevated timber deck, or the brick patio can be left in place and a new timber deck of equivalent square footage built around and above it to create a new exterior deck level with the first-floor elevation.

Raising of the building should be undertaken with special attention to preserve the existing brick façade covering the timber frame. If the façade is kept in place during raising, the process is liable to lead to some cracking in the existing façade. Alternatively, the brick can be removed prior to raising, then replaced with a similar or more flexible finish after completion of the elevation process. The materials and labor involved in exterior façade restoration of the house are not within the scope of this project.

Within the new foundation walls, permanent openings are required to allow floodwater to enter the ground level and equalize the hydrostatic pressure during a flood event. As per the 2018 International Residential Code, New Jersey Edition, the total net area of non-engineered openings must comprise at least 1 square inch for every square foot of enclosed space within the building's ground floor. This equates to approximately 14.8 square feet of total flood openings in the building's new foundation walls. Additionally, a minimum of two openings must be provided for each enclosed area of the new ground floor. These openings must be located no higher than one foot above the adjacent finished exterior grade along the building perimeter. Matrix recommends the use of engineered openings in lieu of non-engineered openings to maximize efficiency and minimize the quantity of openings required.

Additionally, any service equipment, whether outside or in the basement, such as air conditioning, heat pump compressors, gas meters, electric meters, and hot water heaters, must be elevated 3 feet above the

**Engineering Progress** 

BFE. For interior elements, this may include relocation to an upper floor and thus less usable living space. For this residence, the hot water heater, boiler, gas meter, water meter, electrical panel, central vacuum cleaner, and security panel in the basement would require elevating 3 feet above the BFE. The exterior air conditioner unit and generator will also need to be elevated 3 feet above the BFE on new, elevated platforms.



**Engineering Progress** 

### 9.0 CLOSURE

This report has been prepared to assist the State of New Jersey Department of Community Affairs with the structural and geotechnical evaluation of the residential building at 93 Glenroy Road East in Fairfield, New Jersey. The conclusions and recommendations provided within this report were prepared based on our understanding of the project and through the application of generally accepted engineering practices. No warranties, expressed or implied, are made. Matrix should be notified of any changes to the existing building foundation system or if subsurface conditions differing from those described herein are encountered, so the impact on the geotechnical and/or structural recommendations can be evaluated.

Engineering Progress

### **10.0 REPRESENTATIVE SITE PHOTOS**

### **Structural Inspection Photos**



Photo 1. 93 Glenroy Road East (Front of Building)



Photo 2. 93 Glenroy Road East (Front of Attached Garage) 20



Photo 3. 93 Glenroy Road East (Rear of Building, West Side)



Photo 4. 93 Glenroy Road East (Rear of Building) 21

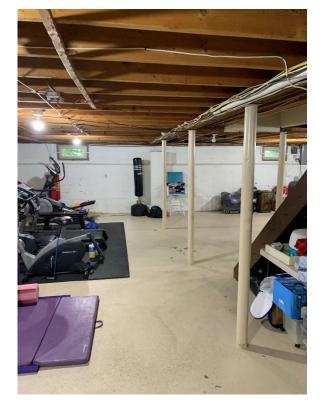


Photo 5. Basement CMU Walls and First Floor Subfloor (Looking Southeast)



Photo 6. Timber Girder with Steel Post Column (Typical)

Engineering Progress

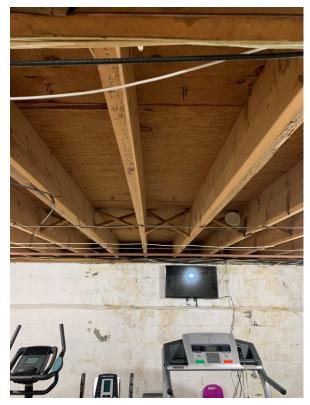


Photo 7. First Floor Timber Floor Joists (Typical)



Photo 8. Boiler & Hot Water Heater in Basement (Looking North)

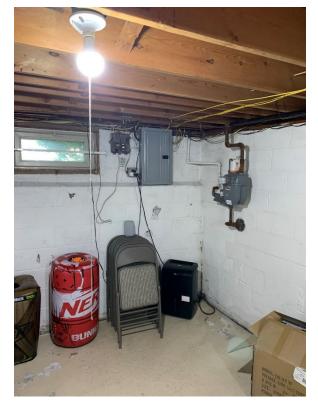


Photo 9. Gas Meter & Electrical Panel in Basement (Looking South)



Photo 10. Garage Walls with Stairs to First Floor of Building (Looking East)



Photo 11. Rear Brick Patio



Photo 12. Roof Overhang with Column Supports on Front Porch

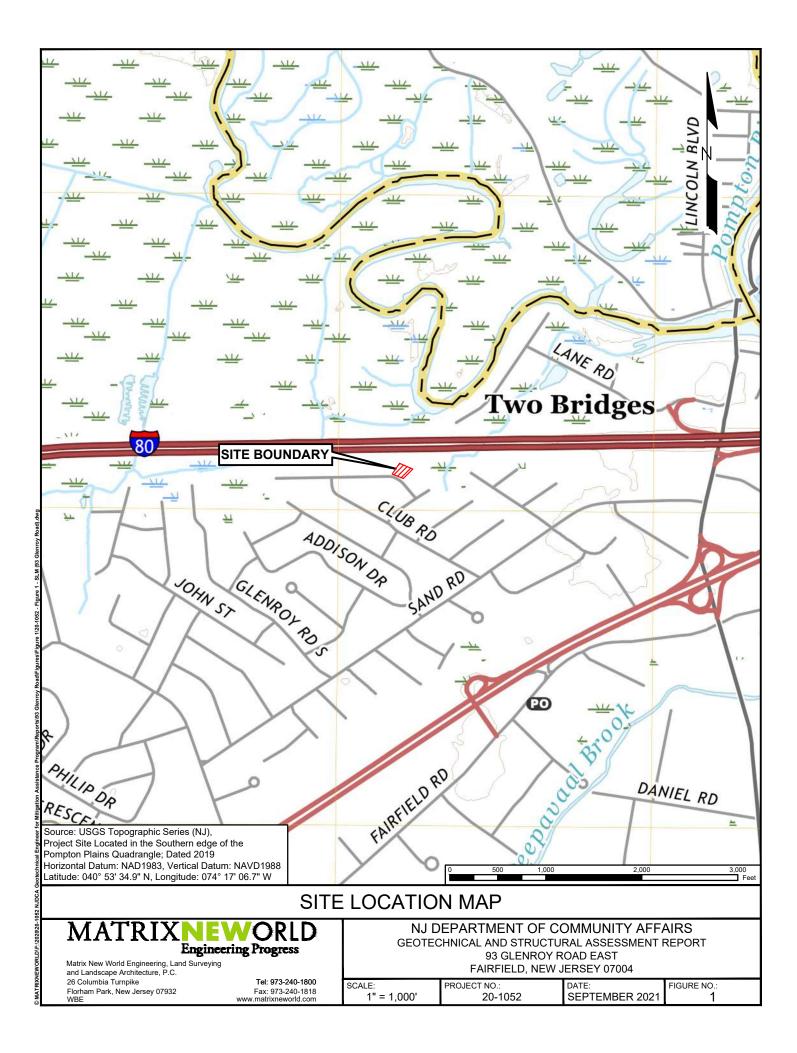


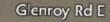
Photo 13. Test Pit TP-1 Location (Front of Building – Basement, Southwest Corner)



Photo 14. Test Pit TP-1 Foundation Wall Conditions

FIGURES





#### NOTES:

ď

- 1. THIS FIGURE IS BASED ON IMAGERY PROVIDED BY MICROSOFT BING.
- 2. BORING LOCATIONS WERE IDENTIFIED IN THE FIELD BY MATRIX PERSONNEL BY TAPING AND LINE OF SIGHT MEASUREMENTS.
- 3. THE BORINGS WERE PERFORMED BY BORING BROTHERS, INC. ON AUGUST 09, 2021 UNDER THE DIRECTION OF A MATRIX REPRESENTATIVE.
- ALL ELEVATIONS SHOWN ON THIS PLAN REFER TO THE NORTH AMERICAN VERTICAL DATUM OF 1988 (NAVD88).

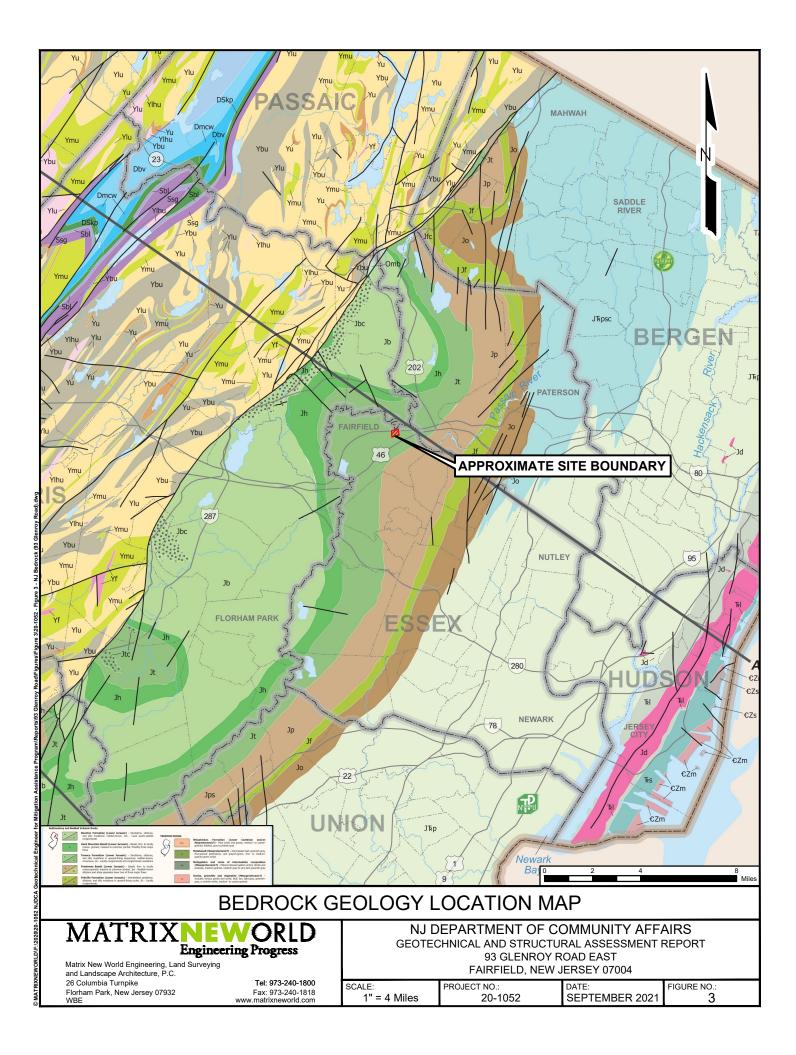
SCALE: 1" = 40

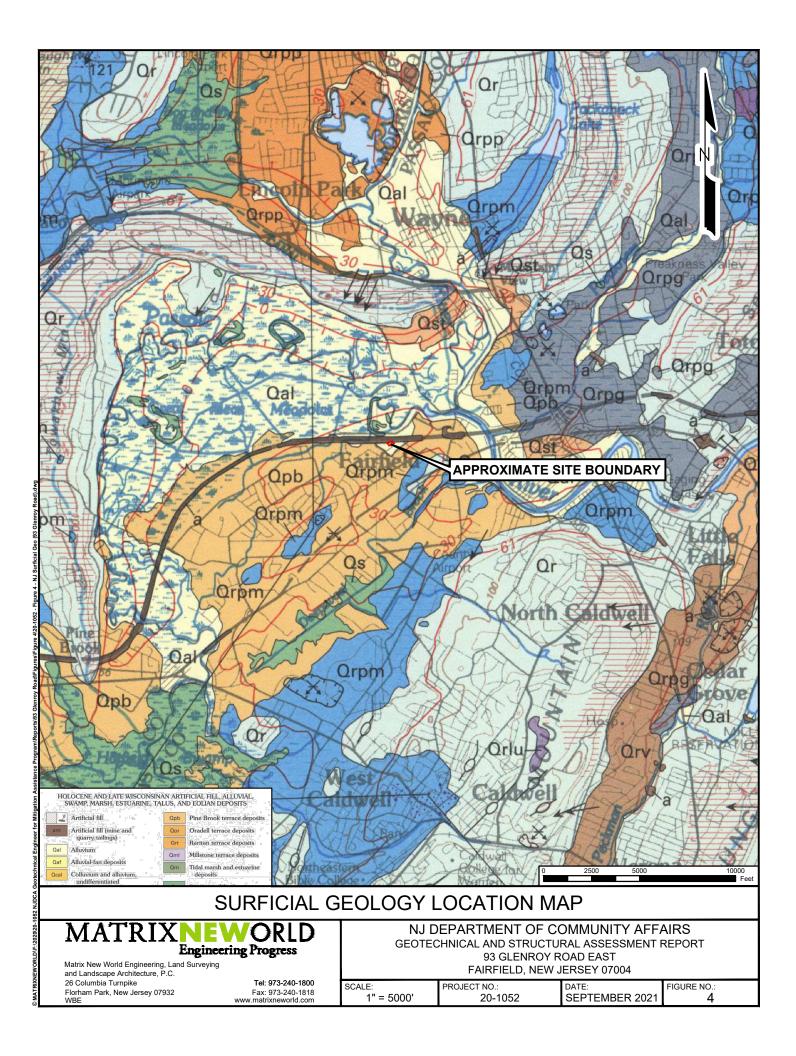
#### LEGEND

B-# 🔶 AS-DRILLED BORING LOCATION

TP-# 🔶 TEST PIT LOCATION







### APPENDIX A

SOIL BORING & TEST PIT LOGS

Engineering Progress

### **BORING LOG**

BORING NO.: B-1

SHEET <u>1</u> OF <u>1</u>

PROJECT NO.: 20-1052	PROJECT: NJDO	CA Geotechnica	al Engineer for Mi	tigation Assistan	ce Program DATE:	8/09/21
PROJECT LOCATION:	Fairfield, N.	J	BORING LOCATI	ON: 93 Glenroy	Road East, West Sid	e in Front of House
DRILLING EQUIPMENT:	CME 55 AN	IGLE: <u>-90.0</u>	DIR.:	ELEV.:	DATUM:	NAVD88
DRILLING CONTRACTOR:	Boring Brothe	ers, Inc.	DRILLER:	D. Osuch	INSPECTOR:	A. Radiola

	CASING an	d HAMMER		SAMPLER and HAMMER				GROUNDWATER LEVELS			
Туре	I.D.	Weight	Drop	Туре	I.D.	Weight	Drop	Date	Time	Depth	Casing Depth
Auto		140 lbs	30"	AUTO		140 lbs	30"	8/09/21		8.0	5
FJ Steel	4"			SS	1 3/8"						

Depth	CASING			SAMPLE		ol ci		Laboratory
Feet (Elev.)	Blows/ Foot	No.	Type	Depth Feet	Blows/6" (REC. %) [RQD %]	Graphic Symbol	Description Of Material	Tests
-		S-1	ss	0.5-2	7-7-7 (89%)	<u>7, 7</u> 7,	6" Grass/Topsoil S-1: Red-Brown fine SAND and Silt, trace fine Gravel, dense, dry	
-		S-2	SS	2-4	8-6-4-3 (54%)		(SM) S-2: Red-Brown fine SAND and Silt, trace fine Gravel, trace Vegetation, dense, dry (SM)	
5	4" Casing	S-3	SS	4-6	WOH/12"- 2-3 (63%)		S-3: Grey-Green fine SAND and Clayey Silt, trace fine Gravel, moist (SM) WC: 19.5%, Gravel: 0.3%, Sand: 64.2%, Fines: 35.5%, <2 μm: 9%	Sieve; Hydrometer
-		S-4	SS	6-8	6-8-10-8 (96%)		S-4: Brown mf SAND, little Silt, trace fine Gravel, moist (SM)	
- -		S-5	SS	8-10	7-9-8-10 (100%)		S-5: Brown cmf SAND, some Silt, trace fine Gravel, wet (SM) WC: 14.7%, Fines: 27%	Pass No 200
[10 		S-6	SS	10-12	4-8-10-7 (100%)		S-6A (Top 18"): Same as Above, wet (SM)	
1 - 1 - 1 17/2/1/6 1/		S-7	SS	15-17	1-2-1-4		S-6B (Bottom 6"): Grey Silty CLAY, dry (CH) S-7: Grey Silty CLAY, wet (CH)	Atterberg Limits
NEWORLD NO GROUT 20-1052 BORING LOGS.GPJ MATRIX EGS.GDT					(96%)		WC: 40.0%, LL: 52, PL: 23, PI: 29	Linnits
20-1052 BORING LOG		S-8	SS	20-22	8-10-8-17 (58%)		S-8: Brown CLAY & Silt and fine Sand, little fine Gravel, wet (CL)	
		S-9	SS	25-25.5	47-100/0" (17%)		_ S-9: Grey fine GRAVEL, wet (GP) Bottom of Borehole @ 25.5 ft.	
_	•					-	BORING NO.:	B-1

Engineering Progress

### **BORING LOG**

BORING NO.: B-2

SHEET <u>1</u> OF <u>1</u>

PROJECT NO.: 20-1052	PROJECT: NJD	CA Geotechnic	al Engineer for Miti	gation Assist	ance Program DATE:	8/09/21
PROJECT LOCATION:	Fairfield, N	J	BORING LOCATIC	N: 93 Glenr	oy Road East, East Sid	le in Front of House
DRILLING EQUIPMENT:	CME 55 AN	NGLE: <u>-90.0</u>	DIR.:	ELEV.:	DATUM:	NAVD88
DRILLING CONTRACTOR:	Boring Brothe	ers, Inc.	DRILLER:	D. Osuch	INSPECTOR:	A. Radiola

	CASING an	d HAMMER		SAMPLER and HAMMER				GROUNDWATER LEVELS			
Туре	I.D.	Weight	Drop	Туре	I.D.	Weight	Drop	Date	Time	Depth	Casing Depth
Auto		140 lbs	30"	AUTO		140 lbs	30"	8/09/21		10.0	5
FJ Steel	4"			SS	1 3/8"						

Depth	CASING		ę	SAMPLE		<u>.</u> 9		Laborator
Feet (Elev.)	Blows/ Foot	No.	Type	Depth Feet	Blows/6" (REC. %) [RQD %]	Graphic Symbol	Description Of Material	Tests
-		S-1	SS	0.5-2	2-2-2 (61%)	<u>77</u>	6" Grass/Topsoil S-1: Brown fine SAND, some Silt, trace fine Gravel, moist (SM)	-
-  -		S-2	SS	2-4	(0170) 2-1-1-1 (29%)		S-2: Red-Brown fine SAND, some Silt, trace fine Gravel, moist (SM)	
5	4" Casing	S-3	SS	4-6	1-1-1-1 (25%)		S-3: Grey/Green fine SAND and Clayey Silt, trace fine Gravel, mottled, moist (SM)	
 		S-4	SS	6-8	3-3-6-8 (96%)		S-4: Grey/Green mf* SAND, some Silt, mottled, moist (SM) WC: 17.8%, Gravel: 0.5%, Sand: 71.0%, Fines: 28.5%	Sieve
-		S-5	SS	8-10	6-7-6-7 (88%)		S-5: Brown mf* SAND, some Silt, little fine Gravel, moist (SM)	
10  		S-6	SS	10-12	6-9-9-11 (100%)		S-6: Brown cmf SAND, little Silt, trace fine Gravel, wet (SM)	
15 15 		S-7	SS	15-17	1-2-2-3 (79%)		S-7: Grey Silty CLAY, wet (CH)	-
- 20 -		S-8	SS	20-22	3-3-2-5 (96%)		S-8: Red-Brown CLAY & Silt and fine Sand, trace fine Gravel, wet (CL) WC: 18.7%, Fines: 60%, LL: 25, PL: 14, PI: 11	- Atterberg Limits; Pass No 200
25 25 		S-9	SS	25-27	29-20-21- 23 (54%)		Drill chatter at ~23 ft. bgs S-9: Red-Brown cmf SAND, some Clay & Silt, little cf Gravel, wet (SC)	
							Bottom of Borehole @ 27 ft.	



TEST	PIT LOG
------	---------

								SHEET	_1_	OF _	1
PROJECT NO .:	20-	1052	PROJECT: <b>NJ</b>	DCA Geotechnical Eng	ineer - Mitiga	tion Assist	ance Progra	mDATE:	8	/9/2021	1
TEST PIT LOCAT	FION:	93 G	Glenroy Road Ea	Fairfield, NJ ast (Front of Building -	Basement)	DATUM:		TIME F	INISHED:	9:45	5:00 AM
CONTRACTOR: EQUIPMENT:				ng Brothers, Inc.							
											-
Depth Inches (Elev) No.	Depth Inches	Graphic Symbol		Desc	ription Of M	aterial					oratory ests
	0-5	<u>17</u> 717 717	Topsoil, Mulch	Cover							
TEST PIT INCH 20-1052 TEST PIT LOGS.GPJ MATRIX EGS.GDT 9/16/21 10 11 12 12 10 12 12 10 12 12 10 12 12 12 12 12 12 12 12 12 12	5-48			ND and Silt, little fine Gra minated at 48" bgs due t pit @ 48 in. lled.		ss. Wall foot	ing not enco	untered.			

TP-1

TEST PIT NO.:

## LOG NOTATION

## Sample Classifications

- SS = Split Spoon
- NR = No Recovery
- NX = Rock Core
- SH = Shelby Tube
- REC = Soil Recovery
- RQD = Rock Quality Designation

## Sand Classifications

- c = Coarse
- m = Medium
- f = Fine
- \* = Predominant Grain Size

## Soil Properties

- WC = Water Content
- PL = Plastic Limit
- LL = Liquid Limit
- PI = Plasticity Index
- OC = Organic Content

# LOG GRAPHICAL LEGEND

	Asphalt
P. 4. 4.	Concrete
	Fill
	Topsoil
	Well graded Gravel (GW)
	Poorly graded Gravel (GP)
	Clayey Gravel (GC)
000	Silty Gravel (GM)
	Well graded Gravel with Clay (GW-GC)
X	Well graded Gravel with Silt (GW-GM)
	Poorly graded Gravel with Clay (GP-GC)
0	Poorly graded Gravel with Silt (GP-GM)
	Well graded Sand (SW)
	Poorly graded Sand (SP)
	Clayey Sand (SC)
	Silty Sand (SM)
	Well graded Sand with Clay (SW-SC)
	Well graded Sand with Silt (SW-SM)
	Poorly graded Sand with Clay (SP-SC)
	Poorly graded Sand with Silt (SP-SM)
	Lean Clay (CL)
	Silty Clay (CL-ML)
	Silt (ML)
	Organic Silt or Clay (Low Plasticity) (OL)
	Fat Clay (CH)
m	Elastic Silt (MH)
	Organic Silt or Clay (High Plasticity) (OH)
	Peat (PT)
	Decomposed Bedrock
Ŵ	Bedrock

# **APPENDIX B**

## SOIL CLASSIFICATION TABLES

м	AJOR DIVISION	IS	GROUP SYMBOLS	TYPICAL NAMES	(EXCLUDING	TIFICATION PR PARTICLES LA G FRACTIONS ( WEIGHTS)		INFORMATION REQUIRED FOR DESCRIBING SOILS		LABORATORY	CLASSIFICATION CRITERIA	۱.
1	2		3	4		5		6		8.6	7	]
	fraction is ve size. 4 sieve size.)	Clean Gravels (Little or no fines)	GW	Well-graded gravels, gravel-sand mixture, little or no fines.				For undisturbed soils add information on stratification, degree of compactness, cementation, moisture condition, and drainage characteristics.		tage of fine s:	$C_u = \frac{D_{60}}{D_{10}} \text{ Greater than 4}$ $C_e = \frac{(D_{30})^2}{D_{10} \times D_{60}} \text{ Between 1 a}$	and 3
size.	rels coarse fractio o. 4 sieve size, he No. 4 sieve	Clean	GP	Poorly graded gravels or gravel-sand mixture, little or no fines.	Predominantly o some intermedia		e of sizes with			follow	Not meeting all gradation requirements for GW	
o. 200 sieve	Gravels Gravels an half of coa er than No. 4 valent to the N	with Fines de amount of nes)	GM	Silty gravels, gravel and silt mixtures.	Nonplastic fines (for identificatio	or fines with low n procedures see	v plasticity ML below).			Depending or clæsified as symbols.	Atterberg limits below "A" line or P1 less than 4 between 4 a	
grained Soils is larger than N	Gravels More than half of coarse fraction is larger than No. 4 sieve size. be used as equivalent to the No. 4 sieve size.)	Sand Gravels no fines) (Appreciat fi	GC	Clayey gravels, gravel and clay mixtures.	Plastic fines (for identificatio	n procedures see	CL below).	Give typical name; indicate approximate percentages of sand and gravel, maximum size; angularity, surface condition, and hardness of the coarse grains; local or geologic name and other pertinent descriptive information; and symbol in parentheses.	on.	avel and sand from grain-size curve. Depending on percentage of fine 200 sieve size) coarse-grained soils are classified as follows: GW, GP, SW, SP, GM, GC, SM, SC. Borderline cases requiring use of dual symbols.	Atterberg limits above "A" line with P1 greater than 7	are orderline ases requiring se of dual
Coarse-grained Soils More than half of material is larger than No. 200 sieve size. st visible to the naked eye.	Sands e than half of coarse fraction is smaller than No. 4 sieve size. (For visual classification, the <sup>1</sup> <sub>4</sub> -in. size may be	ean Sand e or no fines)	sw	Well-graded sands, gravelly sands, little or no fines.	Wide range in g of all intermedia		stantial amounts		given under field identification	sand from gra size) coarse-g ,SW,SP, , SM, SC. ne cases requi	$C_{\ell} = \frac{D_{60}}{D_{10}} \text{ Greater than 6}$ $C_{\ell} = \frac{(D_{30})^2}{D_{10} \times D_{60}} \text{ Between 1 a}$	and 3
than he ble to th	ction is size. n. the '/	Clean (Little or)	SP	Poorly graded sands or gravelly sands, little or no fines.	Predominantly o some intermedia		e of sizes with			gravel and . 200 sieve GW, GP, GM, GC Borderli	Not meeting all gradation requirements for SW	
Coarse sieve size. More than half of materia No. 200 sieve size is about the smallest visible to the naked eye	Sands of coarse fractic No. 4 sieve size classification. th	h Fines amount of s)	SM	Silty sands, sand-silt mixtures.	Nonplastic fines (for identificatio			Example: Silty sand, gravelly; about 20% hard, angular gravel particles <sup>1</sup> / <sub>2</sub> -in. maximum size; rounded and subangular sand grains, coarse to fine; about 15%	SS.	- <u>6</u> ,	Atterberg limits above "A" line or P1 less than 4 Limits plotti in hatched z with P1 between 4 a	zone
	More than half of N (For visual cl	Sands with Fines (Appreciable amount of fines)	SC	Clayey sands, sand-clay mixtures.	Plastic fines (for identificatio	n procedures see	CL below).	nonplastic fines with low dry strength; well compacted and moist in place; alluvial sand; (SM).		Determine percentage o (fraction smaller than N Less than 5% More than 12% 5% to 12%	Atterberg limits above "A" line with Pl greater than 7 are borderline cases requir use of dual symbols.	iring
ze. sieve s				1	Identification Procedure on Fraction Smaller than No. 40 Sieve Size.				identif			
200 sieve size. The No. 200 s					Dry Strength (Crushing Characteristics)	Dilatancy (Reaction to shaking)	Toughness (Consistency near PL)		ze curve in identifying the fractions			
ın No.	and Clays limit is less	00 1	ML	Inorganic silts and very fine sands, rock flour, silty or clayey fine sands or clayey silts with slight plasticity.	None to slight	Quick to slow	None	For undisturbed soils add information on structure,	Use grain-size	Fo	LIQUID LIMIT PLASTICITY CHART r laboratory classification of	
rained Soils s smaller tha	Silts ar Liquid li	man	CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays.	Medium to high	None to very slow	Medium	stratification, consistency in undisturbed and remolded states, moisture and drainage conditions	5		fine-grained soils	
Fine-g iterial i	imit is		OL	Organic silts and organic silty clays of low plasticity.	Slight to medium	Slow	Slight	Give typical name; indicate degree and character of		bu the second se	oparting Soils at Equal Liquid Limit	
Fine-grained More than half of material is smal	and Clays Liquid limit is greater than 50		МН	Inorganic silts, micaceous or diatomaceous fine sandy or silty soils, elastic silts.	Slight to medium	Slow to none	Slight to medium	plasticity; amount and maximum size of coarse grains; color in wet condition; odor, if any; local or geologic name and other pertinent descriptive		> Tem	hness and Dry Strength Increase Increasing Placticity Index. CH	Linc
ore than	nd Clay		СН	Inorganic clays of high plasticity, fat clays.	High to very high	None	High	information; and symbol in parentheses.		20	CL. OH	
Mc	Silts a	Silts and e	он	Organic clays of medium to high plasticity, organic silts.	Medium to high	None to very slow	Slight to medium	Example: Clayey silt, brown; slightly plastic; small percentage		10 14 00 10	MI MI MH 20 30 40 50 60 70 80 50	50 100
Hi	ighly Organic So	ils	Pt	Peat and other highly organic soils.	Readily identifie frequently by fit		spongy feel and	of fine sand; numerous vertical root holes; firm and dry in place; loess; (ML)				

 Boundary classifications: Soils possessing characteristics of two groups are de
 All sieve sizes on this chart are U.S. standard.
 Adopted by Corps of Engineers and Bureau of Reclamation, January 1952. GM-GC, well-graded gravel-sand mixture with clay binder. S. FOI sig bу g upsy

#### BURMISTER SOIL IDENTIFICATION METHOD

#### BURMISTER SOIL IDENTIFICATION METHOD

#### 1. <u>SOIL MATERIAL</u> Composition, Gradation, and Plasticity Characteristics a) Soil Components and Soil Fractions

Sieve	3"	1"	3/8"	No. 10	No. 30	No.	60	No. 200	
				2 mm				0.076 mm	0.02 mm
Granular		GRAV	/EL		SAND	)		SI	LT
Component Fractions	coarse	mediu	ım f	ine coar	se medi	ium	fine	coarse	fine
Clay Soil									-SOIL
Components								Defined and	
								Plastici	ty Basis

b) Identifying Terms for Granular Soils

Composition and Proportion Terms for Components

Component		Proportion	Defining Range		
		Terms	of Percentages		
Principal Compone (all Uppercase)	nts- GRAVEL, SAND, SILT		50% or more		
Minor Components	- Gravel	and	35 to 50%		
	Sand	some	20 to 35%		
	Silt	little	10 to 20%		
		trace	1 to 10%		
Gradation Terms fo	r Granular Soils	ORGANIC SOILS			
coarse to fine	all fractions more than 10%	Plastic	city Basis, as		
coarse to medium	fine less than 10%				
medium to fine	coarse less than 10%	Organi	c SILT, H. PI		
medium	coarse and fine less than 10%				
fine	coarse and medium less than 10%	Organic SILT, L. PI			
PLUS or MINUS sig	gns used to indicate upper or lower limits.	5			

 c) Identifying Terms for CLAY SOILS. Plasticity Basis for Combined Silt and Clay Components, Expressing the Relative Dominance of Clay

Overall Plasticity	Plasticity Index	Principal Component	Minor Component
Non-Plastic	0	SILT	Silt
Slight	1 to 5	Clayey SILT	Clayey Silt
Low	5 to 10	SILT & CLAY	Silt & Clay
Medium	10 to 20	CLAY & SILT	Clay & Silt
High	20 to 40	Silty CLAY	
Very High	more than 40	CLAY	

Example: Soil 60% coarse to fine Sand, 25% medium to fine Gravel, 15% Clayey Silt and color-brown.
 Identification: Br. coarse to fine SAND, some medium to fine Gravel, little Clayey Silt.

- References: 1) D. M. Burmister, "Principles and Techniques of Soil Identification" 29<sup>th</sup> Highway Research Board Proceedings, 1949.
  - "Identification and Classification of Soils An appraisal and Statement of Principles", ASTM Special Technical Publication No. 113, 1951.

# Field Classification of Soil Using the USCS

SPT N-Value (corrected)	Apparent Density
0 - 4	Very loose
5 - 10	Loose
11 - 30	Medium Dense
31 - 50	Dense
> 50	Very Dense

## **Apparent Density of Coarse-Grained Soils**

## **Consistency of Fine-Grained Soils**

SPT N-Value (uncorrected)	Consistency	Compressive Strength (ksf)	<b>Results of Manual Manipulation</b>
< 2	Very Soft	< 0.5	Specimen (height = twice the diameter) sags under its own weight; extrudes between fingers when squeezed
3 - 4	Soft	> 0.5 - 1.0	Speciment can be pinched in to between the thumb and forefinger; remolded by light finger pressure
5 - 8	Medium stiff	> 1.0 - 2.0	Can be imprinted easily with fingers; remolded by strong finger pressure
9 - 15	Stiff	> 2.0 - 4.0	Can be imprinted with considerable pressure from fingers or indented by thumbnail
16 - 30	Very stiff	> 4.0 - 8.0	Can be barely imprinted by pressure from the fingers or indented by thumbnail
> 30	Hard	> 8.0	Cannot be imprinted by fingers or difficult to indent by thumbnail

# **APPENDIX C**

## GEOTECHNICAL LABORATORY TESTING RESULTS

#### Matrix New World Engineering, P.C. #20-1052-017 NJDCA MAP - 93 Glenroy Road East LABORATORY TESTING DATA SUMMARY

BORING	SAMPLE	DEPTH			IDENTI	FICATIO	N TESTS			REMARKS
			WATER	LIQUID	PLASTIC	PLAS.	USCS	SIEVE	HYDRO.	
NO.	NO.		CONTENT	LIMIT	LIMIT	INDEX	SYMB.	MINUS	% MINUS	
							(1)	NO. 200	2 µm	
		(ft)	(%)	(-)	(-)	(-)		(%)	(%)	
B-1	S-3	4-6	19.8				SM	35.5	9	
B-1	S-5	8-10	14.7				SM	27		
B-1	S-7	15-17	40.0	52	23	29	СН			
B-2	S-4	6-8	17.8				SM	28.5		
B-2	S-8	20-22	18.7	25	14	11	CL	60		

Note: (1) USCS symbol based on visual observation and Sieve and Atterberg limits reported.

**TerraSense** 45H Commerce Way Totowa, NJ 07512

COBB	BLES	COBBLES GRAVEL SAND					SAND	SILT or CLAY		Symbol		$\diamond$	0
		COARSE		FINE	COA	ARSE MED	IUM FINE			Boring	B-1	B-2	
	-	=						7		Sample	S-3	S-4	
		1/2	4	≅o		0	20 660 1140	440 #100 #2000				6-8	
1			<del>; 0</del>	<del>• @</del>					· · · · · ·	% +3"	0	0	
		+++								% Gravel	0.3	0.5	
	90	+++	_							% SAND	64.2	71	
		+++	-		╎╎╎╎	+				%C SAND	0.2	4.8	
	80	+++	_							%M SAND	6.4	24.6	
		+++								%F SAND	57.6	41.6	
븄	70									% FINES	35.5	28.5	
EIG		+++							+	D <sub>100</sub> (mm)	9.53	9.53	
Š	60	+++	+						╡──┤│	D <sub>60</sub> (mm)	0.123	0.282	
B		+++								D <sub>30</sub> (mm)	0.059	0.082	
PERCENT PASSING BY WEIGHT	50	+++							<u>+</u>	D <sub>10</sub> (mm)	0.002		
SSA		+++	+							Cc	11.8		
L P/	40 +++++++		<u> </u>							Cu	51.3		
		111								Sieve			
RC	30	+++	_							Size/ID #		Percent Finer Da	ta
H H			+							6"	100.0	100.0	
	20	+++	+							4"	100.0	100.0	
								Ů <u>ŮŮŮŮŮŮ</u>		3"	100.0	100.0	
	10	$\frac{1}{1}$	+							1 1/2"	100.0	100.0	
		1 1 1								1"	100.0	100.0	
	0 +	!!!							<u> </u>	3/4"	100.0	100.0	
	100			10		1	0.1 PARTICLE SIZE -mm	0.01	0.001	1/2"	100.0	100.0	
										3/8"	100.0	100.0	
	n Symbols:						ted for complete sample			#4 #10	99.7 99.5	99.5 94.7	
SYMBOL	w (%)			-	USCS	AASHTO		RIPTION AND REMARKS	DATE	#10 #20	99.5 97.8	84.1	
										#20 #40	93.1	70.1	
	19.8				SM		Brown, Silty sand		08/24/21	#40 #60	93.1 84.4	56.8	
										#00 #100	69.3	43.6	
$\diamond$	17.8	1			SM		Grayish brown, Silty san	d	08/24/21	#100 #140	52.3	34.3	
_										#200	35.5	28.5	
0										5μ m	14		
Made N						-0.047				2μ m	9		
Matrix New	v World Eng	lineering	J, P.C.		#20-105	52-017	NJDCA MAP				7		
	TerraS	aneo			#21004	19534	93 Glenroy Road East					SIZE DISTRIBUTI	
_								-			ASTM D6	913 & ASTM D792	
erraSense	Analysis E	ilo: Crai		16Dov	1015							Sigv1g v	(lsx 9/1/202

TerraSense Analysis File: GrainSizeV6Rev1a15

Siev1a.xlsx 9/1/2021

# APPENDIX D

FEMA NFIP ELEVATION CERTIFICATE

# **ELEVATION CERTIFICATE**

**Important:** Follow the instructions on pages 1–9.

-		- · · · -							(-) -			
Con	aanen lle v	of this F	lovation	Cortificate and	l all attachment	e for (1	) community	1 official	(2) insurance	agent/company	and (3)	) building owner.
υup			lovation		. an allaoinnoil	3 101 (1		y onioiai,		agonycompany		/ Dunung Owner.

						-	, -
SECTION A – PROPERTY INFORMATION						ANCE COMPANY USE	
A1. Building Owner's Name					Policy Numl	per:	
A2. Building Street Address (including Apt., Unit, Suite, and/or Bldg. No.) or P.O. Route and Company NAIC Number:							AIC Number:
93 Glenroy Road East							
City				State		ZIP Code	
Town of Fairfield				New Jers		07004-1112	
A3. Property Descriptio Block 401, Lot 10	on (Lot ar	id Block Numbers, Ta	x Parcel	Number, Leo	gal Description, etc	.)	
A4. Building Use (e.g.,	Resident	tial, Non-Residential,	Addition,	, Accessory, e	etc.) Residentia	l	
A5. Latitude/Longitude:	: Lat. N4	10°53'34"	Long. W	/74°17'07"	Horizontal	Datum: 🗌 NAD 1	927 🗙 NAD 1983
A6. Attach at least 2 ph	notograph	ns of the building if the	e Certific	ate is being u	sed to obtain flood	l insurance.	
A7. Building Diagram N	lumber	2A					
A8. For a building with	a crawlsp	pace or enclosure(s):					
a) Square footage	of crawls	space or enclosure(s)		1	469.00 sq ft		
b) Number of perm	anent flo	od openings in the cra	awlspace	e or enclosure	e(s) within 1.0 foot	above adjacent gra	ide 5
c) Total net area of	f flood op	enings in A8.b		N/A sq in			
d) Engineered floo	d openin	gs? 🗌 Yes 🗶 N	lo				
A9. For a building with a	an attach	ed garage:					
a) Square footage of attached garage 468.00 sq ft							
b) Number of permanent flood openings in the attached garage within 1.0 foot above adjacent grade 0							
c) Total net area of	f flood op	enings in A9.b		N/A sq	in		
d) Engineered flood	d opening	gs? 🗌 Yes 🕱 N	lo				
	SE	CTION B – FLOOD I	NSURA	NCE RATE	MAP (FIRM) INF	ORMATION	1
	B1. NFIP Community Name & Community Number B2. County Name B3. State						
Fairfield, Township of				Essex			New Jersey
B4. Map/Panel B5. Number	. Suffix	B6. FIRM Index Date	Effe	RM Panel ective/ vised Date	B8. Flood Zone(s)	B9. Base Flood E (Zone AO, use	levation(s) e Base Flood Depth)
34013C0018 G		04-03-2020	04-03-2		AE	174' (NAVD88')	
B10. Indicate the source of the Base Flood Elevation (BFE) data or base flood depth entered in Item B9:							
☐ FIS Profile 🕱 FIRM  ☐ Community Determined  ☐ Other/Source:							
B11. Indicate elevation datum used for BFE in Item B9: NGVD 1929 X NAVD 1988 Other/Source:							
B12. Is the building located in a Coastal Barrier Resources System (CBRS) area or Otherwise Protected Area (OPA)? 🗌 Yes 🕱 No							
Designation Date:	:		CBRS				

					OMB No. 1660-0008 Expiration Date: November 30, 2022		
					FOR INSURANCE COMPANY USE		
Building Street Address (including Apt., Unit, Suite, and/or Bldg. No.) or P.O. Route and Box No.P93 Glenroy RoadP							
City	State ZIP	Code	Company	NAIC N	lumber		
Town of Fairfield	New Jersey 070	04-1112					
SECTION C -	BUILDING ELEVATION INFORMA	TION (SURVEY RE		)			
	required when construction of the buildi	<b>o</b> 1	L		ed Construction		
C2. Elevations – Zones A1–A30, AE, Al- Complete Items C2.a–h below acco Benchmark Utilized: CORS Network	rding to the building diagram specified	in Item A7. In Puert	o Rico only	–A30, A /, enter r	neters.		
	e elevations in items a) through h) belo						
NGVD 1929 X NAVD 1	, , ,	w.					
	nust be the same as that used for the E	BFE.					
		N N	-		asurement used.		
a) Top of bottom floor (including ba	sement, crawlspace, or enclosure floor	,		feet			
b) Top of the next higher floor			173.2	k feet	meters		
c) Bottom of the lowest horizontal s	tructural member (V Zones only)		N/A	feet	meters		
d) Attached garage (top of slab)			170.5	feet	meters		
<ul> <li>e) Lowest elevation of machinery o (Describe type of equipment and</li> </ul>	r equipment servicing the building location in Comments)		165.7	c feet	meters		
f) Lowest adjacent (finished) grade	next to building (LAG)		169.9	c feet	meters		
g) Highest adjacent (finished) grade	e next to building (HAG)		170.9	c feet	meters		
<ul> <li>h) Lowest adjacent grade at lowest structural support</li> </ul>	elevation of deck or stairs, including		169.8	feet	meters		
SECTION D	- SURVEYOR, ENGINEER, OR AR		CATION				
This certification is to be signed and seal I certify that the information on this Certif statement may be punishable by fine or i	ficate represents my best efforts to inter	rpret the data availa	law to cer ble. I unde	tify eleva erstand ti	ation information. hat any false		
Were latitude and longitude in Section A	provided by a licensed land surveyor?	X Yes 🗌 No	Ch	eck here	e if attachments.		
Certifier's Name Frank J. Barlowski	License Number 24GS03973500						
Title Professional Land Surveyor				DI	ace		
Company Name			_				
Matrix New World Engineering, Land Su	rveying and Architecture, P.C.				eal		
Address 442 State Route 35, Second Floor				Н	ere		
City Eatontown	State New Jersey	ZIP Code 07724					
Signature	Date	Telephone	Ext.				
Copy all pages of this Elevation Certificate	and all attachments for (1) community or	fficial, (2) insurance	agent/comp	bany, and	d (3) building owner.		
Comments (including type of equipment a C2(e): Base of hot water heater was at E	,						

OMB No.	1660-0	0008		
Expiration	Date:	November	30,	2022

ELEVATION CERTIFICATE	Expiration Date: November 30, 2022		
IMPORTANT: In these spaces, copy the correspo	nding information	from Section A.	FOR INSURANCE COMPANY USE
Building Street Address (including Apt., Unit, Suite, and/or Bldg. No.) or P.O. Route and Box No. 93 Glenroy Road			Policy Number:
City Town of Fairfield	State New Jersey	ZIP Code 07004-1112	Company NAIC Number
SECTION E – BUILDING FOR ZC		RMATION (SURVEY NO E A (WITHOUT BFE)	T REQUIRED)
For Zones AO and A (without BFE), complete Items complete Sections A, B,and C. For Items E1–E4, us enter meters.	E1–E5. If the Certifi e natural grade, if av	icate is intended to support vailable. Check the measur	a LOMA or LOMR-F request, ement used. In Puerto Rico only,
<ul><li>E1. Provide elevation information for the following a the highest adjacent grade (HAG) and the lower</li><li>a) Top of bottom floor (including basement,</li></ul>			er the elevation is above or below
crawlspace, or enclosure) is b) Top of bottom floor (including basement,		feet mete	ers above or below the HAG.
crawlspace, or enclosure) is		feet mete	ers above or below the LAG.
E2. For Building Diagrams 6–9 with permanent floor the next higher floor (elevation C2.b in	d openings provided	I in Section A Items 8 and/o	or 9 (see pages 1–2 of Instructions),
the diagrams) of the building is		feet mete	ers above or below the HAG.
E3. Attached garage (top of slab) is		feet mete	ers above or below the HAG.
E4. Top of platform of machinery and/or equipment servicing the building is		feet 🗌 mete	ers 🗌 above or 🗌 below the HAG.
E5. Zone AO only: If no flood depth number is avail floodplain management ordinance? [] Yes			ccordance with the community's t certify this information in Section G.
SECTION F – PROPERTY O	WNER (OR OWNE	R'S REPRESENTATIVE) (	ERTIFICATION
The property owner or owner's authorized represent community-issued BFE) or Zone AO must sign here	ative who completes . The statements in	s Sections A, B, and E for Z Sections A, B, and E are co	Cone A (without a FEMA-issued or prrect to the best of my knowledge.
Property Owner or Owner's Authorized Representati	ve's Name		
Address	(	City S	State ZIP Code
Signature	[	Date T	elephone
Comments			
			Check here if attachments.

OMB No.	1660-0	8000		
Expiration	Date:	November	30,	2022

ELEVATION CERTIFICATE	Expiration Date: November 30, 2022		
IMPORTANT: In these spaces, copy the corr	FOR INSURANCE COMPANY USE		
Building Street Address (including Apt., Unit, S 93 Glenroy Road	o. Policy Number:		
City Town of Fairfield	State New Jersey	ZIP Code 07004-1112	Company NAIC Number
SECTI	ON G – COMMUNITY IN	IFORMATION (OPTION	AL)
The local official who is authorized by law or o Sections A, B, C (or E), and G of this Elevation used in Items G8–G10. In Puerto Rico only, en	n Certificate. Complete th nter meters.	he applicable item(s) and	d sign below. Check the measurement
G1. The information in Section C was tal engineer, or architect who is authori data in the Comments area below.)	<en document<br="" from="" other="">zed by law to certify elev</en>	tation that has been sign ation information. (Indica	ned and sealed by a licensed surveyor, ate the source and date of the elevation
G2. A community official completed Sec or Zone AO.	tion E for a building locat	ed in Zone A (without a	FEMA-issued or community-issued BFE)
G3. The following information (Items G4	-G10) is provided for cor	mmunity floodplain mana	agement purposes.
G4. Permit Number	G5. Date Permit Issue	ed (	G6. Date Certificate of Compliance/Occupancy Issued
G7. This permit has been issued for:		Substantial Improvemer	nt
G8. Elevation of as-built lowest floor (includin of the building:			] feet 🔲 meters Datum
G9. BFE or (in Zone AO) depth of flooding at	the building site:	L	] feet meters Datum
G10. Community's design flood elevation:			feet meters Datum
Local Official's Name		Title	
Community Name		Telephone	
Signature		Date	
Comments (including type of equipment and lo	ocation, per C2(e), if appl	licable)	
			Check here if attachments.

### **ELEVATION CERTIFICATE**

### **BUILDING PHOTOGRAPHS**

See Instructions for Item A6.

OMB No. 1660-0008 Expiration Date: November 30, 2022

IMPORTANT: In these spaces, copy the	FOR INSURANCE COMPANY USE		
Building Street Address (including Apt., 93 Glenroy Road	Policy Number:		
City Town of Fairfield	State New Jersey	ZIP Code 07004-1112	Company NAIC Number

If using the Elevation Certificate to obtain NFIP flood insurance, affix at least 2 building photographs below according to the instructions for Item A6. Identify all photographs with date taken; "Front View" and "Rear View"; and, if required, "Right Side View" and "Left Side View." When applicable, photographs must show the foundation with representative examples of the flood openings or vents, as indicated in Section A8. If submitting more photographs than will fit on this page, use the Continuation Page.



Photo One Caption Front View

Clear Photo One



Photo Two Caption Rear View FEMA Form 086-0-33 (12/19)

Replaces all previous editions.

#### **ELEVATION CERTIFICATE**

## **BUILDING PHOTOGRAPHS**

**Continuation Page** 

OMB No. 1660-0008 Expiration Date: November 30, 2022

IMPORTANT: In these spaces, copy	FOR INSURANCE COMPANY USE		
Building Street Address (including Apt 93 Glenroy Road	Policy Number:		
City	State	ZIP Code	Company NAIC Number
Town of Fairfield	New Jersey	07004-1112	

If submitting more photographs than will fit on the preceding page, affix the additional photographs below. Identify all photographs with: date taken; "Front View" and "Rear View"; and, if required, "Right Side View" and "Left Side View." When applicable, photographs must show the foundation with representative examples of the flood openings or vents, as indicated in Section A8.



Photo Three Caption Right Side View

Clear Photo Three



Photo Four Caption Left Side View

Clear Photo Four

FEMA Form 086-0-33 (12/19)

Replaces all previous editions.